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# LARGE WOODY DEBRIS IN BULL TROUT SPAWNING STREAMS IN NORTHWEST MONTANA

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## INTRODUCTION

Large woody debris (LWD) plays numerous important roles in the structure and function of stream ecosystems (Gregory et al. 1991; Lamberti and Gregory 1996). Riparian forests often contribute vast quantities of LWD to a channel network, directly affecting both large and small scale stream geomorphology, hydrologic processes, and stream biota (Abbe and Montgomery 1996; Bisson and Montgomery 1996). Large wood accumulations influence the dissipation of stream energy and thus the ability of the stream to transport material. For example, LWD has been associated with channel avulsion, floodplain formation, and island development (Triska 1984; Abbe and Montgomery 1996). LWD also plays an important role in localized modification of streambed morphology (Bisson et al. 1987; Ralph et al. 1994), pool frequency and channel geometry (Bestcha and Platts 1986; Fausch and Northcote 1992; Richmond and Fausch 1995). The orientation and position of LWD in streams affects storage of organic and inorganic matter (Bilby and Ward 1989; Nakamura and Swanson 1993; Webster and Meyer 1997). Likewise , wood serves as trophic support of stream biota by providing organic matter for stream invertebrates and substratum for attachment and growth (Angermeier and Karr 1984; Benke et al. 1985; Hauer and Benke 1987, 1991).

The factors that directly affect introduction, stability, or character of stream LWD have a potentially significant influence on native fish populations that utilize streams for spawning, rearing, or growth and

completion of life histories (Andrus et al. 1988). Large woody debris and the implications of change in LWD on salmonid populations have been the focus of numerous studies (e.g., Marcus et al. 1990; Ralph et al. 1994; Riley and Fausch 1995). Of particular interest in western Montana, and indeed, throughout the Pacific Northwest are bull trout (*Salvelinus confluentis*), a native char whose populations have been declining range-wide and in many areas eliminated because of habitat degradation (Fraley and Shepard 1989; Howell and Buchanan 1992; Rieman and McIntyre 1993), over-harvest, and displacement by exotic species (Donald and Alger 1992; Leary et al. 1993).

Despite a generally ubiquitous trend of decline, until recently, the bull trout populations of the Flathead Basin in northwest Montana were considered relatively healthy. Strong spawning populations from Flathead Lake, Swan Lake and Hungry Horse Reservoir have been an important part of the native fish fauna and an important sport fishery. In the past several years, however, frequency distributions of bull trout spawning in tributaries of the North and Middle Forks of the Flathead River (i.e., the Flathead Lake population) have demonstrated serious declines (Weaver in press). Over fishing, competitive interactions, predation of juveniles, food web alterations in Flathead Lake, and loss of habitat for spawning and rearing have all been suggested as causes for this decline. It is highly likely, however, that no single factor can be isolated as the over-riding bottleneck. Rather, these factors likely play a synergistic role in the reduction of the Flathead Lake population. For example, inundation of spawning gravels with fine sediments or changes in channel form and complexity may be major factors affecting the decline in bull trout spawning in the tributary drainages of the North and Middle Forks of the

Flathead River (Weaver and Fraley 1991). Low frequency of spawning in some of the tributaries of the Swan River have been associated with the presence of logging roads (Baxter 1997). Although, the mechanisms that may be leading to the observed decline in bull trout are unclear, either on the landscape or in the streams, hydrologic and vegetative changes associated with past and perhaps present land use may play a role. A significant part of that role may be the result of change in the frequency and character of in-stream LWD.

Although it is known that LWD plays an important role among Pacific Northwest Coastal and Cascade streams and in Rocky Mountain streams in Colorado, little information is available about the character or function of LWD in streams of the northern Rocky Mountains. One should not assume that the processes that have been documented among Washington and Oregon streams (e.g., Nakamura and Swanson 1993; Ralph et al. 1994; Bisson and Montgomery 1996) or streams in Colorado (e.g., Fausch and Northcote 1992; Richmond and Fausch 1995) are seamlessly applicable in western Montana. Differences in climatic regime, landscape geomorphology, hydrologic regime, and the size, density and longevity of dominant riparian species among these regions will have direct bearing on the interactive relationship between stream structure and function and LWD.

Regardless of the various debates as to the cause of bull trout population declines or the current cumulative effects impinging on the health and long-term viability of bull trout populations in western Montana, the maintenance of productive spawning and rearing habitat will be critical to the long-term sustainability or recovery of bull trout (see Fausch and Northcote 1992). As the recent changes in the food web of

Flathead Lake, with its cascading effects on higher trophic levels (Spencer et al. 1991), comes to some new quasi-equilibrium; population restoration for bull trout will be significantly affected by reproductive success and juvenile survivorship. LWD may play a critical role in maintaining appropriate stream habitat and thus affect the long-term sustainability of bull trout populations in the Flathead Basin.

The purpose of this study was to describe the characteristics and selected functions of LWD among an array of known, historical bull trout spawning streams in the Flathead Basin. It was not our intention to specifically locate bull trout redds or covariation of redds and LWD; however, in several instances redds did occur with a study reach. Rather, streams were selected from each of the four major tributaries in the drainage; [the North and Middle Forks of the Flathead River (i.e., serving the Flathead Lake bull trout population), the South Fork of the Flathead River (i.e., serving the Hungry Horse Reservoir population) and the Swan River drainage (i.e., serving the Swan Lake population)] as subbasin representatives for the purposes of LWD characterization. Study streams also represented differing levels of land-use; including drainages with extensive harvest, including riparian clearcutting, to streams within designated wilderness. There were several primary objectives of the research: 1) to characterize LWD in bull trout spawning streams of the Flathead Basin, 2) examine relationships of LWD size, position, and orientation across an array of stream sizes 3) the role of LWD in affecting local scale, bed-form and stream morphology, and 4) to examine the potential effect of watershed landuse and/or riparian harvest on the size frequency structure, orientation and decay relationships of LWD.

## STUDY AREA and METHODS

### *The Flathead Basin*

This study was conducted in the Flathead Basin, an approximately 24,000 km<sup>2</sup> drainage in northwestern Montana and southeastern British Columbia along the west slope of the Continental Divide and within the belt-series of the northern Rocky Mountains (Figure 1). Sedimentary bedrock from the late Paleogene to the Proterozoic underlies the region and has been affected by low-grade metamorphosis (Ross 1959, Raup et al. 1983). These mountain ranges are part of the Rocky Mountain Belt Supergroup and consist of argillites, siltites, and carbonates with a maximum stratigraphic thickness of 5,200m (Whipple et al. 1984). The heavily forested valleys are mantled by colluvium and glacial till. During the height of the last major glaciation, about 20,000 years ago, the Flathead Basin was covered by glacial ice. The main glacial advance flowed from the cordilleran ice sheet down the Rocky Mountain Trench. Smaller valley glaciers flowed from the Livingston, Whitefish, Swan, Flathead and Mission Ranges to merge along the valley floors forming trunk glaciers as much as 1000m thick (Alden 1953). Alluvial valley segments of tributary drainages formed with faulting and local accumulations of valley fill from alluvial and glacial sources.

Twenty stream reaches were selected for study from eight streams distributed around the basin (Figure 1; Table 1). All reaches were in third or fourth order segments (*sensu* Strahler 1963) of streams identified by Montana Department of Fish, Wildlife and Parks as known bull trout spawning tributaries (T. Weaver, pers. comm.). Additionally, streams were selected based on their drainage-wide land use history. Reaches within

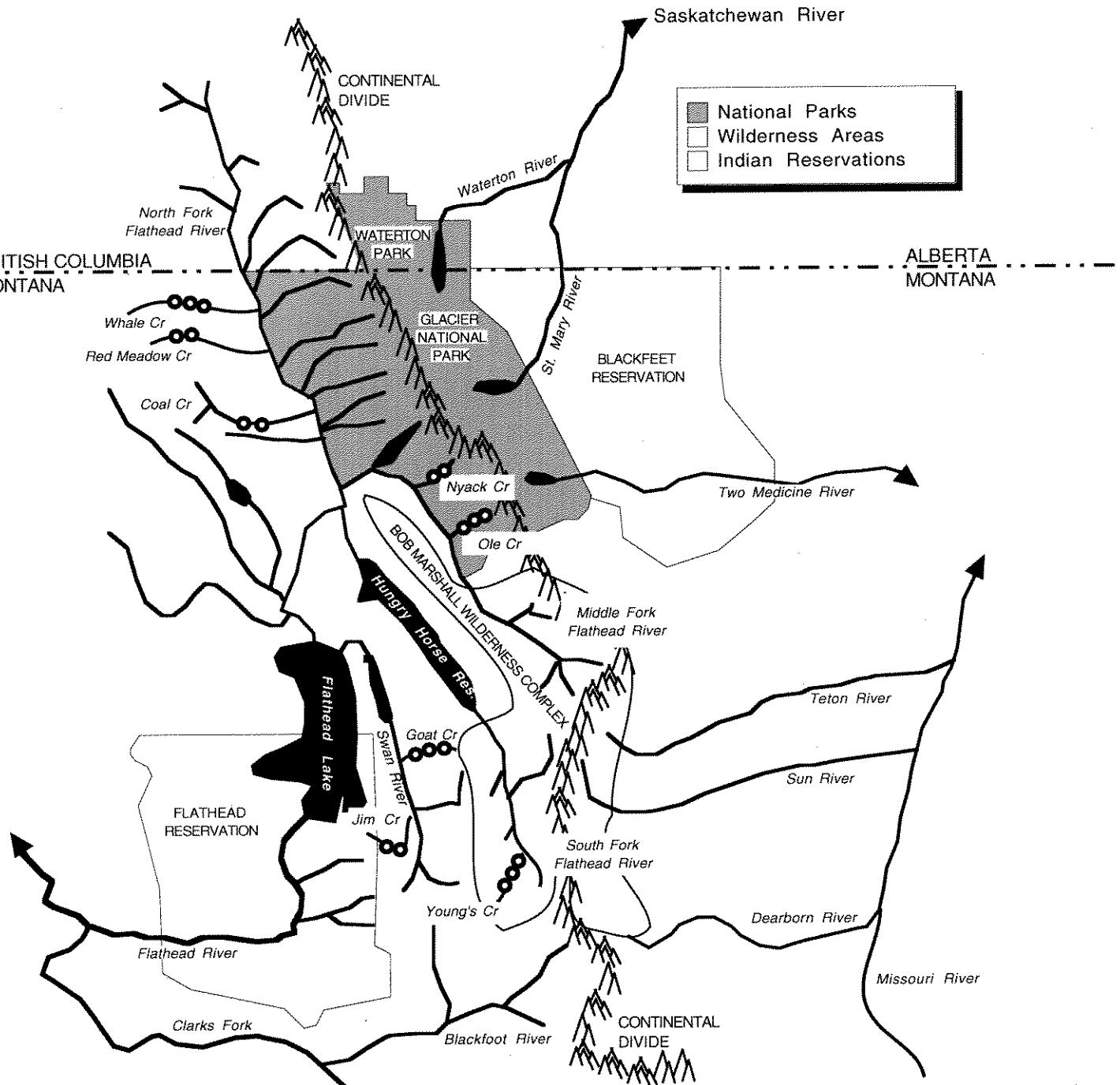


Figure 1. Map of the Flathead Basin and northern Continental Divide region of northwest Montana. Names of major drainages are given next to each river. Study stream reaches are denoted by open circles and names of the study streams.

Table 1. Drainage, stream name, reach, watershed area above study reaches and the number of channels in each study reach.

Flathead River Drainage	Stream Name	Drainage area (acres)	Reach	Number of channels
Middle Fork	Ole Creek	25429	A	1
			B	1
			C	1
North Fork	Nyack Creek	54353	A	1
			B	1
			A	1
North Fork	Red Meadow Creek	3982	B	1
			A	1
			B	1
South Fork	Whale Creek	24296	C	1
			A	2
			B	1
South Fork	Coal Creek	29920	C	1
			A	2
			B	1
Swan River	Young's Creek	57523	A	1
			B	1
			C	1
Swan River	Jim Creek	9151	A	1
			B	1
			A	2
Swan River	Goat Creek	13837	B	3
			C	4

streams were selected based on prevalent streamside management within the basin. In some cases, as in Red Meadow Creek, the selected reaches flowed through riparian clearcuts, which occur commonly along that stream's length. Among other streams, such as Ole Creek in Glacier National Park, the riparian zone along the study reach was in a natural, undisturbed condition.

### *Stream Channel*

Stream cross-sectional profiles, sinuosity and gradient were measured at each stream reach using an Abney level, a Sonin® electronic distance measurer, and a leveling rod. Eleven transects (A-K) were taken across each stream reach at 10m intervals covering a total reach length of 100m. Each transect consisted of channel profiles measured from the stream thalweg perpendicularly to the top of the bankfull channel on both sides of the stream. Typically 8-12 measures were taken to develop the channel profile at each transect. The channel profile data included all major breaks in elevation, the wetted channel width, water depth at the thalweg (at the time of measure), and height of the average bankfull channel. The angle from the stream bank to the stream thalweg and then to the thalweg position of the upstream transect was measured with a surveying compass. The change in bed height and water depth between each transect profile was measured using the Abney level, electronic distance measurer, and the leveling rod. Current velocity at the thalweg of each transect was estimated as the mean of five separate measures over a 3m distance using a surface float and stopwatch. The 10m intervals between each transect was identified as a stream reach block.

### *Large Woody Debris*

Measures of LWD were made within the 10m stream reach blocks of each 100m stream reach and referenced to the lower transect. For example, the LWD in segment **g** would be all pieces between transects **G** and **H**. LWD was defined as logs  $\geq$ 10cm diameter and  $\geq$ 1m in length. Although there is no standard criteria established as to the minimum size that constitutes LWD, the criteria used here are the same as has been used in research at other locations (Andrus et al. 1988, Fausch and Northcote 1992, Richmond and Fausch 1995). Each piece of wood meeting the LWD criteria was measured if any part occurred within or was suspended above the bank-full stream channel. The diameter was measured at each end of the LWD piece with a 1m caliper. The length of each piece was measured with the Sonin® electronic distance measurer if the length was  $>$ 2m or with the caliper for shorter pieces. Piece volume was estimated from the equation in Lienkaemper and Swanson (1987):

$$V = \frac{\pi(D_1^2 + D_2^2)L}{8}$$

where V is the volume,  $D_1$  and  $D_2$  are the diameters at opposite ends of the piece and L is the piece length. All large root wads were considered LWD regardless of length. Stumped root wads with a length  $<$ 1m were common among streams whose riparian areas had been logged. Volume of root wads were determined by measuring the diameter of the root structure across the dominant mass ( $D_1$ ) and the bole of the tree or stump above the root structure ( $D_2$ ) and the distance between these measurements (L).

The position and orientation of LWD to the channel was determined

for each LWD piece. Piece position was recorded as being in one of three possibilities: (a) no contact with either bank, (b) contacting either the left or right bank, and (c) contacting both banks. In addition to simply contacting a bank, many pieces were strongly attached to one, or rarely, both banks. Bank attachment appeared to have a significant effect on orientation and the ability of the piece to resist stream power and remain across the stream thalweg. In turn, this dramatically affected streambed morphology.

Orientation of LWD is known to affect stream flow and bed morphology (Robison and Bestcha 1990). Likewise, stream power affects piece orientation by moving unattached ends in a downstream direction. Piece orientation was divided into three categories: (a) at an approximately  $0^\circ$  angle (parallel) to the channel, (b) at an approximately  $45^\circ$  angle to the channel, and (c) at an approximately  $90^\circ$  angle (perpendicular) to the channel. We also noted whether a piece had a rootwad attached to the bole since this plays an important function in the attachment, orientation, and distribution dynamics of the piece.

The relative age of each piece was assessed using a modification of the Grette (1985) decay classification procedure which divided LWD into four decay classes: (1) bark and branches attached, (2) bark and branches missing, wood solid with evidence of decay restricted to the outer perimeter, (3) wood showing significant signs of decay to at least depths of 5-10cm, and (4) wood soft and decayed nearly or completely to the center of the piece. We later combined categories c and d for our analysis because of the infrequency of observing type 4 decay-class LWD. We believe the scarcity of decay-class 4 wood is due to the rapidity of final decay and disappearance once a piece transitions from class 3 to class 4.

## **RESULTS and DISCUSSION**

Summary illustrations for each stream reach are given in Appendix A. The LWD data are compiled for reference in Appendix B. The Appendix A illustrations are organized by study reach and consist of three illustrations for each reach.

In Appendix A, Illustration 1 for each stream reach consists of three panels; 1) a topographical representation of the study reach including elevation contours, the location and orientation of survey transects and survey points, the position of the stream thalweg and bull trout redds, if present, 2) Figure A, is the number of LWD pieces measured within each of the ten 10m study segments, and 3) Figure B, the LWD volume ( $m^3$ ) within those same 10m segments.

Illustration 2 consists of six figures of percentages of LWD pieces within each of the 10m segments: 1) percent by diameter (cm) class, 2) percent by decay stage, 3) percent by position, 4) percent by orientation, 5) percent by attachment, and 6) percent having a root wad attached.

Illustration 3 consists of two figures: 1) the top panel is a longitudinal profile of thalweg and water surface elevation, and 2) the lower panel is a longitudinal profile of current velocity at the thalweg of each transect.

These illustrations of each stream reach, the LWD found within each reach, and the streambed contours and thalweg current velocities are presented to provide a quick reference for the data from each stream reach.

### *General Characteristics of Study Reaches*

All study reaches were within 3rd- to 4th-order segments of known bull trout streams. Mean bank-full widths of all stream reaches combined were 14.15m (6.6m [1 stddev]) with a range of 3.9m to 36.7m across all transects. Study reaches were variable, both between and within streams. Stream gradients among all reaches were moderate (mean 1.02%, max 2.6%), but again highly variable. The thalweg position of some downstream transects were at a higher elevation than upstream transects; clearly illustrating streambed habitat complexity.

Five of the 20 study reaches had one or more side channels. In cases where side channels were present, there was always one dominant channel. The side channels were always small with only minor flow. The side channels in Coal Creek Reach A and Young's Creek Reach B contained a high density of LWD and likely were at one time the main channel.

Stream depths across all transects ranged from a minimum depth of 0.15m in Ole Creek Reach A to a maximum of 1.33m in Young's Creek Reach C (Figure 2). Among reach maximum depths, Young's Creek, which also had the largest drainage area above the study reaches, had the highest maximum depths. The relationship of stream depths to drainage area showed a weakly positive correlation for both maximum depth and mean depth. The minimum depth of each stream reach was not correlated with basin size (Figure 3).

The substratum of each study reach was similar, generally composed of gravel and cobble; although occasionally larger boulders (50-100cm) were also present. The drainage area above the study reaches varied from 57,523 acres (23,289 ha) on Young's Creek to 3,982 acres (1,612 ha) on Red Meadow Creek (Table 1).

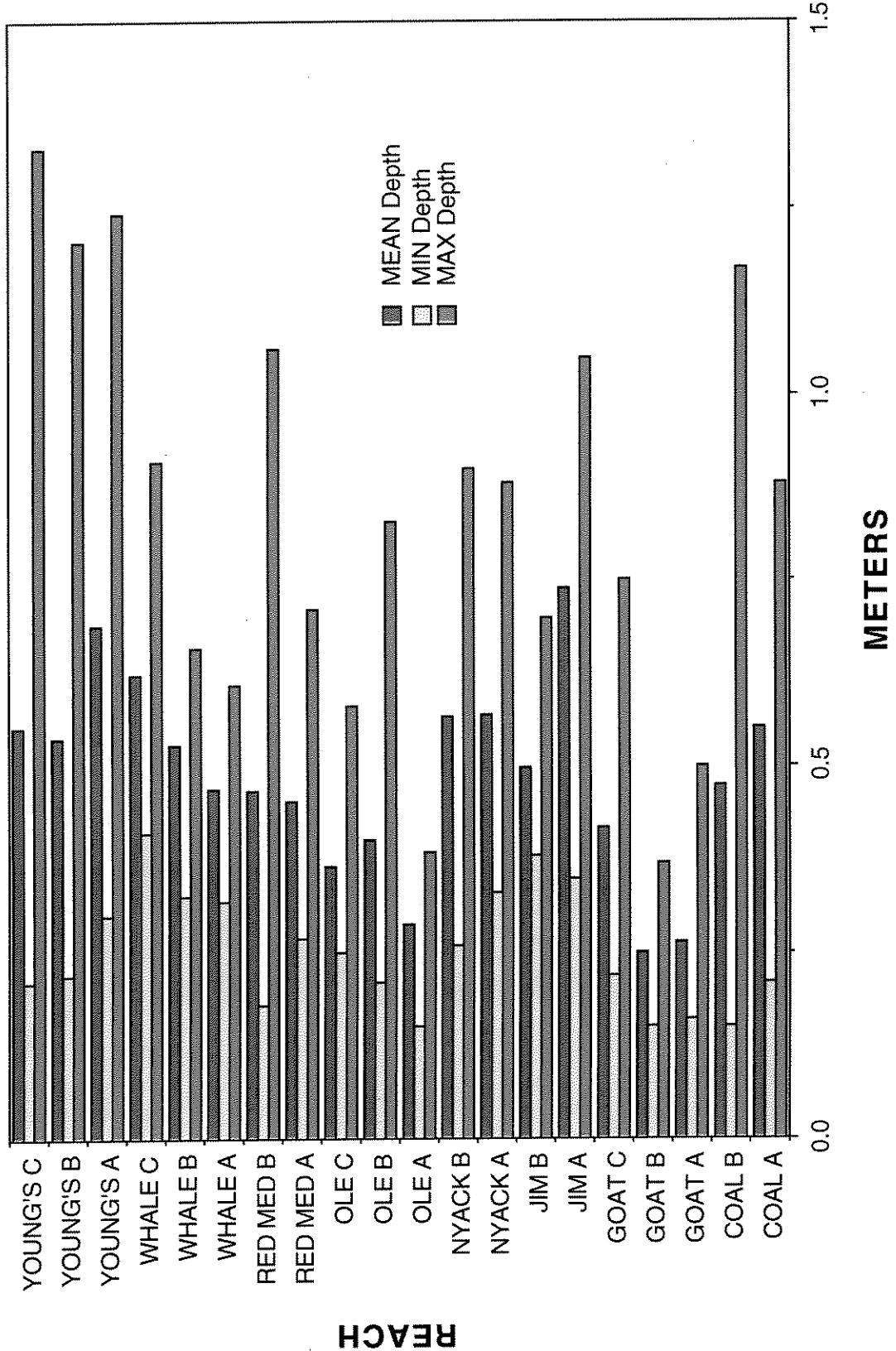


Figure 2. Mean, maximum and minimum depth of the stream thalweg across all transects within the study stream reaches.

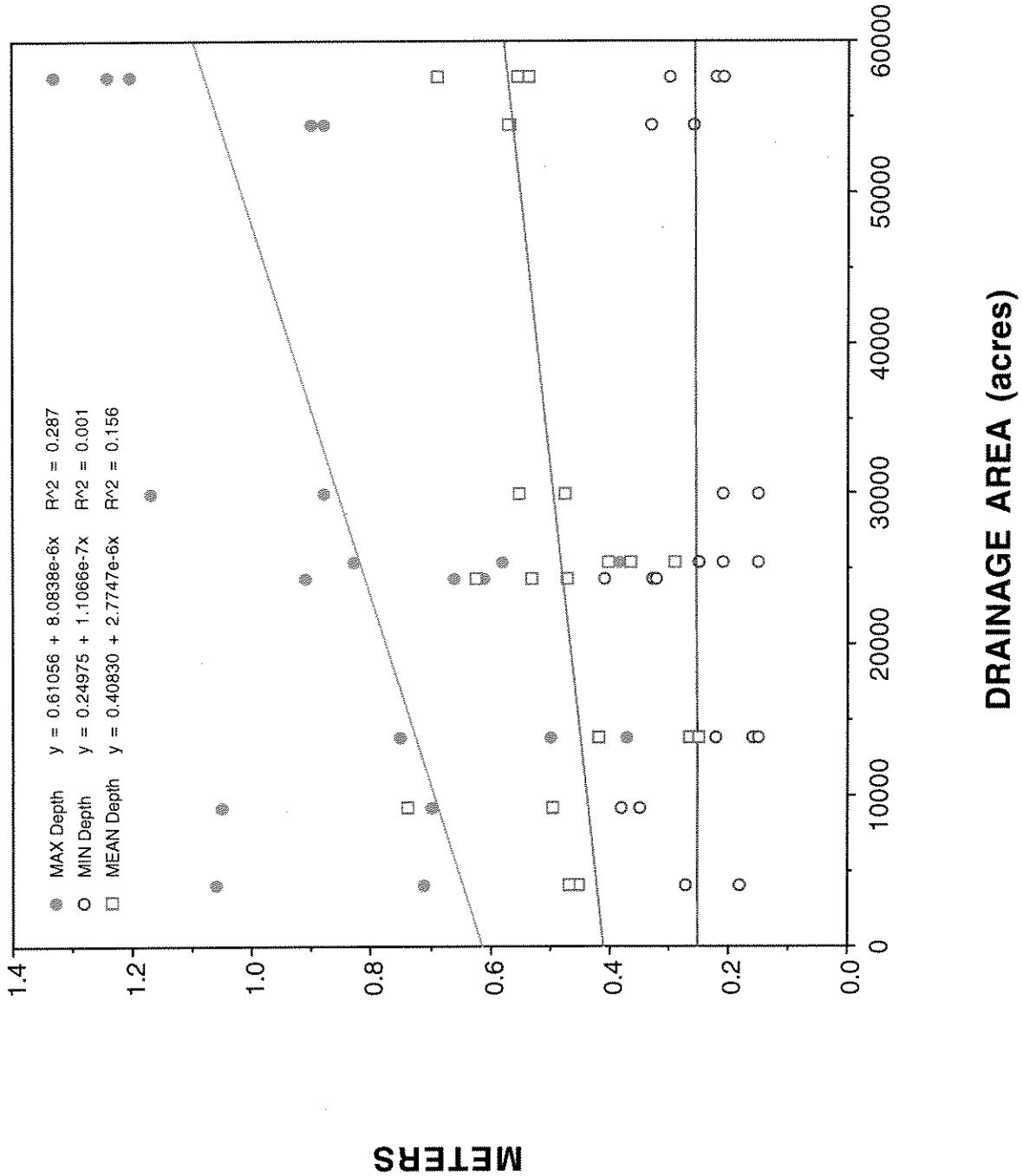


Figure 3. Mean, maximum and minimum thalweg depths among all transects for each stream reach regressed against the drainage area of each watershed above each study reach.

### *General Characterization of Large Woody Debris*

A total of 1320 pieces of LWD were counted and measured among all study reaches. The number of pieces and volume of LWD across all reaches was highly variable (Table 2). For example, Reach A on Young's Creek had 184 pieces, while in contrast Reach B on Nyack Creek had only 5 pieces of LWD.

Among all stream reaches the size of the LWD was also extremely variable (Figure 4). About 70% of all LWD was in the smaller two diameter classes (>35% 10-19cm; and >30% 20-29cm; Figure 4 Panel A). Likewise, >50% of the LWD was between 1m and 4m in length (Figure 4, Panel B). Both diameter measures and tree length measures demonstrated a decreasing exponential curve (Figure 4). Together, well over 50% of the LWD across all stream reaches consisted of pieces <30cm in diameter and <4m in length. However as in other studies, we found that the large pieces played the primary role in stream bed configuration and the formation of aggregates. (Discussed at greater length below).

Other studies have found that LWD attachment to one or both banks and/or the presence of the tree's rootwad are important factors influencing the stability (i.e., the resistance to being moved during flood) and orientation of the LWD piece (Bestcha and Platts 1986, Ralph et al. 1996). We found attachment to one or both banks and the numbers of pieces that had rootwads to be highly variable; commensurate with the high variation in LWD between stream reaches (Tables 2 and 3). However, we did find interesting relationships between the orientation of the LWD piece (Table 4) the percentage attached to one or both banks, the volume of the LWD piece, and the length of the piece (Figure 5).

Table 2. Volume, attachment, and with or without a connected rootwad of LWD among the study reaches.

Stream Name	Reach	Frequency (no)	Volume (m3)	Attachment		Rootwad	
				attached	unattached	WITHOUT	WITH
Ole Creek	A	13	20.6	5	8	7	6
	B	29	25.9	17	12	27	2
	C	32	58.7	7	25	25	7
Nyack Creek	A	7	1.6	1	6	7	0
	B	5	12.0	2	3	4	1
	C	51	82.4	35	16	42	9
Red Meadow Creek	A	123	212.1	95	28	115	8
	B	56	57.2	26	30	55	1
	C	87	77.5	37	50	87	0
Whale Creek	A	91	116.8	59	32	74	17
	B	123	119.0	57	66	119	4
	C	36	51.0	19	17	34	2
Young's Creek	A	184	200.6	90	94	157	27
	B	77	53.2	49	28	62	15
	C	37	38.5	17	20	32	5
Jim Creek	A	117	172.3	72	45	99	18
	B	46	38.8	35	11	44	2
	C	61	41.4	31	30	53	8
Goat Creek	A	70	60.3	49	21	64	6
	B	75	177.3	54	21	55	20
	C						

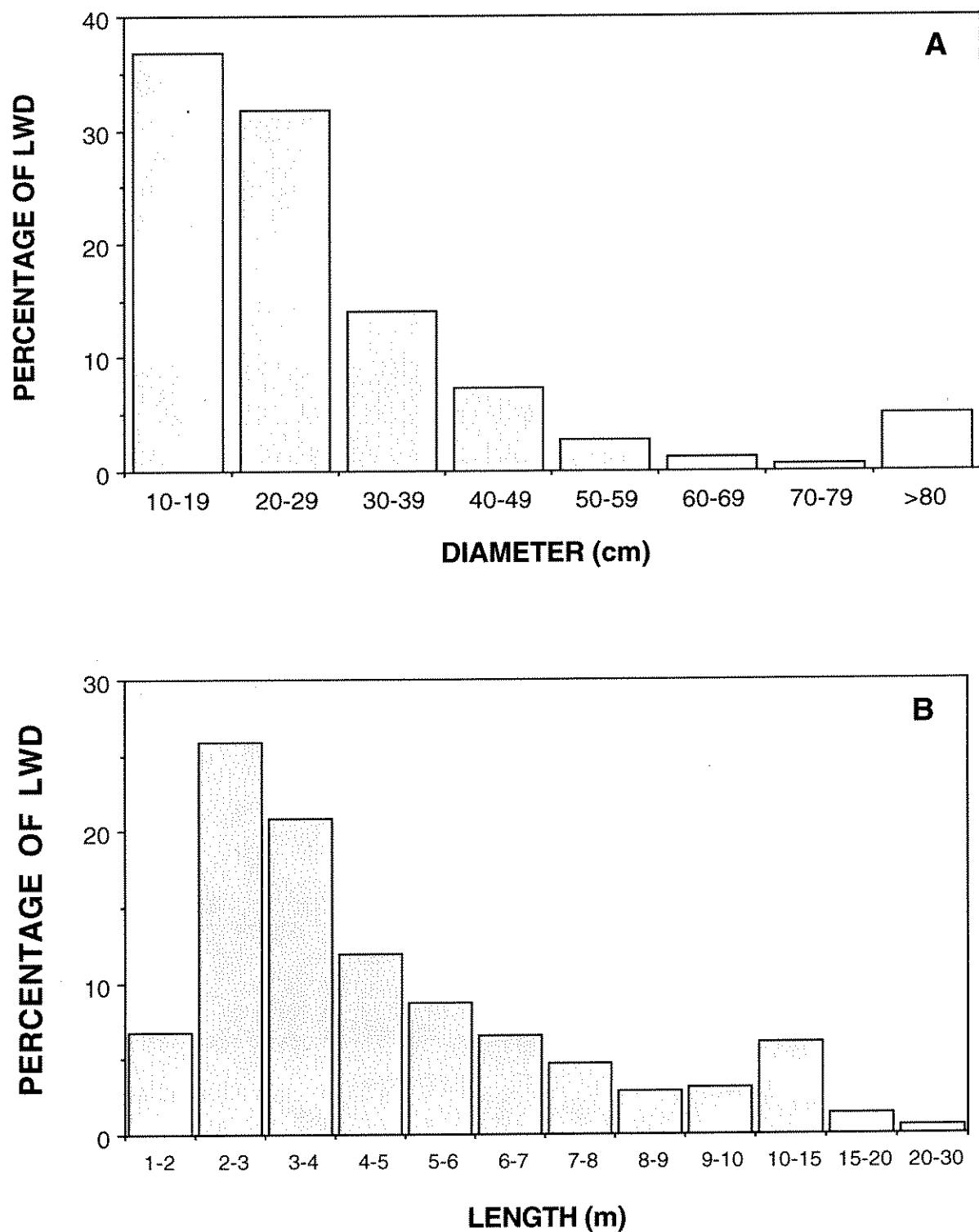


Figure 4. (Panel A) The percent of Large Woody Debris in each of 8 diameter size classes. (Panel B) The percent of Large Woody Debris in each of 12 length size classes.

Table 3. Position of LWD in each study stream reach by diameter class and whether it is in contact with the stream banks.

Flathead River Drainage Fork	Stream Name	Drainage area (acres)	Reach	No contact with banks				Contracting one bank by Diameter Class				POSITION			
				No contact with banks by Diameter Class				Contracting one bank by Diameter Class				Contacting both banks by Diameter Class			
				1	2	3	4	1	2	3	4	1	2	3	4
Middle Fork	Ole Creek	25429	A	2	0	0	1	2	3	2	3	0	0	0	0
			B	5	3	2	4	7	5	1	2	0	0	0	0
			C	3	6	1	4	5	5	3	5	0	0	0	0
Nyack Creek	54353	3982	A	2	0	0	0	3	1	0	0	0	0	0	0
			B	1	1	0	0	1	0	1	1	0	0	0	0
			C	4	7	2	7	4	9	7	9	0	1	1	0
North Fork	Red Meadow Creek	3982	A	7	21	10	13	9	19	13	30	0	0	0	1
			B	19	12	6	1	20	18	8	3	0	0	0	0
			C	15	19	9	6	14	15	8	5	0	0	0	0
Whale Creek	24296	A	14	14	1	0	13	7	4	3	0	0	0	0	0
			B	14	14	1	0	20	18	8	3	0	0	0	0
			C	15	19	9	6	14	15	8	5	0	0	0	0
Coal Creek	29920	A	44	24	5	4	16	17	4	6	0	2	1	0	0
			B	9	4	3	1	8	3	2	5	0	1	0	0
			C	15	7	3	5	11	16	7	14	1	1	0	0
South Fork	Young's Creek	57523	A	56	37	20	14	14	18	13	10	0	0	0	0
			B	11	7	2	5	24	13	6	9	0	0	0	0
			C	15	7	3	5	3	3	1	0	0	0	0	0
Swan River	Jim Creek	91151	A	23	22	8	6	11	16	7	14	1	3	4	2
			B	7	2	0	0	17	8	1	5	1	0	3	1
			C	11	9	3	9	7	5	6	11	2	3	1	8

Diameter Classes: 1 = 10-20cm; 2 = 20-30cm; 3 = 30-40cm; 4 = >40cm

Table 4. Orientation of LWD in the study streams by diameter class.

Flathead River Drainage	Stream Name	Drainage area (acres)	Reach by Diameter class	ORIENTATION							
				0 degrees				45 degrees			
				1	2	3	4	1	2	3	4
Middle Fork	Ole Creek	25429	A	1	0	1	0	2	3	1	4
			B	4	3	0	1	4	3	2	3
			C	4	6	3	4	3	4	1	1
Nyack Creek	54353		A	2	0	0	0	3	1	0	0
			B	2	1	1	0	0	0	0	0
			C	4	5	4	3	3	2	4	3
North Fork	Red Meadow Creek	3982	A	2	4	5	4	5	18	9	12
			B	3	7	1	4	5	18	9	12
			C	13	19	3	1	10	2	2	2
Whale Creek	24296		A	13	19	3	1	18	13	6	1
			B	19	14	6	3	18	13	6	1
			C	13	14	14	5	11	13	3	1
Coal Creek	29920		A	33	20	3	4	17	17	6	6
			B	7	2	2	3	5	2	0	1
			C	13	14	14	5	11	13	3	1
South Fork	Young's Creek	57523	A	16	16	8	5	43	29	20	9
			B	11	7	2	1	20	9	3	10
			C	6	4	0	4	9	4	4	0
Swan River	Jim Creek	9151	A	9	8	2	3	19	19	8	8
			B	7	3	0	2	13	7	1	2
			C	6	4	0	4	9	4	4	0
Goat Creek	13837		A	6	7	1	2	6	2	2	1
			B	15	5	3	3	9	7	1	4
			C	4	5	2	4	7	3	4	8

Diameter Classes: 1 = 10-20cm; 2 = 20-30cm; 3 = 30-40cm; 4 = >40cm

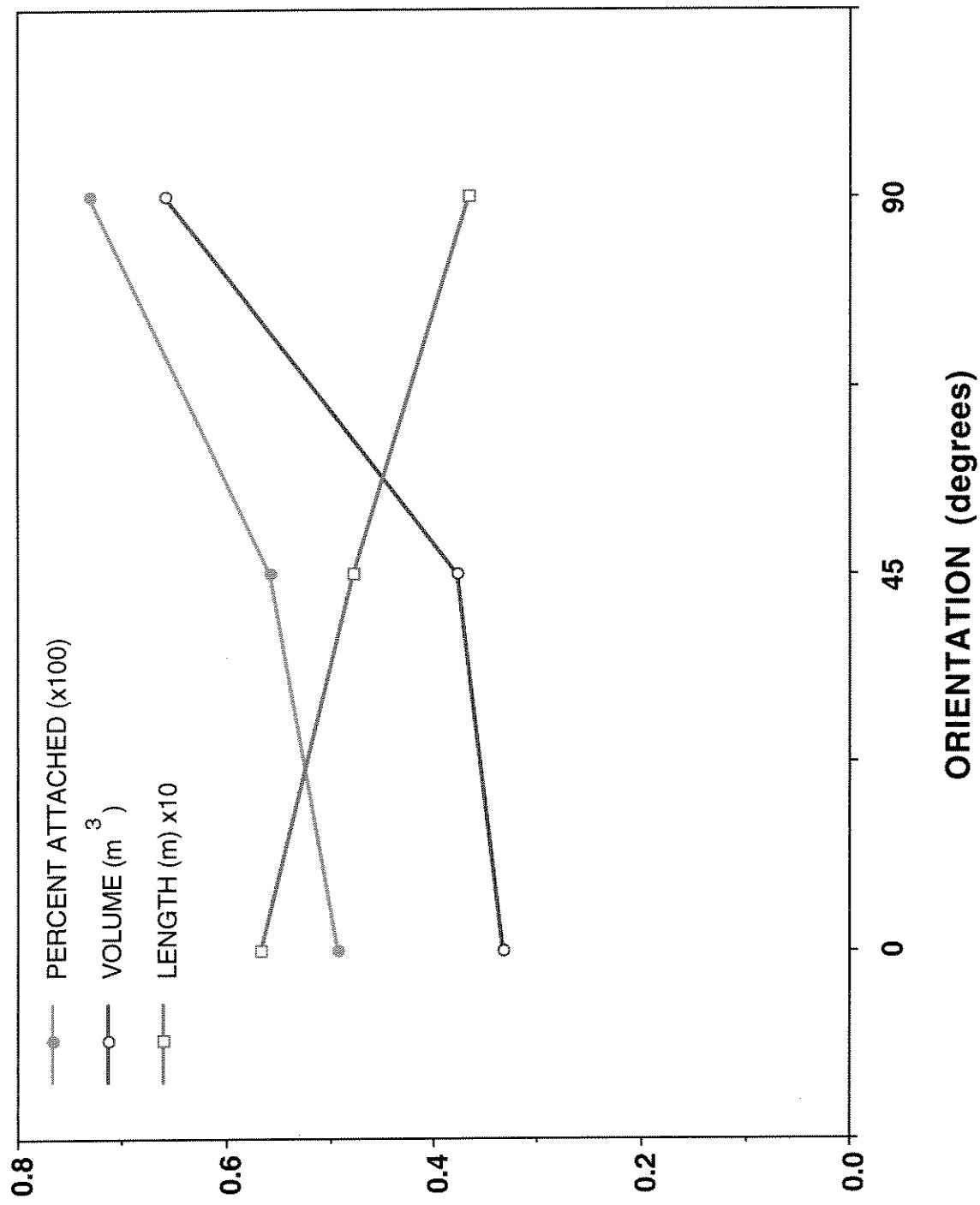


Figure 5. Among all stream reaches combined, the mean percent attached, the mean volume and the mean length of Large Woody Debris oriented at 0 degrees (parallel), 45 degrees, or 90 degrees (perpendicular) to the stream current.

Among all LWD pieces from all reaches combined, those oriented at a 90° angle to the current (i.e., perpendicular to the thalweg) had a much higher frequency of attachment to a bank and had a larger volume than those pieces that were at either a 45° angle or parallel to the stream flow. We found that bank attachment often extended a considerable distance onto the bank and back into the riparian vegetation. These pieces were often the most stable and demonstrated resistance to change in orientation.

There was also a significant trend in decreasing stem length among LWD pieces that were parallel vs. perpendicular to the flow. This is likely due to longer pieces being subject to rotation around an anchor point, such as a bank attachment, during flooding when stream power and floatation of the LWD is at its highest. To summarize, those pieces that were at a 90° angle to the current tended to be attached to at least one of the banks and tended to be large diameter and short. These features are particularly important since 90° angle pieces are the most interactive with the stream channel and tend to be most responsible for change in streambed morphology and complexity.

We also examined the relationship of LWD wood decay (Table 5). We found that among all stream reaches most LWD was in Stage 2 decay class; that is, most pieces had been stripped of their bark and branches and showed only the earliest signs of rotting at the surface. This finding has a couple of implications: 1) that most of the wood has been in the stream for at least several years, long enough to lose the outer bark and limbs, but not so long as to enter advanced decay stages, 2) the paucity of Stage 3 and 4 decay classes suggests that once a LWD piece enters latter stages of decay decomposition processes occur rapidly. The later stages of decay may be significantly enhanced during spring runoff as increased stream

Table 5. Decay class of LWD, by diameter class, in the study streams.

Flathead River Drainage	Stream Name	Drainage area (acres)	Reach	DECAY CLASS			
				w/ bark&limbs	Surface rotted	by Diameter class	by Diameter class
Middle Fork	Ole Creek	25429	A	1 0 0 0	3 3 2 4	1 2 3 4	1 2 3 4
			B	6 2 0 1	6 6 3 5	0 0 0 0	0 0 0 0
			C	2 1 0 2	6 10 4 7	0 0 0 0	0 0 0 0
Nyack Creek	54353	A	2 1 0 0	3 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0
		B	1 0 1 1	1 1 0 0	0 0 0 0	0 0 0 0	0 0 0 0
			C	0 1 0 0	8 16 10 16	0 0 0 0	0 0 0 0
North Fork	Red Meadow Creek	3982	A	0 0 0 0	16 40 23 44	0 0 0 0	0 0 0 0
		B	0 0 0 0	25 20 2 2	0 0 0 0	0 0 0 0	0 0 0 0
			C	5 4 2 0	34 26 12 4	0 0 0 0	0 0 0 0
Whale Creek	24296	A	2 1 3 1	24 31 15 9	0 0 0 0	0 0 0 0	0 0 0 0
		B	5 4 2 0	45 28 6 8	2 2 2 0	0 0 0 0	0 0 0 0
			C	5 3 2 2	12 7 5 5	0 0 0 0	0 0 0 0
Coal Creek	29920	A	13 13 2 2	69 54 32 22	0 0 0 0	0 0 0 0	0 0 0 0
		B	5 1 0 1	35 20 8 14	0 0 0 0	0 0 0 0	0 0 0 0
			C	1 1 0 1	17 9 4 4	0 0 0 0	0 0 0 0
South Fork	Young's Creek	57523	A	2 2 1 2	32 34 14 14	0 0 0 0	0 0 0 0
		B	0 0 0 0	20 9 1 3	0 1 0 1	0 1 0 1	0 1 0 1
			C	1 1 0 1	15 13 6 8	1 4 1 4	1 4 1 4
Swan River	Jim Creek	9151	A	3 7 5 5	19 13 4 4	0 3 1 0	0 3 1 0
		B	5 0 3 2	14 13 8 13	0 0 0 0	0 0 0 0	0 0 0 0
			C	6 4 2 12	14 13 8 13	0 0 0 0	0 0 0 0

Diameter Classes: 1 = 10-20cm; 2 = 20-30cm; 3 = 30-40cm; 4 = >40cm

power causes decomposed logs to break apart. We did not conduct tests that would permit us to age the LWD to directly determine to rate of decomposition; however, based on our knowledge of aggregate accumulations at many sites throughout the Flathead Basin we know of pieces that have been in streams for over 20 years and are showing no signs of surface decomposition. Thus, it appears that LWD may remain in these streams for very long time periods (e.g., >50 years).

#### *LWD Influence on Streambed Morphology*

An important feature of stream habitat structure is the development and stability of streambed morphology. Streams that alternate between riffles, pools and runs provide complex habitats for high biodiversity, biomass, and secondary production of aquatic insects and fishes. Likewise, complex variation in stream habitat and streambed morphology are frequently required for different life history stages and reproductive success among macroinvertebrates and fish species.

Using correlation analysis, we examined the role of LWD and its influence on streambed morphology. We found that as the number of pieces of LWD and the volume of LWD increased within a stream reach block (i.e., 10m section between transects) there was a corresponding increase in the negative slope of the reach immediately downstream (Figure 6). The most strongly negative bedslopes were all associated with upstream aggregates, large snags with rootwads, or large diameter LWD oriented perpendicular to the stream thalweg. Each of these LWD structures perform one or both of two important bedforming functions; 1) the retention of gravels on the upstream side of the structure, and/or 2) the focus of hydraulic flow and thus stream power on the downstream bed

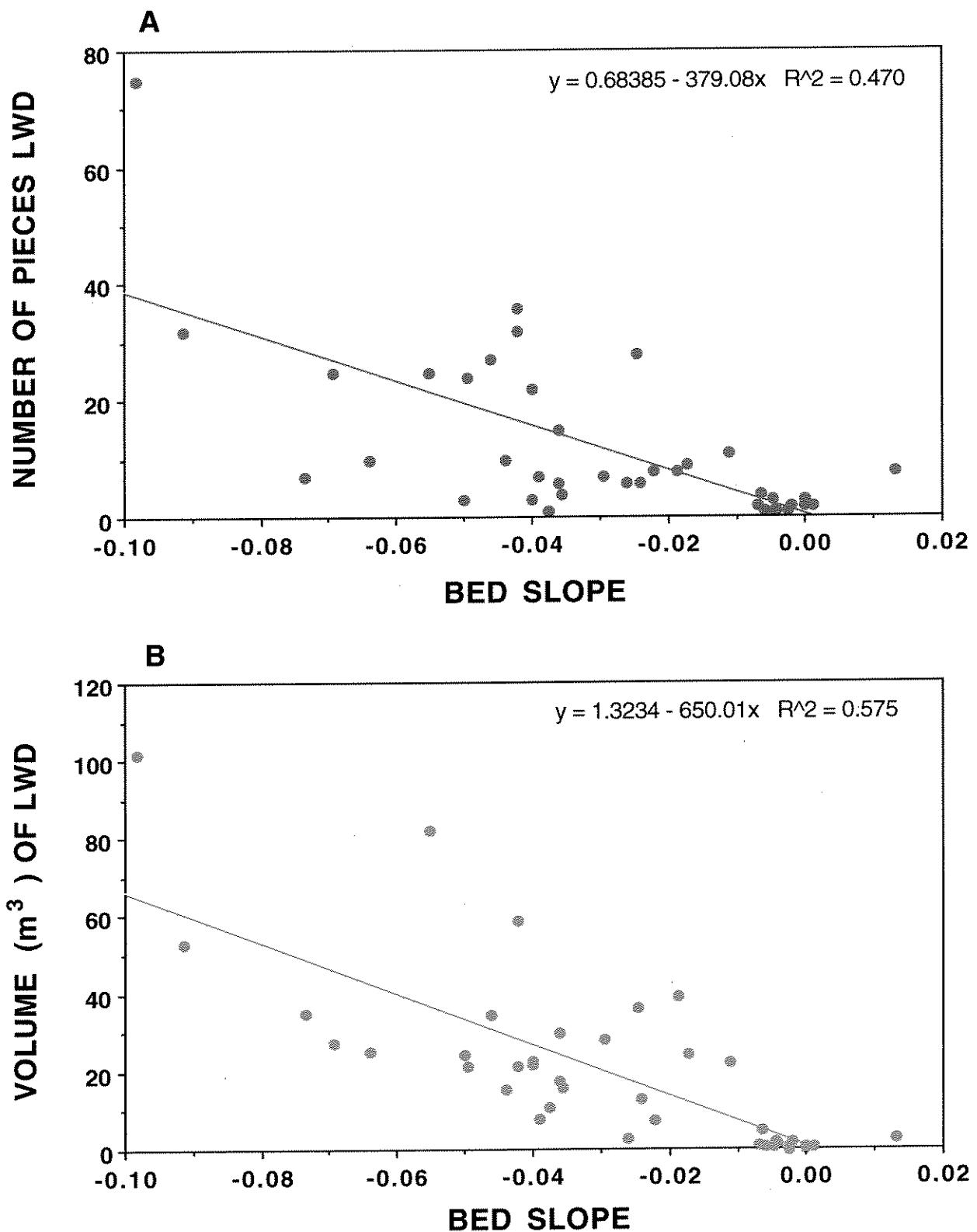


Figure 6. The number of pieces of Large Woody Debris (Panel A) and the volume of Large Woody Debris (Panel B) in the upstream 10 m reach block and the corresponding downstream bedslope.

material. Both of these factors lead to the aggregation of upstream gravel and cobble and the downstream degradation of bed material. Interestingly, the  $r^2$  for LWD volume was much higher than that for frequency of pieces. This underscores the importance of large wood, and large wood within aggregates, to stabilize bedload, capture gravel, and promote pool formation.

#### *Land-use Influence on LWD*

Three of the 8 watersheds (8 of 20 study reaches) examined were located within Glacier Park or the Bob Marshall Wilderness. Each of these 3 watersheds are managed as wilderness and have never been harvested or roaded. The other 5 watersheds were in the North Fork or the Swan River drainages and flow through lands managed for multiple use, including timber harvest. Each of the 12 study reaches were sited downstream from harvested portions of the 5 watersheds.

We found that there was a linear relationship between large LWD (dia.  $\geq 30\text{cm}$ ) and small LWD (dia.  $< 30\text{cm}$ ) among the reaches draining wilderness areas (Figure 7), with a remarkably small variance in the relationship ( $r^2 = 0.977$ ). In contrast, among reaches in watersheds with upstream harvest the large to small LWD size relationship was highly scattered and not significantly different from zero ( $r^2 = 0.032$ ). These data suggest that there is a highly predictable and relatively stable relationship between the frequency of large diameter trees and small diameter trees entering the LWD pool in unharvested watersheds, independent of the total number of LWD pieces present. Among the watersheds with timber harvest we noted that three of the four data points (Figure 7, blue) located above the regression line of the unharvested watersheds (Figure 7, red)

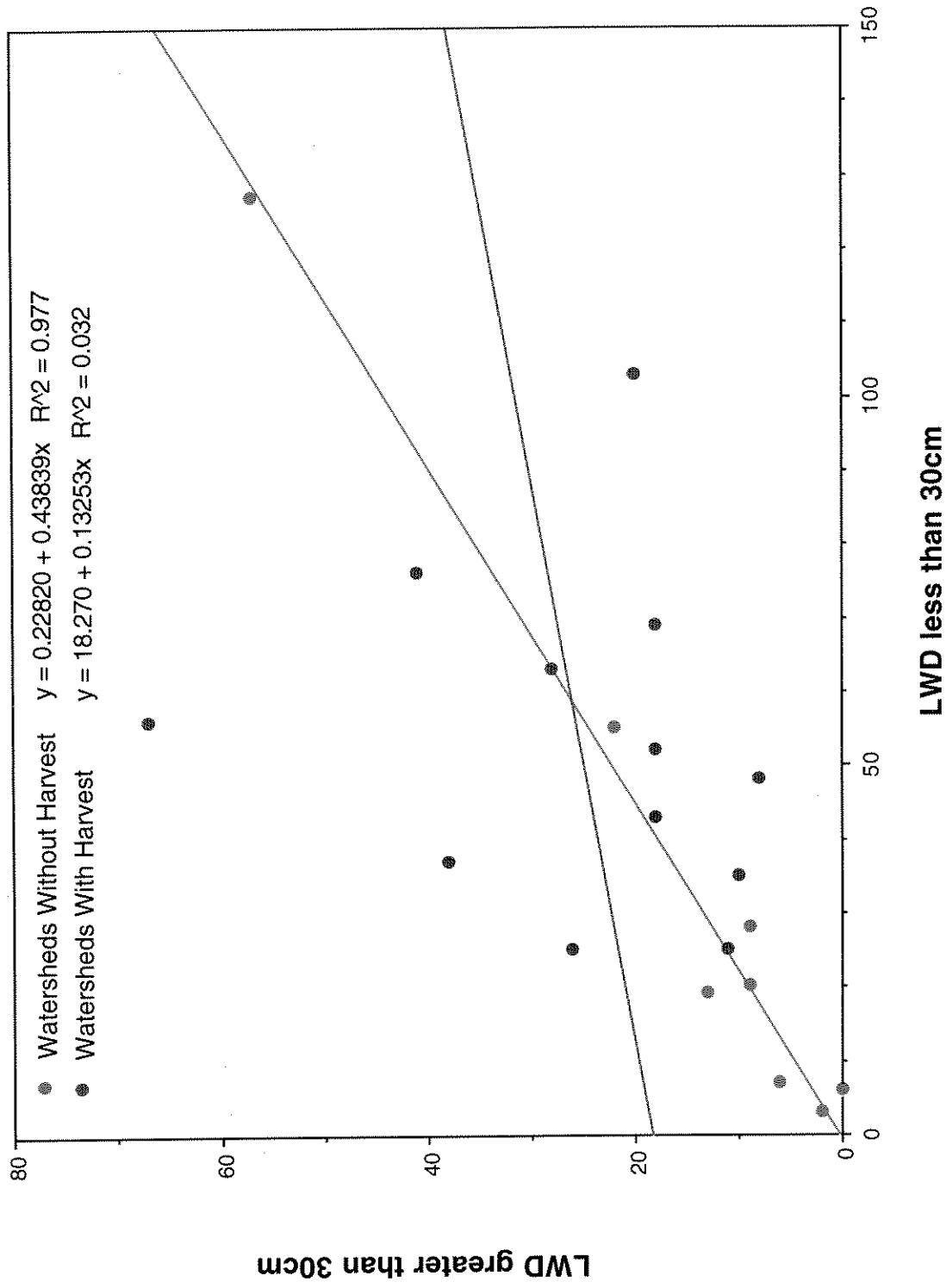


Figure 7. The frequency of large diameter ( $>30$  cm) vs. the frequency of small diameter ( $< 30$  cm) Large Woody Debris among study stream reaches in watersheds without harvest (red) and in watersheds with harvest (blue).

were among reaches with extensive riparian zone harvest (i.e., had more large diameter LWD than predicted among unharvested watershed reaches). The highest value as well as highest ratio of large to small LWD (67:56) occurred in Red Meadow Creek (Reach B) where the riparian forest had been clearcut approximately 20 years previous.

Although it would require additional, very focused study to determine the cause and effect relationship of what might lead to increased large wood input into reaches associated with riparian harvest (as well as detailed investigation into the specific history of each riparian cutting unit), the relationship may be driven by either direct or indirect harvest activities. Regardless of whether these are direct actions, (e.g., direct cutting of large diameter trees), that result in LWD input to the stream rather than removed from the site, or indirect forces (e.g., post harvest blowdown) they both result in departures from natural relationships.

We also examined the relationship of attachment of LWD to the stream bank among reaches in unharvested watersheds Vs watersheds with harvest. Again we found that among watersheds without harvest there was a relatively close relationship ( $r^2 = 0.875$ ) between the frequency of attached vs. unattached LWD and a highly scattered relationship among watersheds with harvest (Figure 8). It is not clear what driving mechanisms may be leading to these relationships; however, within this same comparative structure we examined the relationship between the frequency of LWD pieces with and without rootwads. Again, among the reaches in unharvested watersheds there was a linear relationship with low variance ( $r^2 = 0.912$ ) and in contrast there was no

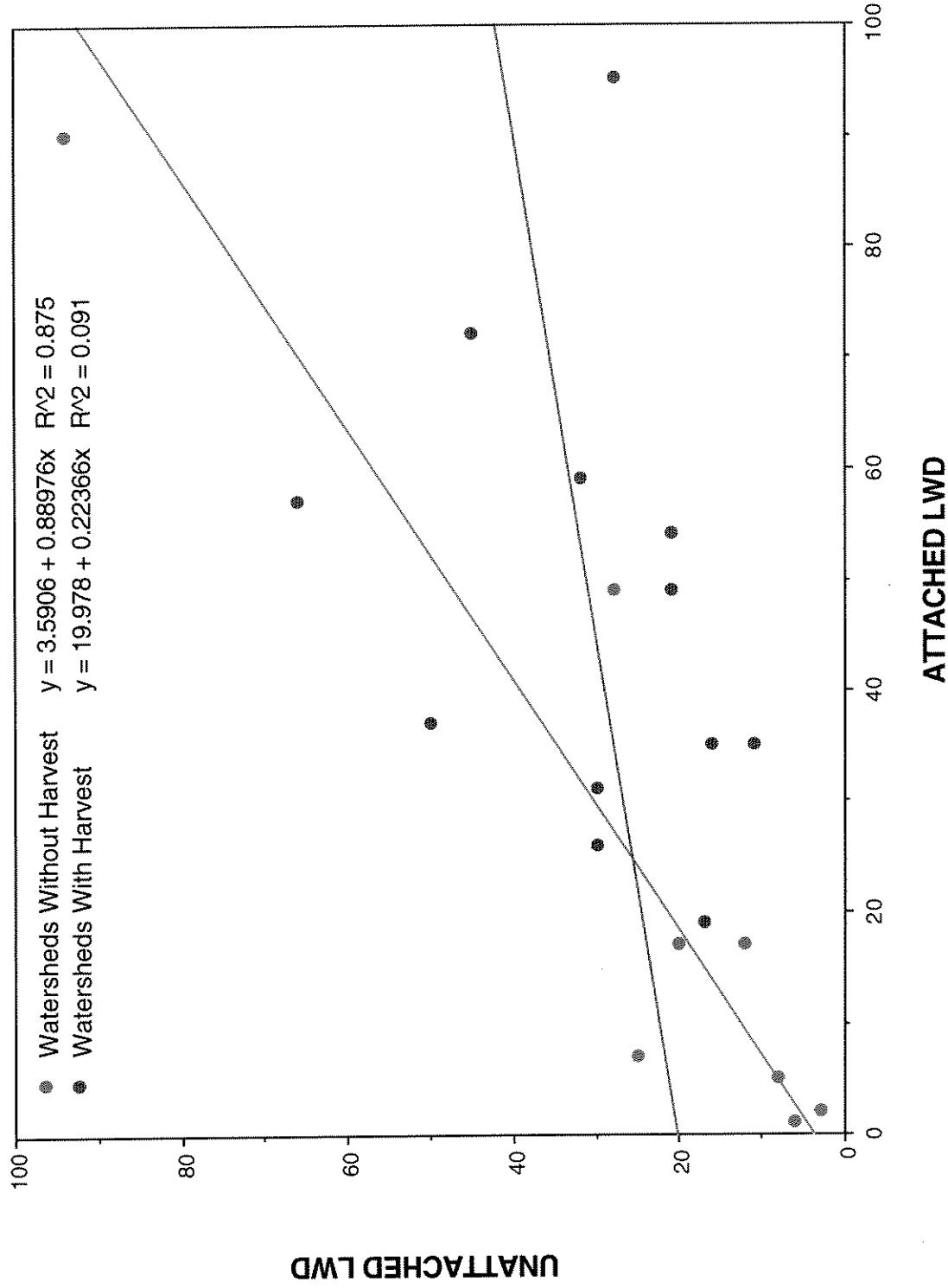


Figure 8. The frequency of attached vs. unattached Large Woody Debris among study stream reaches in watersheds without harvest (red) and in watersheds with harvest (blue).

linearity in the comparative relationship between LWD with and without rootwads among harvested watersheds (Figure 9).

We found these comparative relationships between harvested and unharvested watersheds to be quite remarkable. Although these data do not establish direct cause and effect relationships or mechanisms, they do illustrate an increased variance and loss of continuity among reaches in harvested watersheds.

#### *Implications for Watershed and Streamside Management*

We found that pool frequency and pool depth to stream width ratio increased with higher LWD abundance. We also found that pool frequency and depth were significantly related to large pieces of LWD that were oriented either perpendicular or at least at a 45° angle to the thalweg. This suggests that large, stable pieces within the bankfull stream channel are the primary influence promoting pool formation. In addition to large individual pieces, aggregates were also important structures adding to bedform and channel complexity. Many LWD pieces were oriented parallel to the thalweg and thus were generally much less interactive with the pool-forming stream flows. Thus, position, orientation and stability of a few pieces was more important than simply LWD frequency or volume. Grette (1985) and Richmond and Fausch (1995) also reported a significant positive relationship between LWD and the abundance of pools as well as the importance of relatively few, stable LWD pieces that accounted for most of the pool formation.

Wohl et al. (1993) reported that stream depth and gradient (stream power) and the resistance of bed and bank materials to erosion were important determinants of pool size. We observed a similar relationship

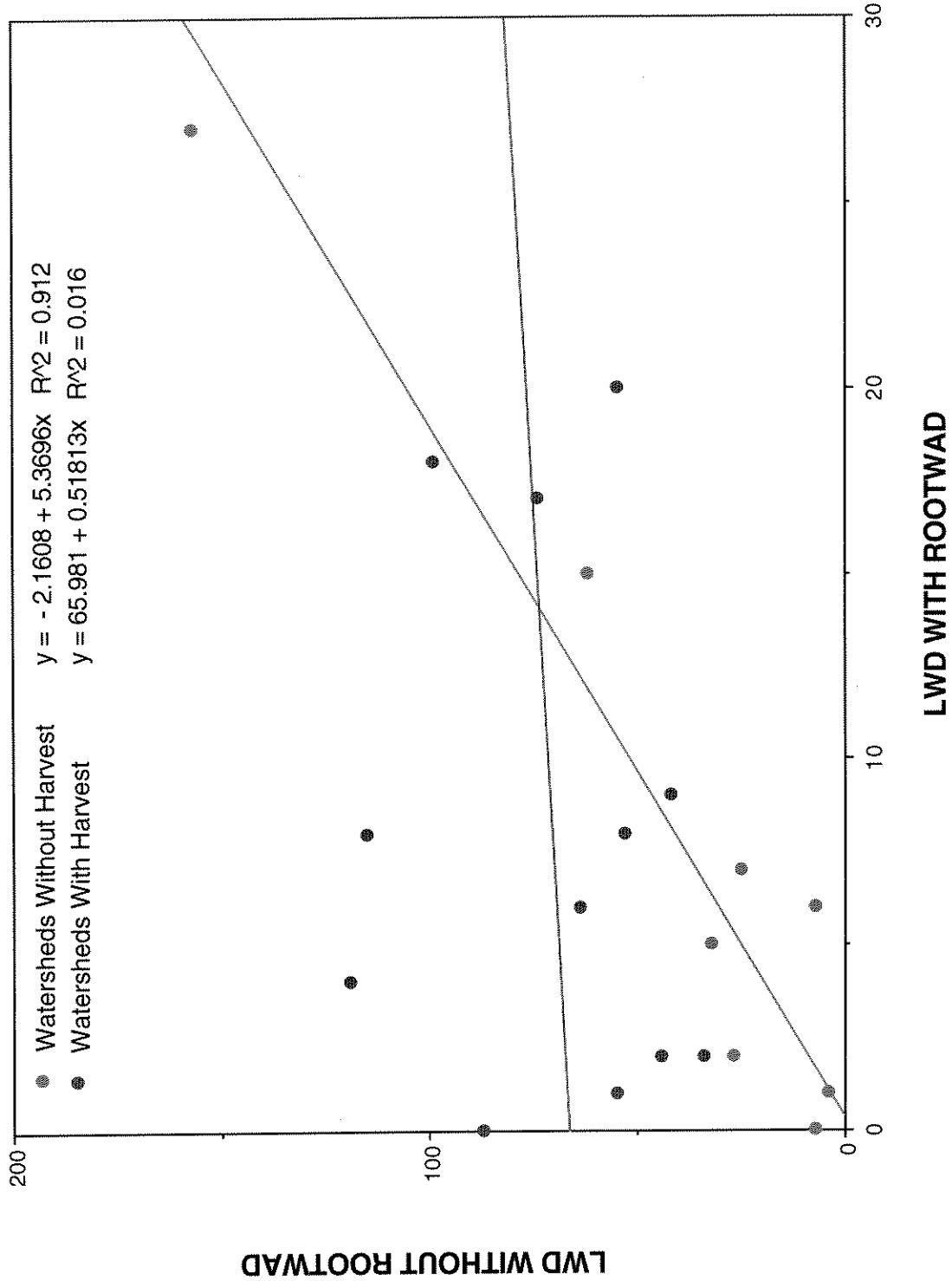


Figure 9. The frequency of Large Woody Debris with rootwad vs. without rootwad among study stream reaches in watersheds without harvest (red) and in watersheds with harvest (blue).

and with scour pools around aggregates in the largest streams (e.g., Young's Creek, Coal Creek).

LWD is an essential component in forming pools and overhead cover for fish. However, the relationship between stream size and power and the position and role played by LWD in the modification of bedform and channel development is a changing one. It is apparent from this study that large diameter, shorter pieces of LWD have a higher frequency of perpendicular orientation and thus a greater degree of pool forming interaction with stream flows. Likewise, as the stream increases in size there is increased requirement that LWD be associated with an aggregate to remain stable and interactive with the channel. Thus, the structure and function of LWD is largely determined by the interaction of piece diameter, length and position and the characteristics of the watershed and stream. These variables, in undisturbed stream systems, tend to be relatively linear in comparative relationships; however, become fairly unpredictable in streams that have been influenced by harvest. A detailed investigation into the specifics of various cutting histories would be necessary to determine how site prescriptions may affect the outcome of LWD to stream relationships.

The implications of this study for forest managers are twofold: 1) that with harvest comes increased unpredictability in the frequency of size, attachment, and stability of the LWD and 2) riparian zones without harvest may be essential to long term maintenance of natural stream morphology and habitat features. These issues will be critical for land managers attempting to prevent future detrimental environmental change or setting restoration goals for degraded bull trout spawning streams (c.f. Reeves et al. 1991).

(Figure 3) in which the streams of the larger drainages had the deepest pools, even though there was no significant difference in depth of riffles (i.e., minimum thalweg depths) between drainages. Other researchers have suggested that large streams and associated large river characteristics of gradient, stream power, maximum stream width, and maximum bankfull depth override the influence of channel modifying LWD (Andrus et al. 1988; Evans et al 1993). Our results support this suggestion since within the largest watershed streams, such as Young's Creek, pool forming LWD occurred almost exclusively as aggregates. In other words, as a stream get larger, in our study exemplified by Young's Creek, stream power, maximum stream width, and maximum bankfull depth override a threshold that is interactive with the maximum size of the riparian trees. Thus, large LWD along the coastal mountain streams of Washington and Oregon can remain interactive with the channel and pool forming in larger stream reaches than the large LWD in northern Rocky Mountain streams.

Robison and Bestcha (1990) and Richmond and Fausch (1995) showed that changing relationships between LWD and stream flow influenced pool types and that the majority of pools were formed by LWD spanning the channel perpendicular to flow. Richmond and Fausch (1995) found plunge and dammed pools to be the most prevalent pool type in the small subalpine streams of Colorado. Bilby and Ward (1989) found a similar pool types in smaller streams (<7m width) in southwestern Washington, but mainly scour pools in large streams (Bilby and Ward 1991). We found similar relationship among streams in the Flathead Basin where pools in the smaller streams (e.g., Goat Creek, Red Meadow Creek) were primarily associated with plunging or dammed water around LWD

and with scour pools around aggregates in the largest streams (e.g., Young's Creek, Coal Creek).

LWD is an essential component in forming pools and overhead cover for fish. However, the relationship between stream size and power and the position and role played by LWD in the modification of bedform and channel development is a changing one. It is apparent from this study that large diameter, shorter pieces of LWD have a higher frequency of perpendicular orientation and thus a greater degree of pool forming interaction with stream flows. Likewise, as the stream increases in size there is increased requirement that LWD be associated with an aggregate to remain stable and interactive with the channel. Thus, the structure and function of LWD is largely determined by the interaction of piece diameter, length and position and the characteristics of the watershed and stream. In undisturbed stream systems, these variables tend to be relatively linear, but become fairly unpredictable in streams that have been influenced by harvest (see Figures 7, 8, and 9). A detailed investigation into the specifics of various cutting histories would be necessary to determine how site prescriptions may affect the outcome of LWD to stream relationships.

The implications of this study for forest managers are twofold: 1) that with harvest comes increased unpredictability in the frequency of size, attachment, and stability of the LWD and 2) riparian zones without harvest may be essential to long term maintenance of natural stream morphology and habitat features. These issues will be critical for land managers attempting to prevent future detrimental environmental change or setting restoration goals for degraded bull trout spawning streams (c.f. Reeves et al. 1991).

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# APPENDIX A

## LARGE WOODY DEBRIS IN BULL TROUT SPAWNING STREAMS IN NORTHWEST MONTANA

F. Richard Hauer

John T. Gangemi

and

Colden V. Baxter

Flathead Lake Biological Station

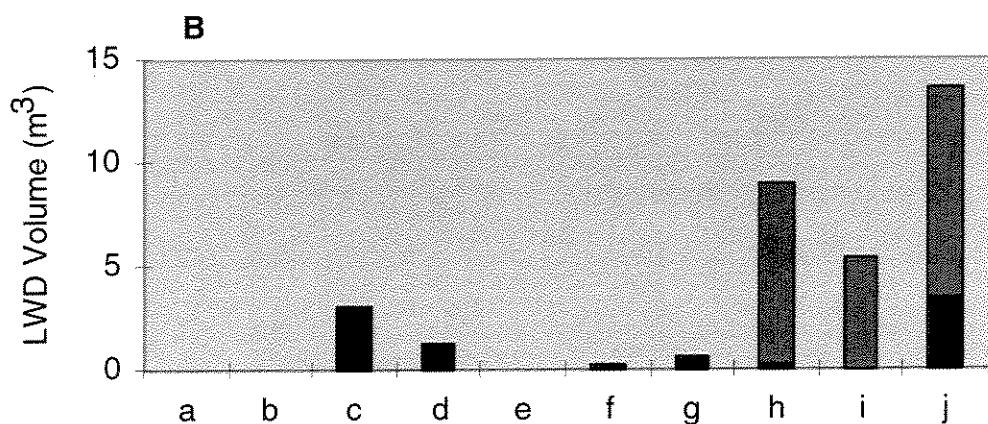
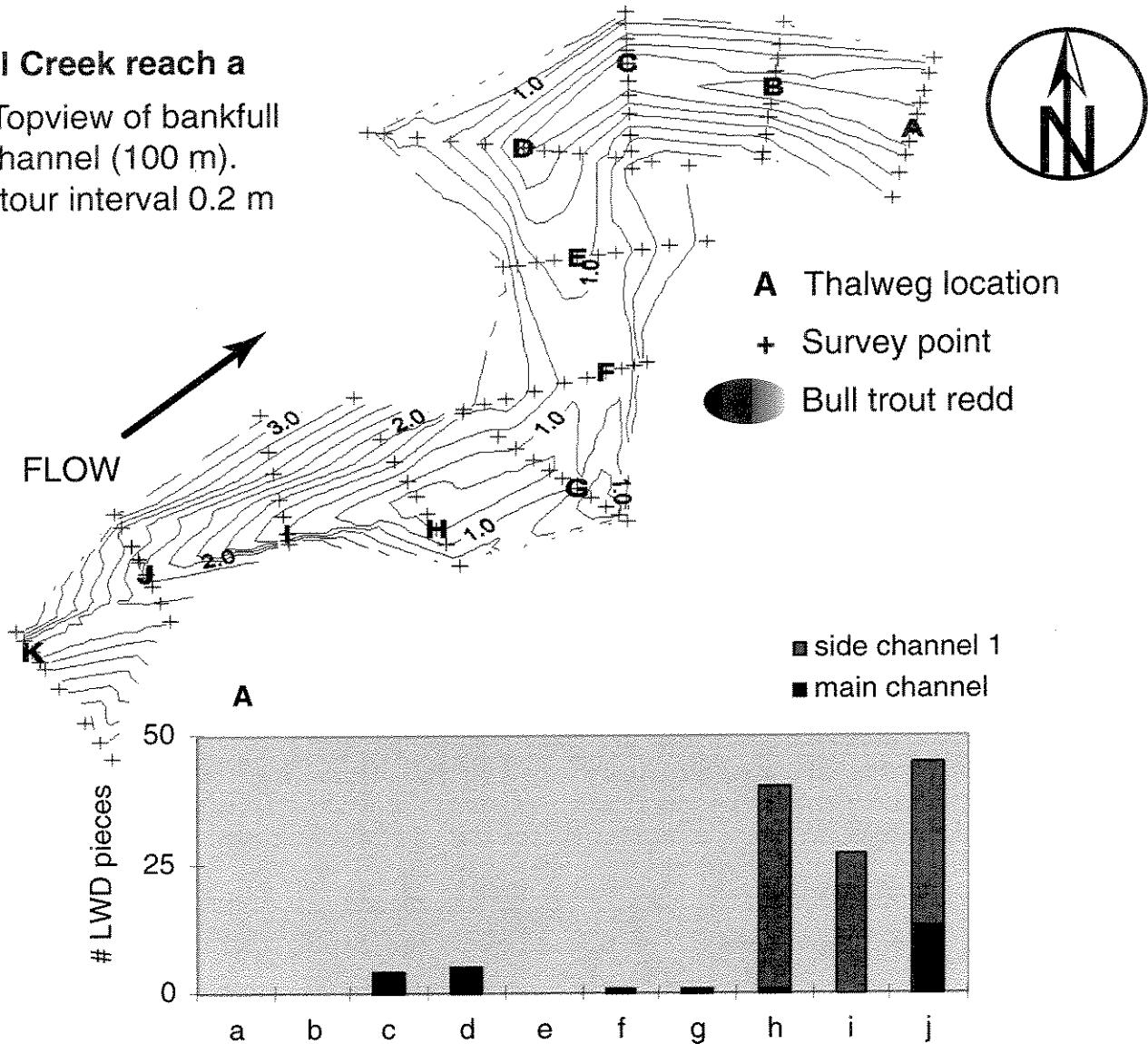
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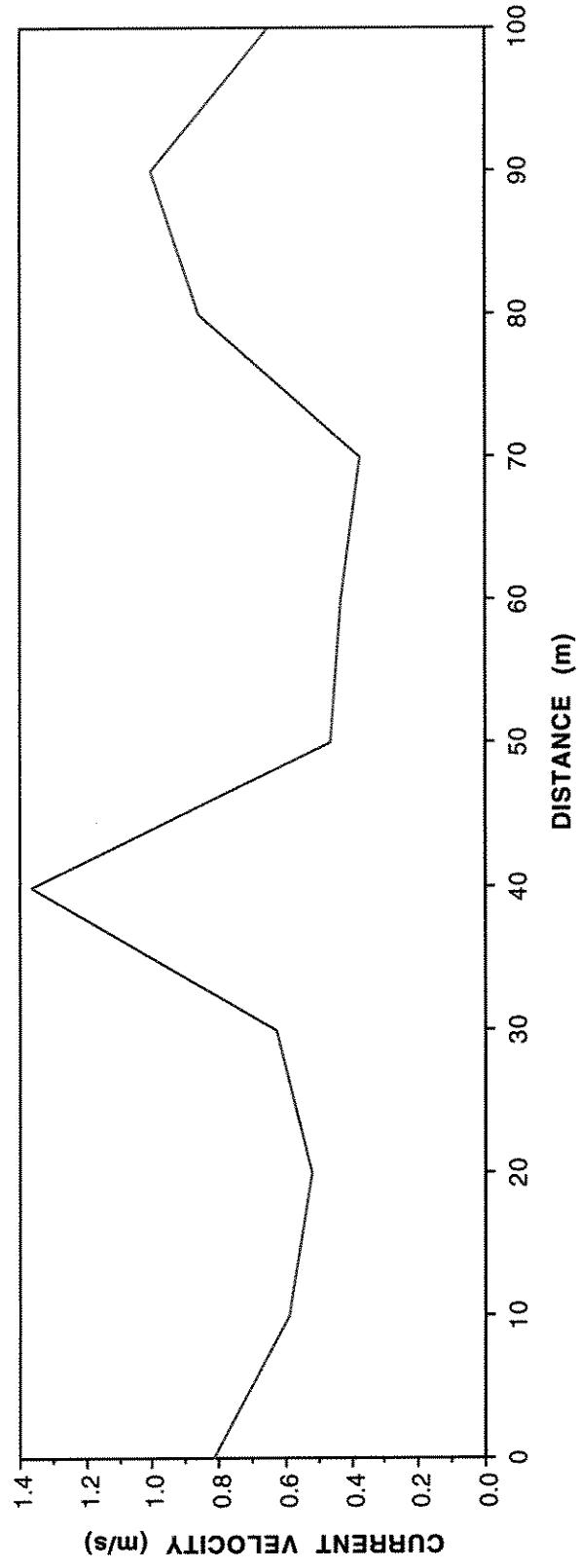
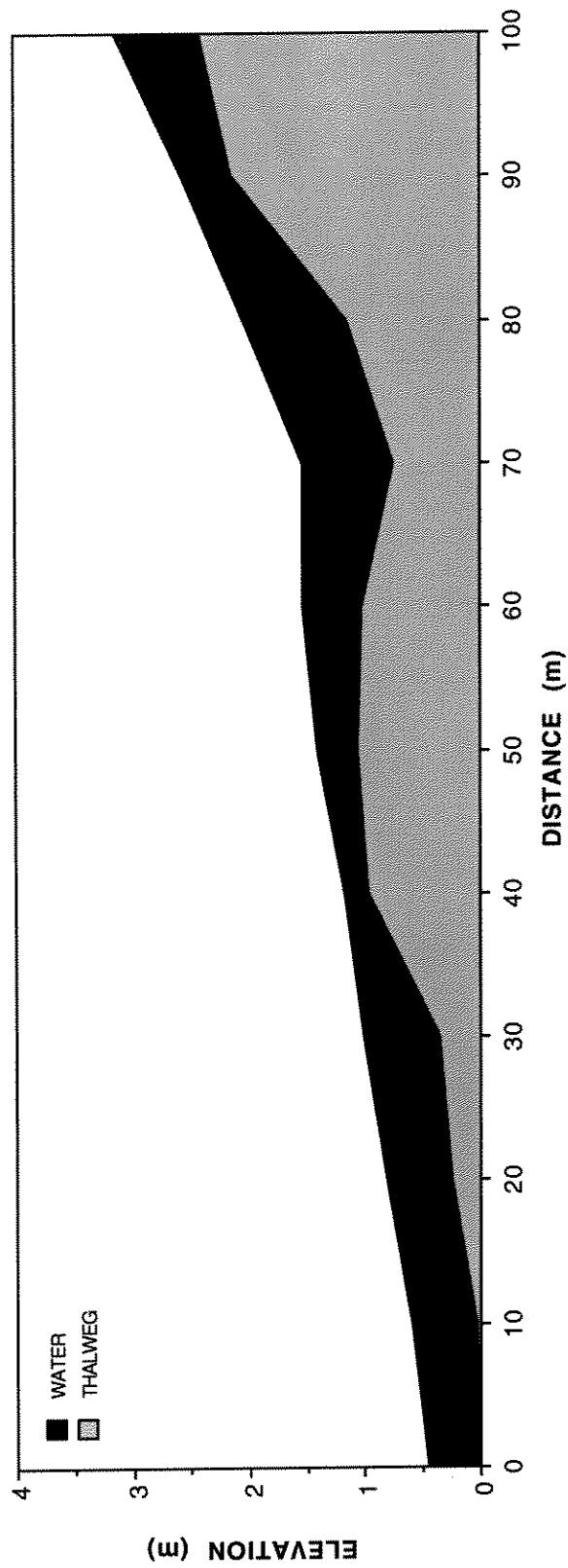
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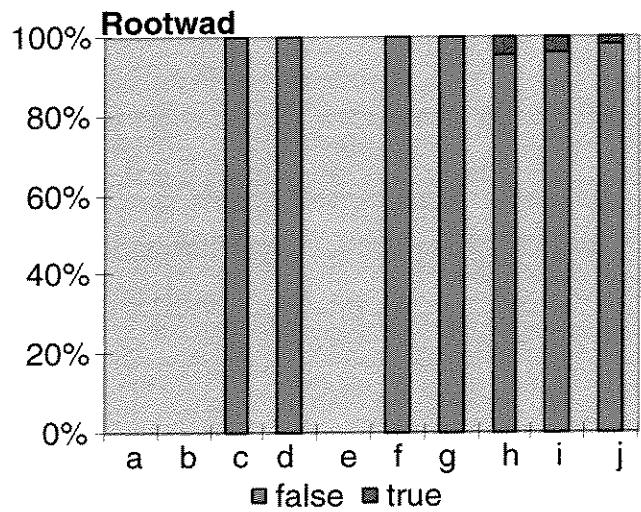
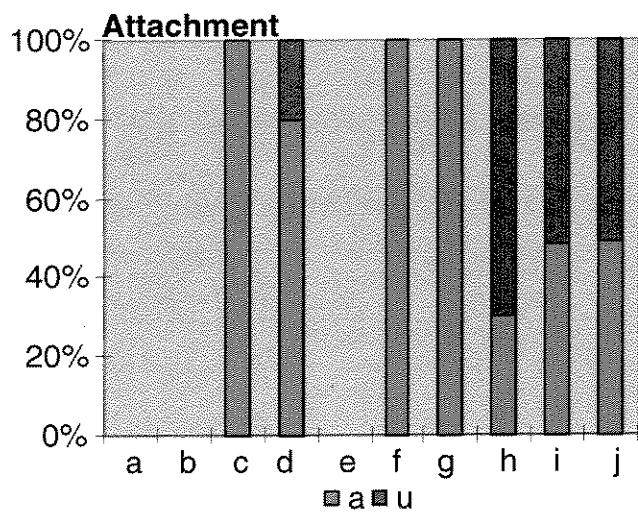
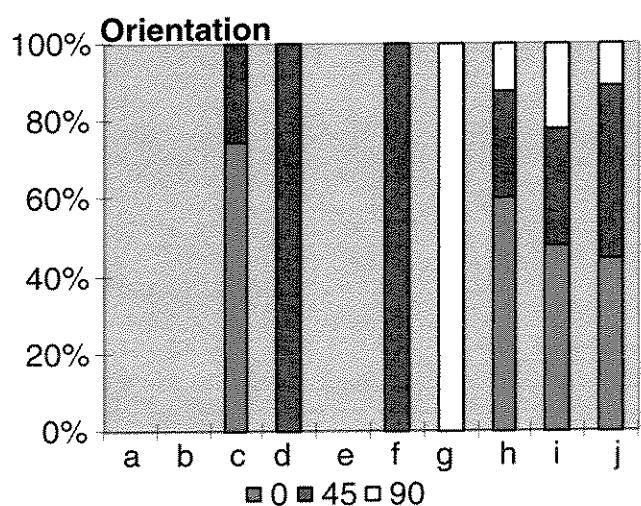
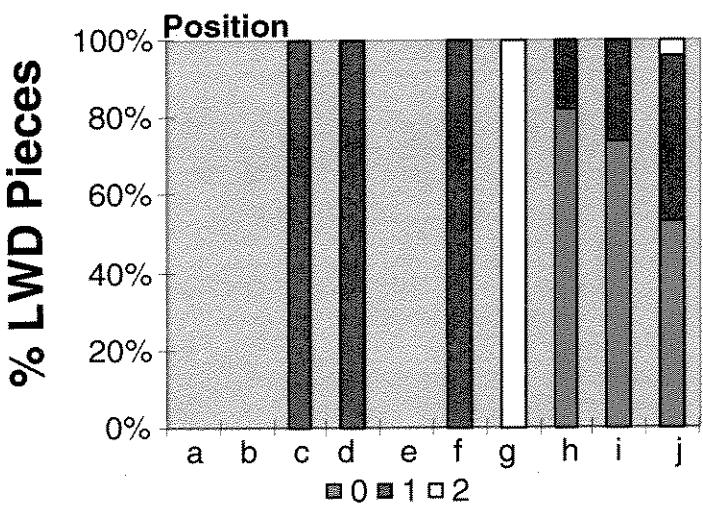
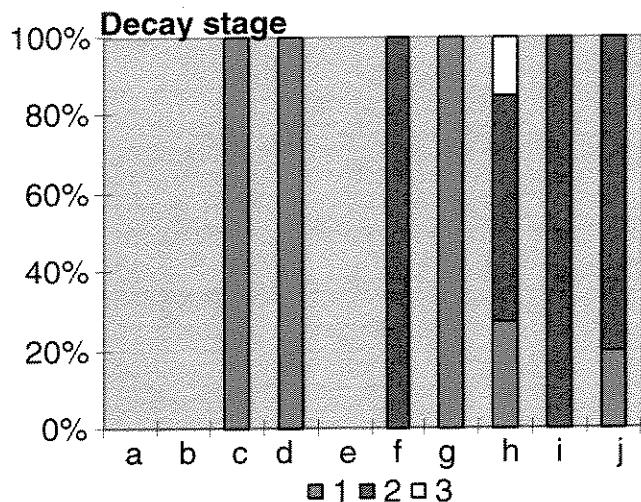
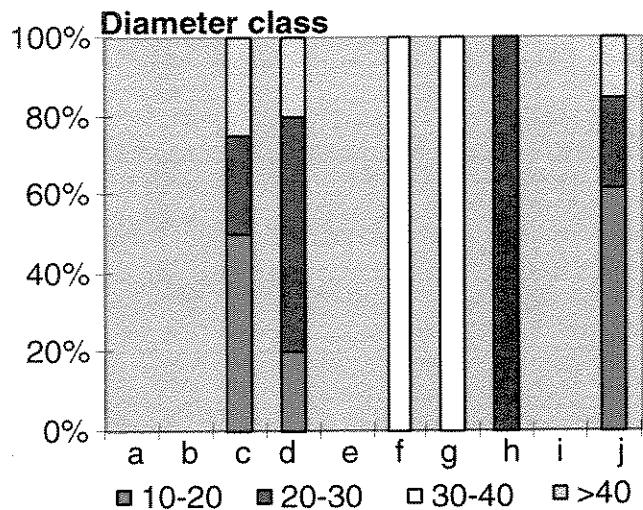
## Coal Creek reach a

A: Topview of bankfull channel (100 m).  
contour interval 0.2 m



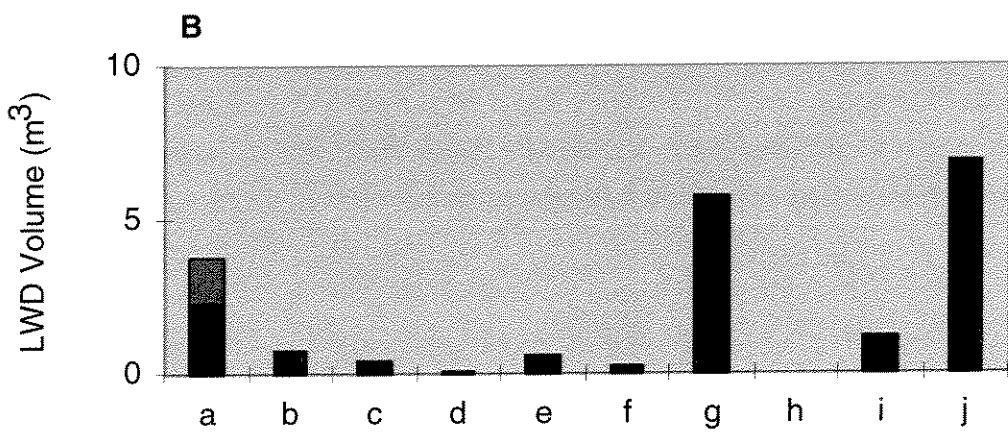
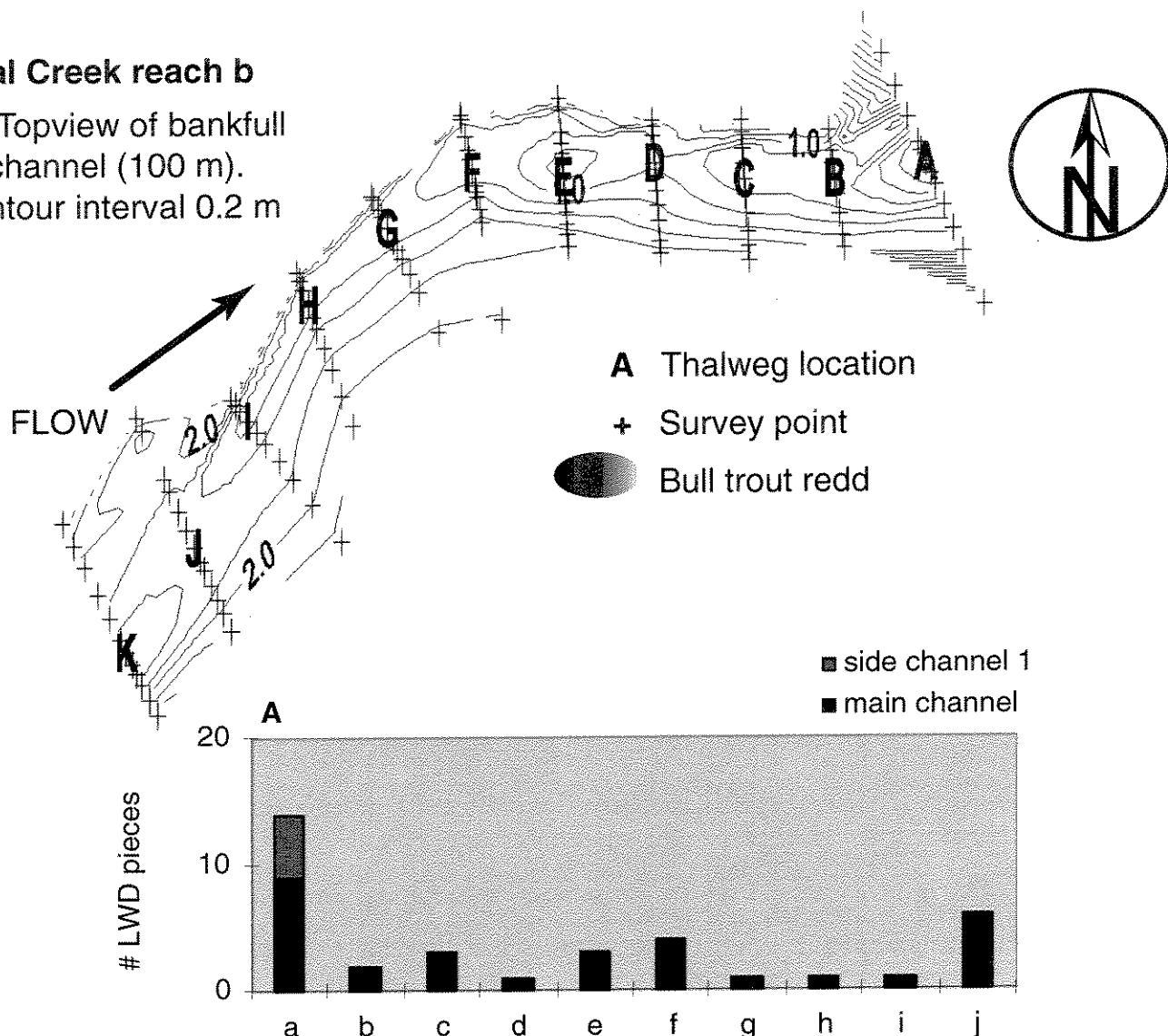
**Coal Creek Reach A**



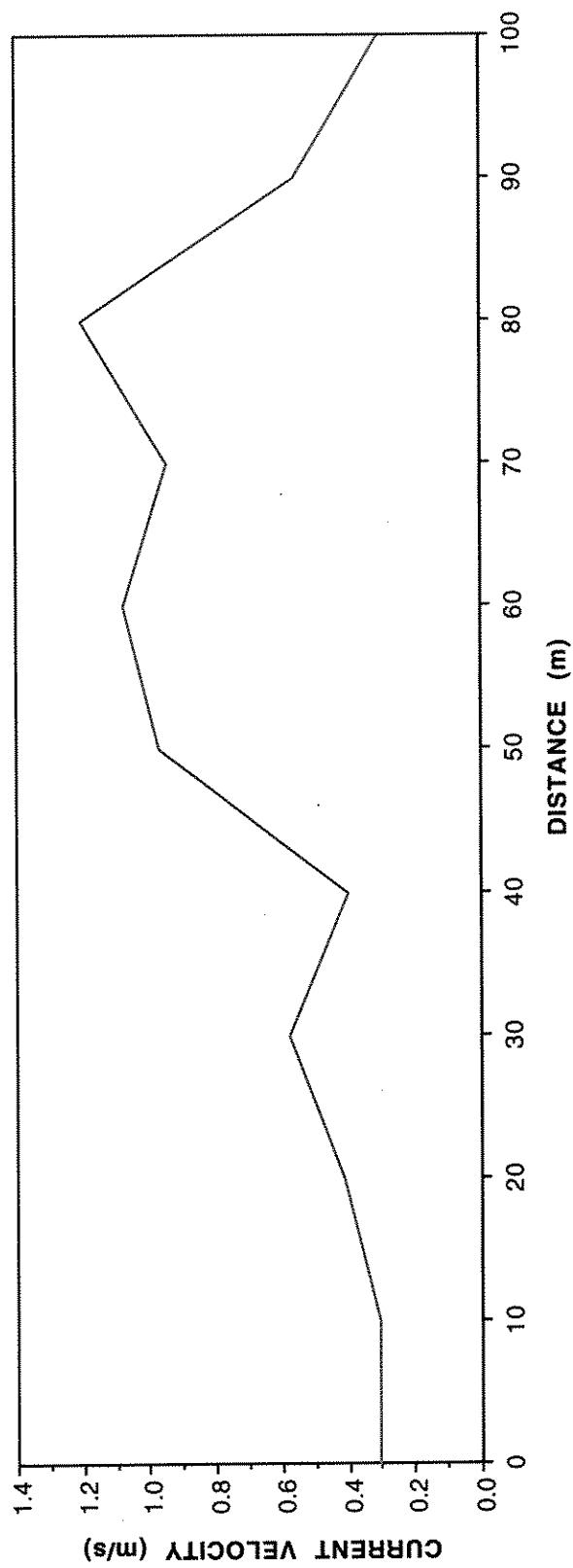
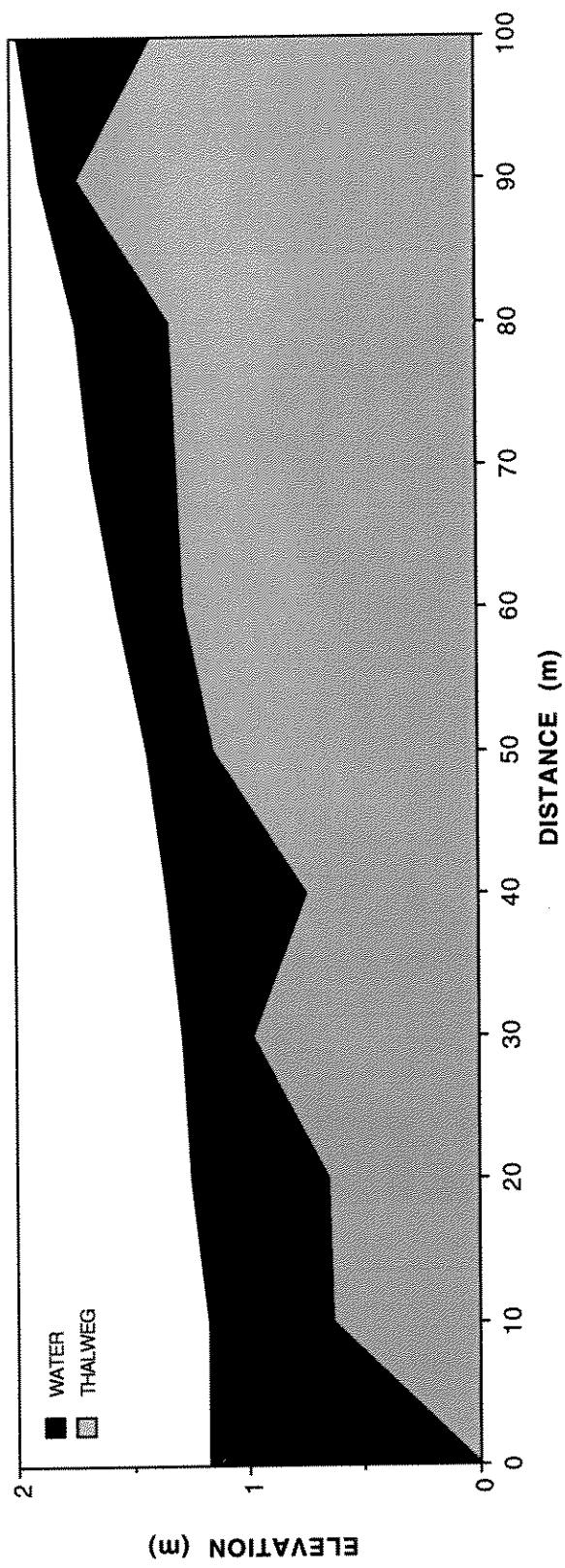


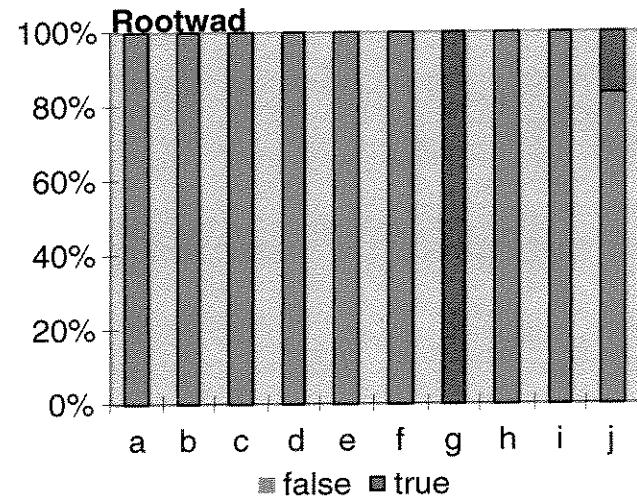
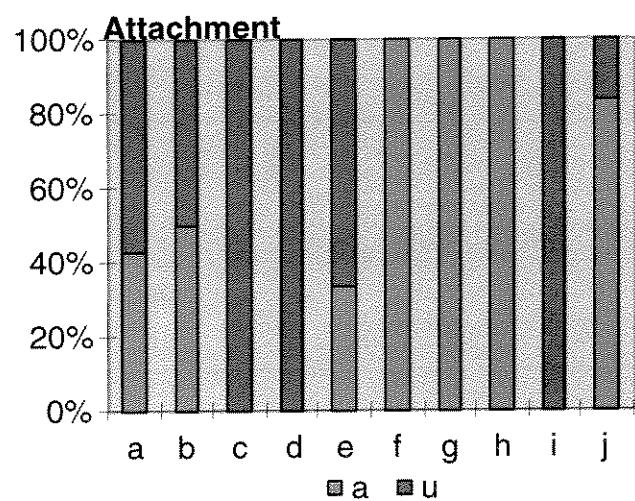
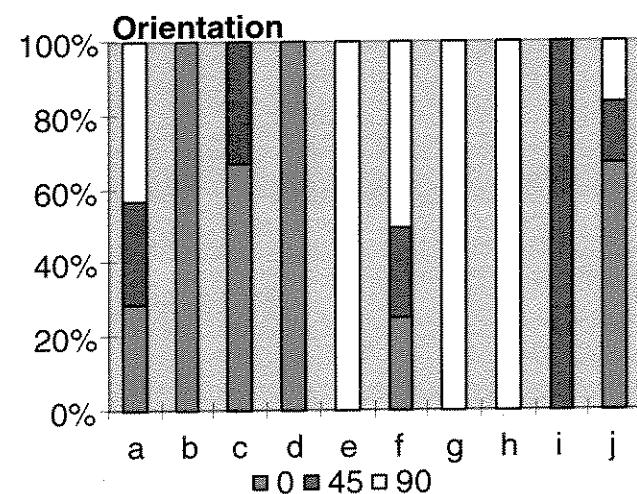
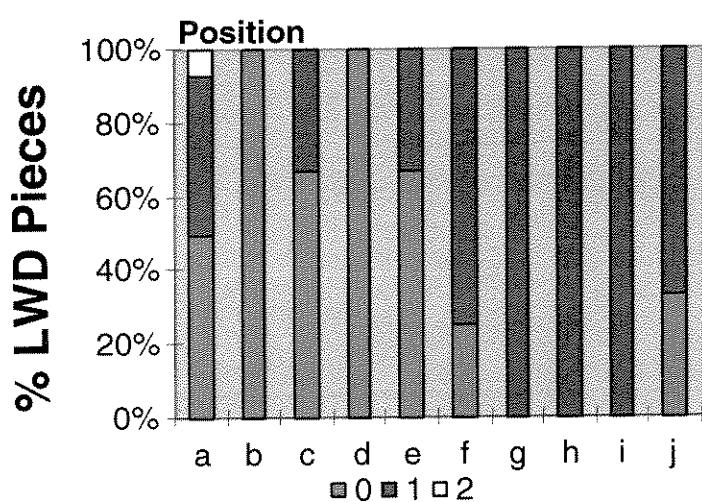
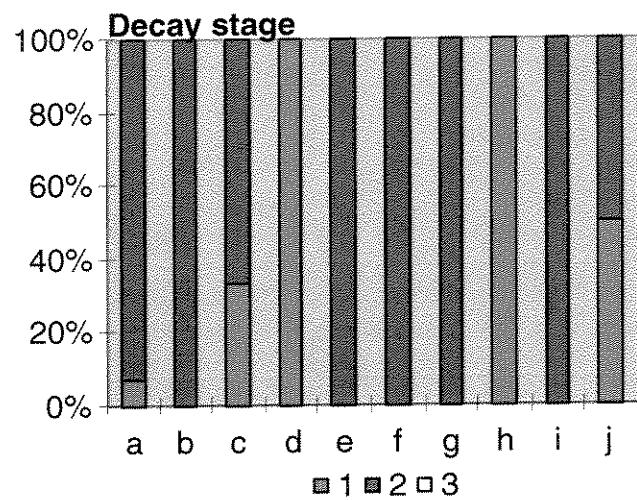
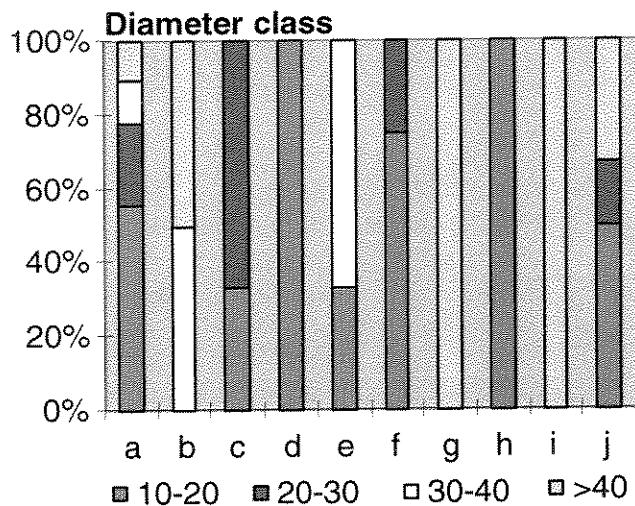
## Coal Creek reach b

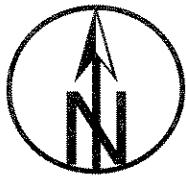
A: Topview of bankfull channel (100 m).  
contour interval 0.2 m



Coal Creek Reach C

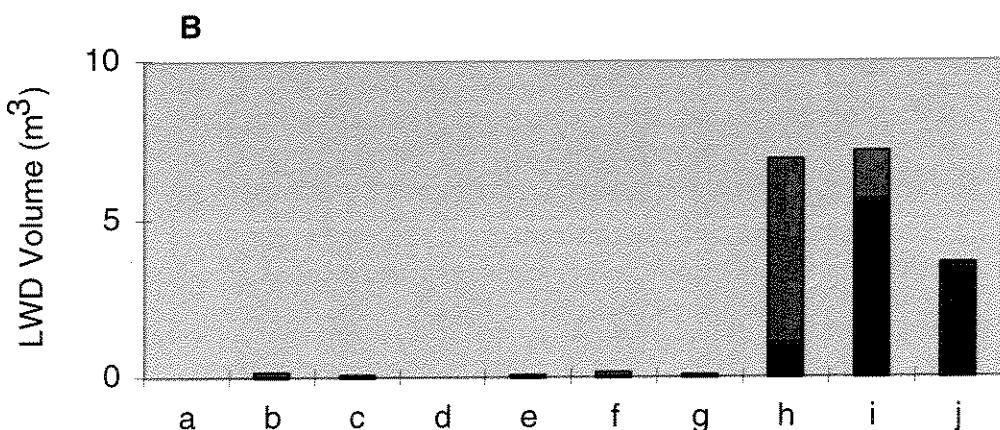
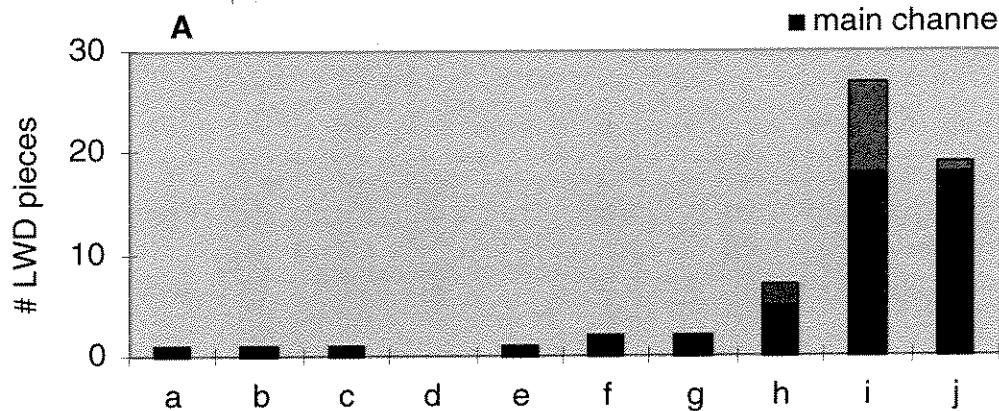
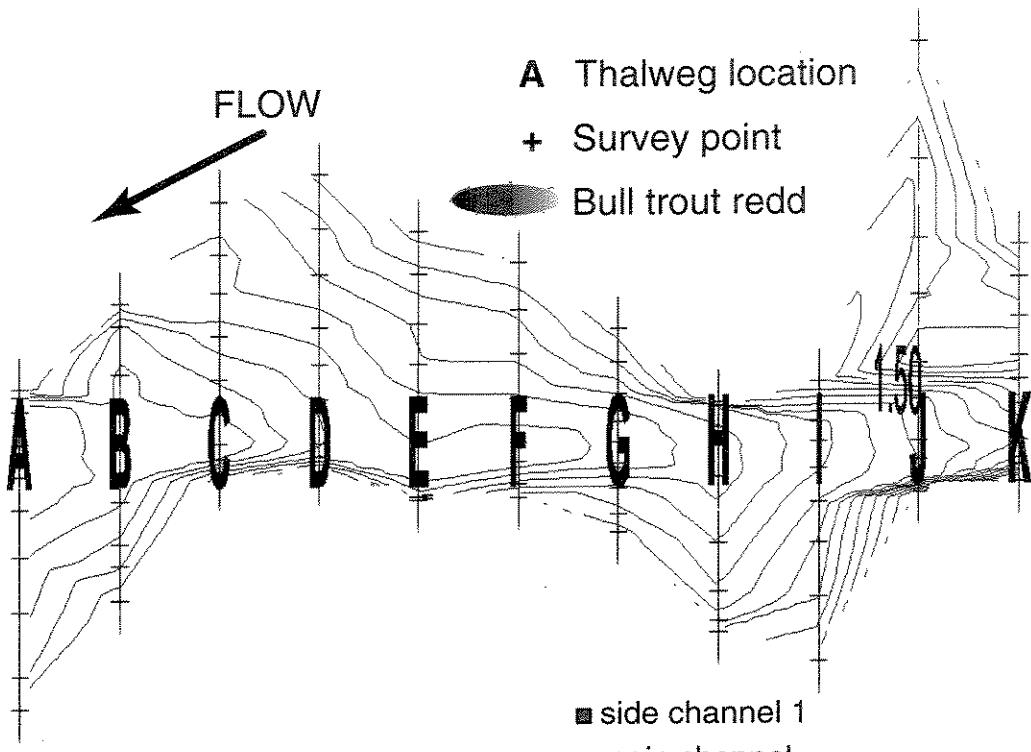




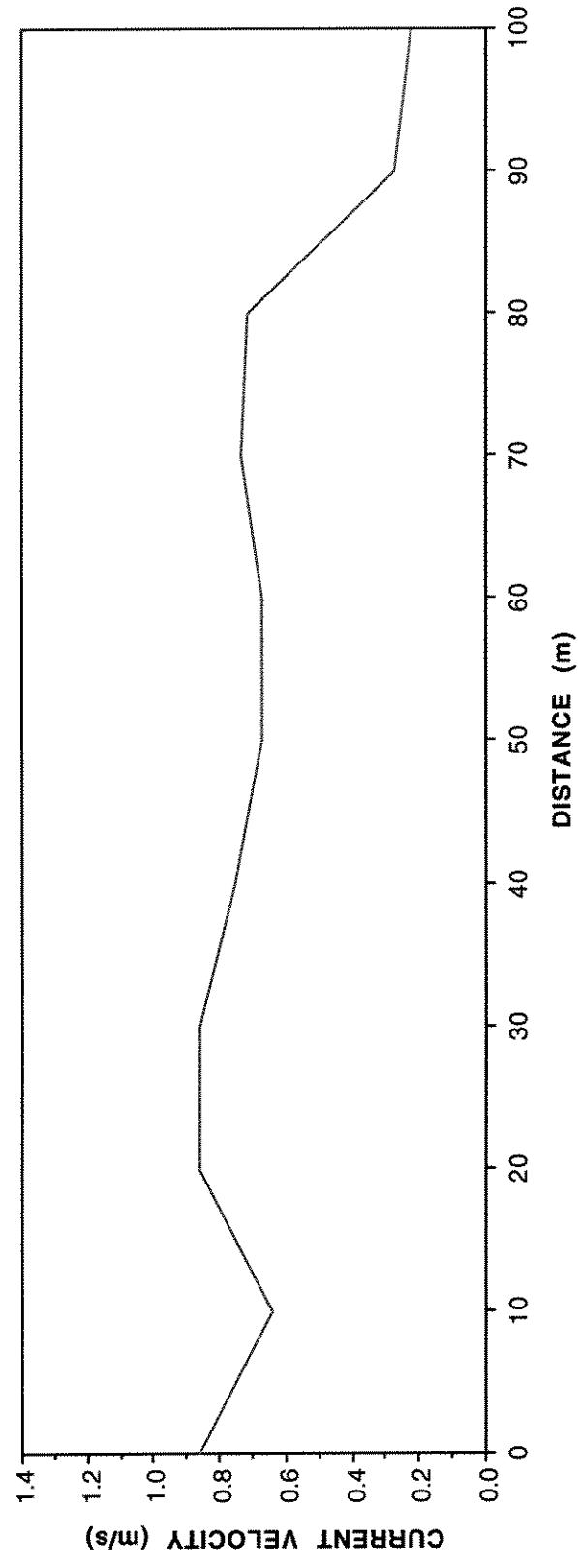
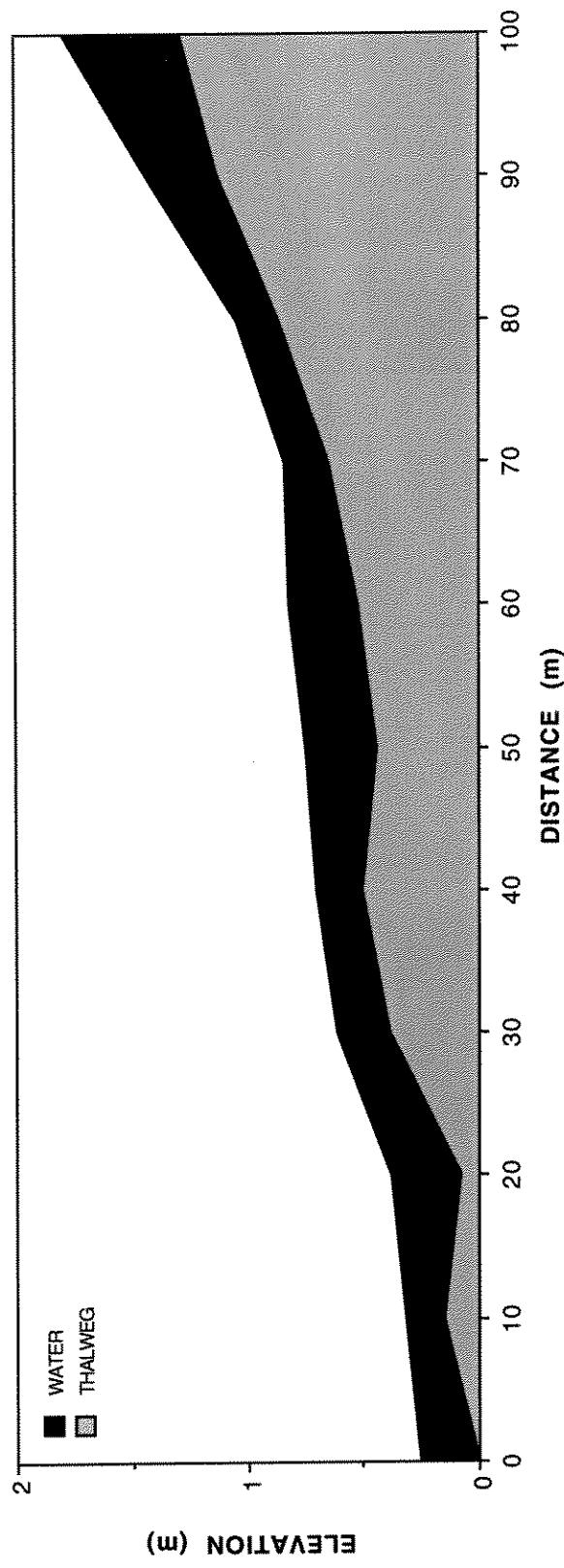


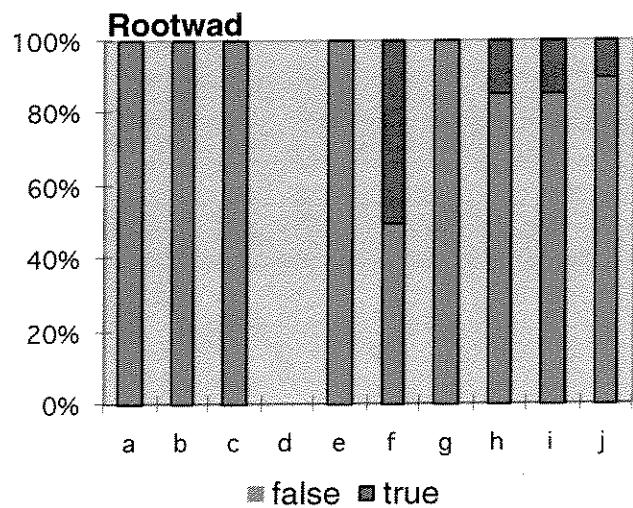
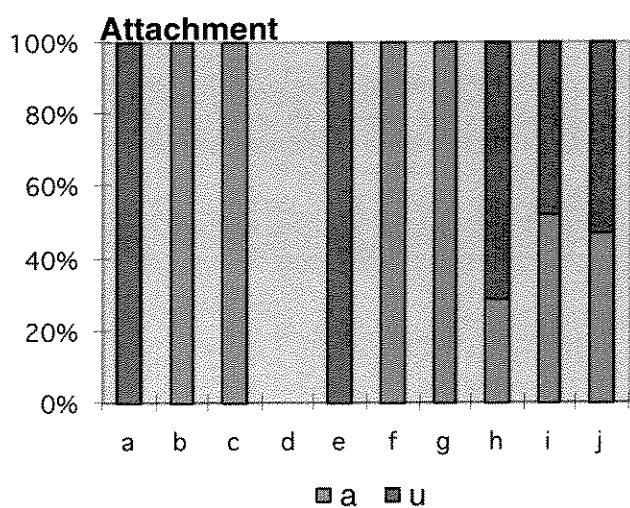
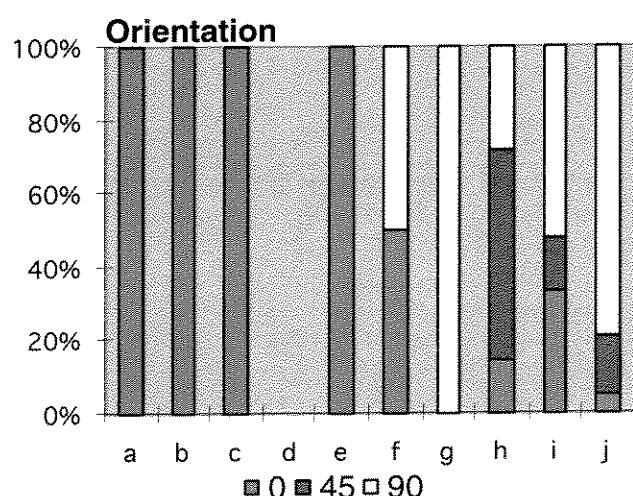
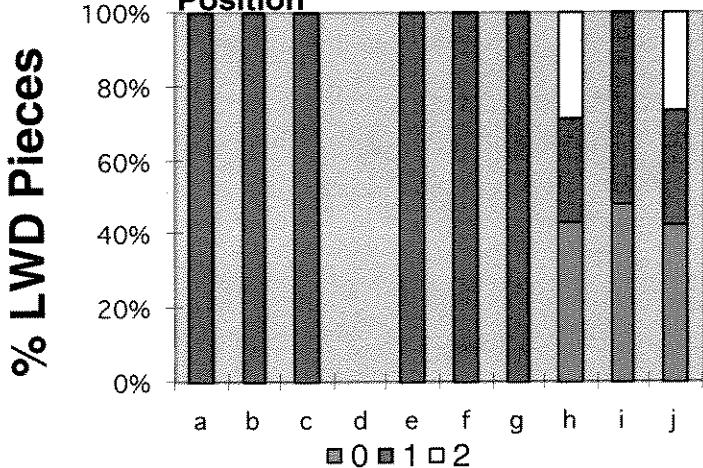
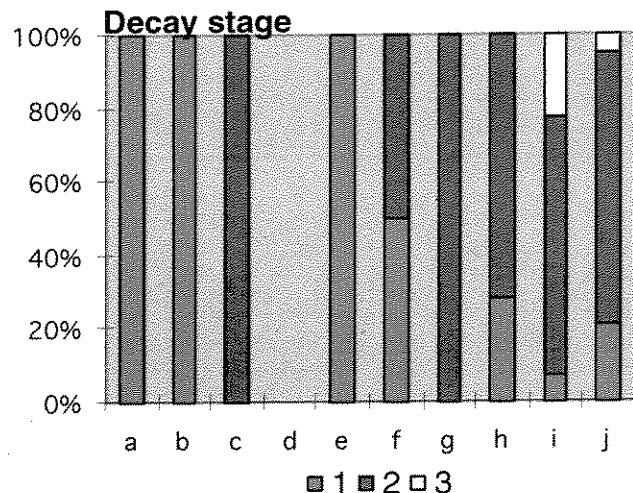
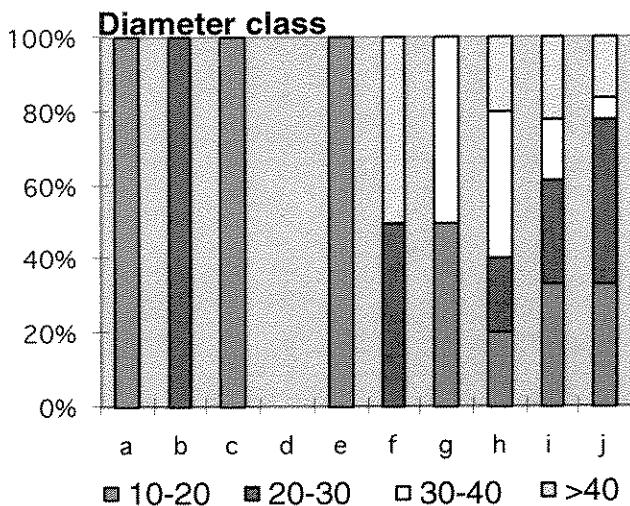
### Goat Creek reach a

A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



Goat Creek Reach A

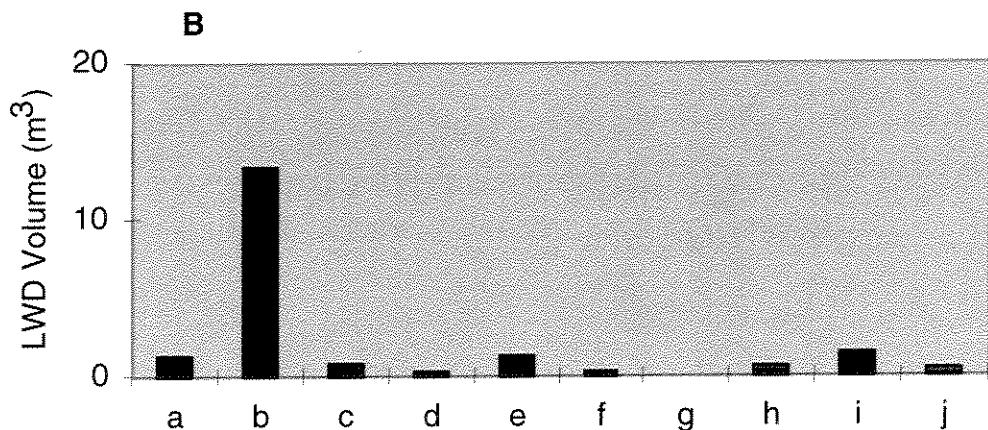
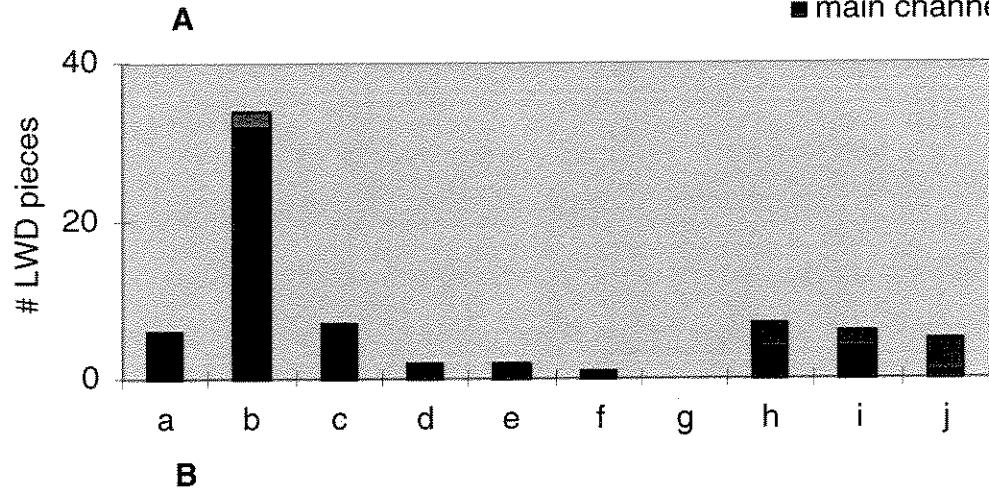
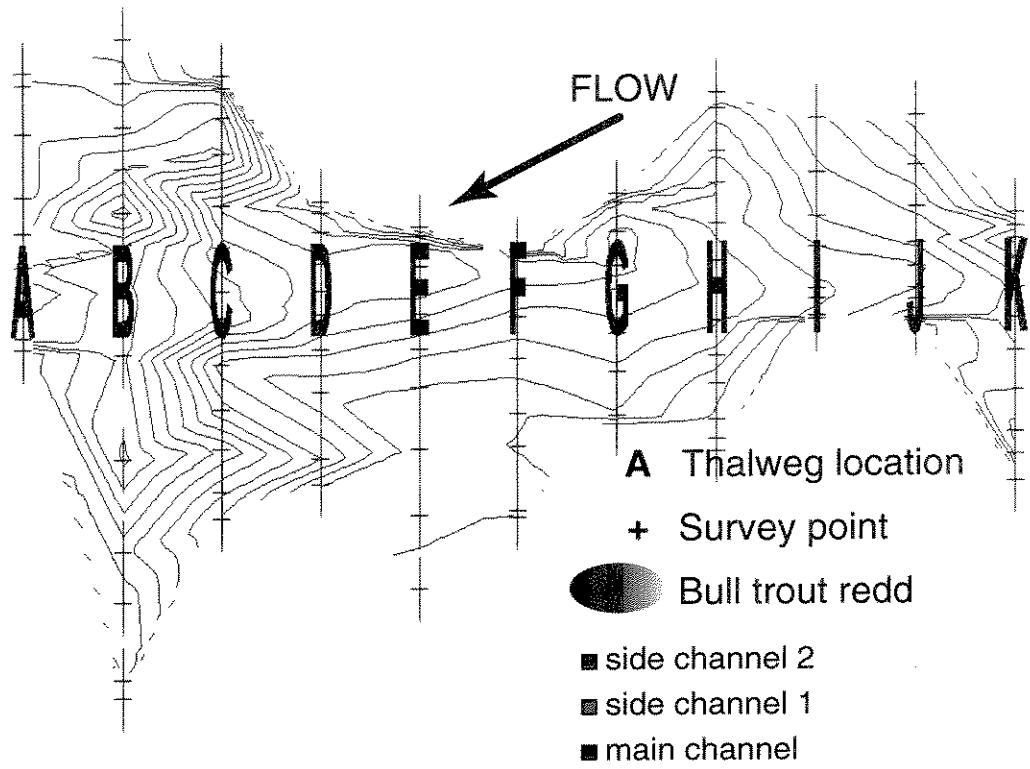




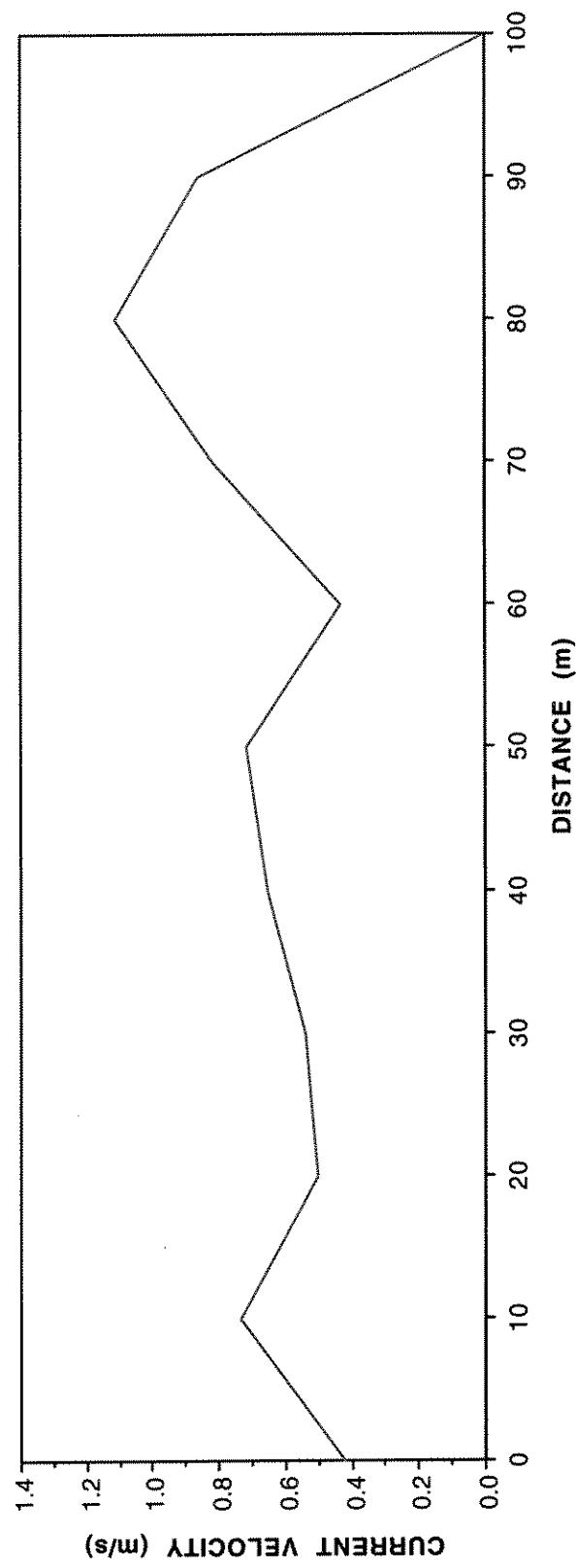
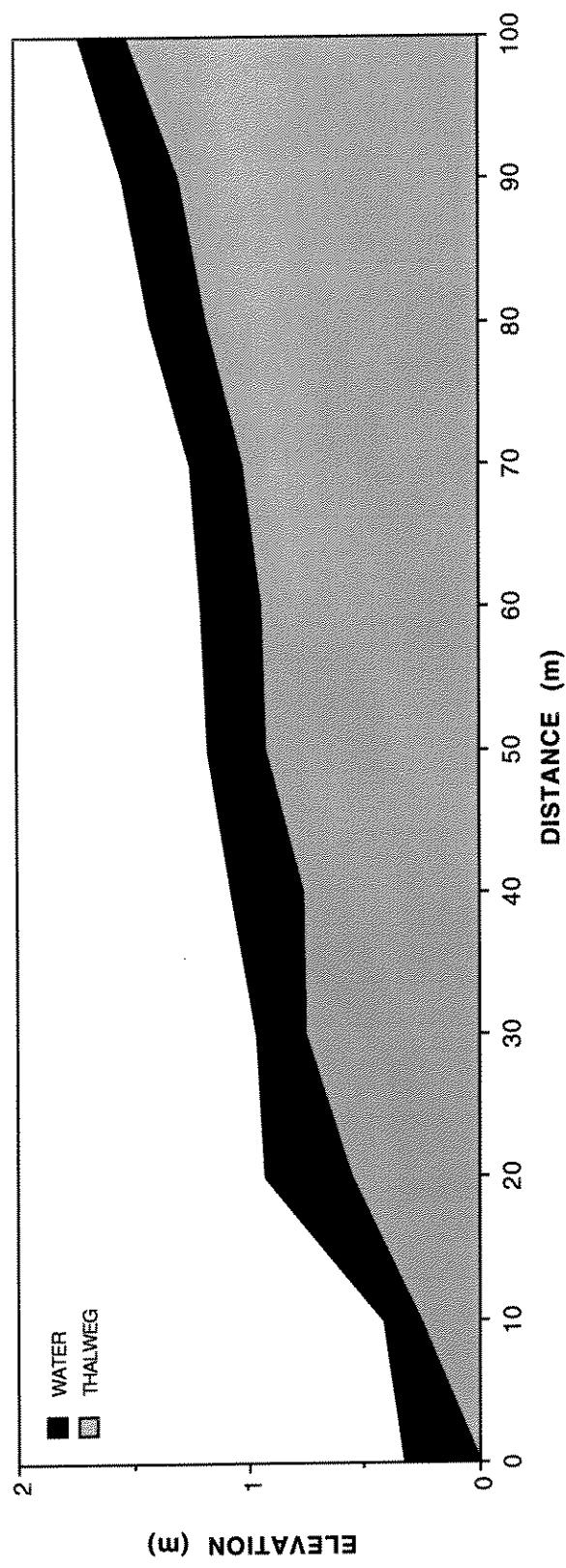


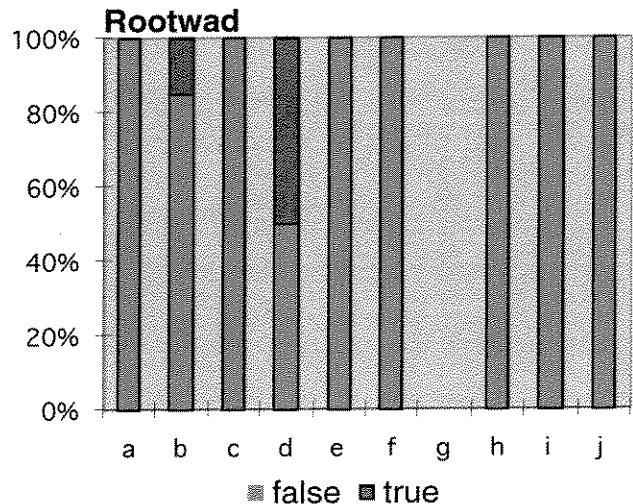
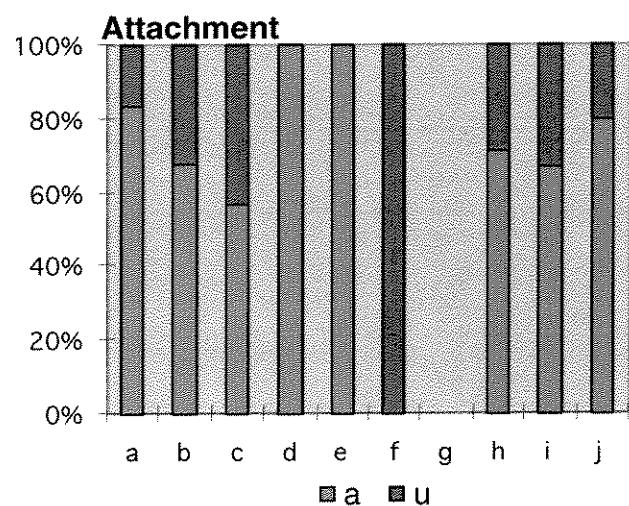
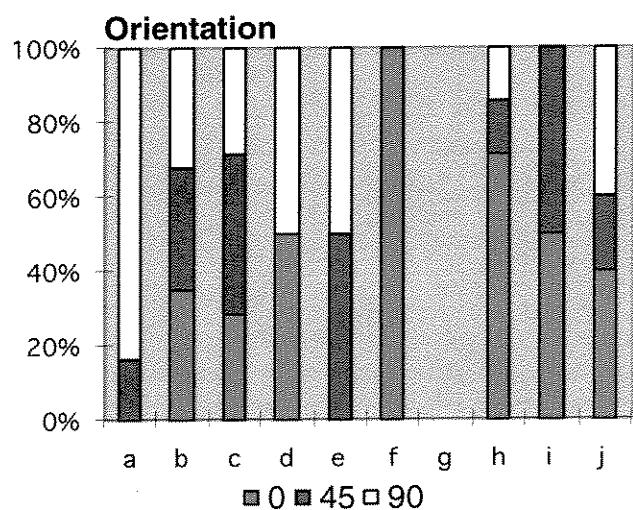
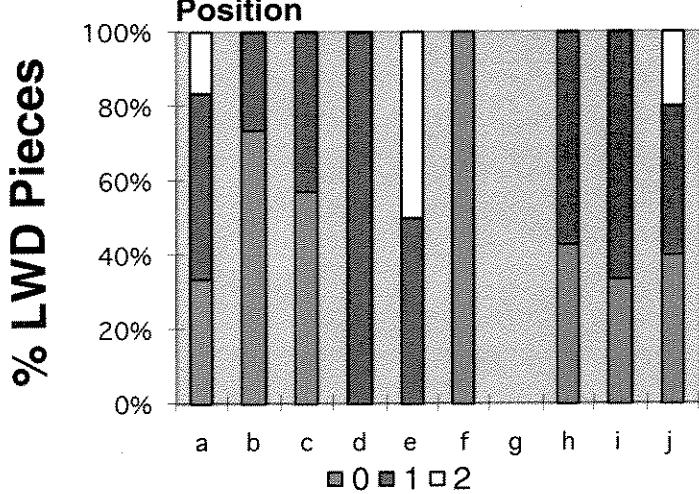
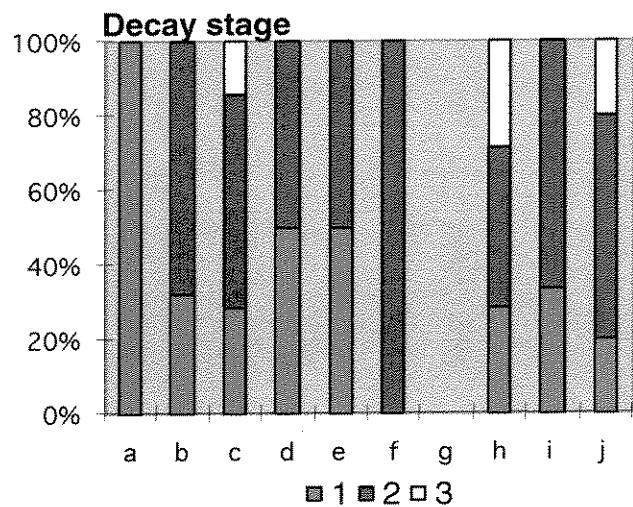
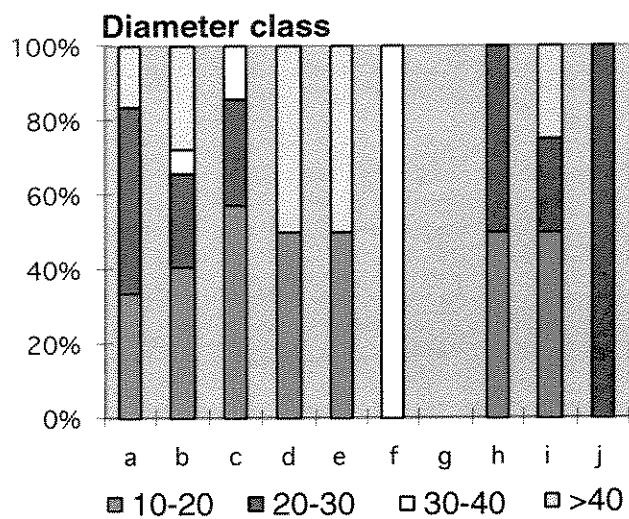
### Goat Creek reach b

A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



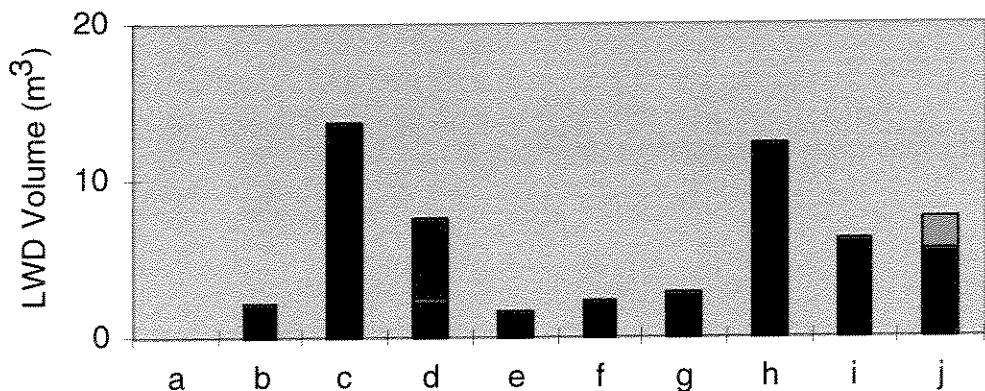
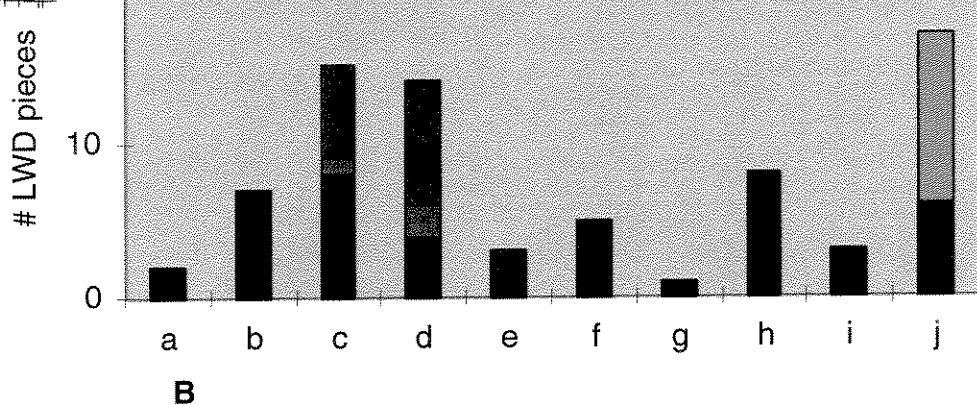
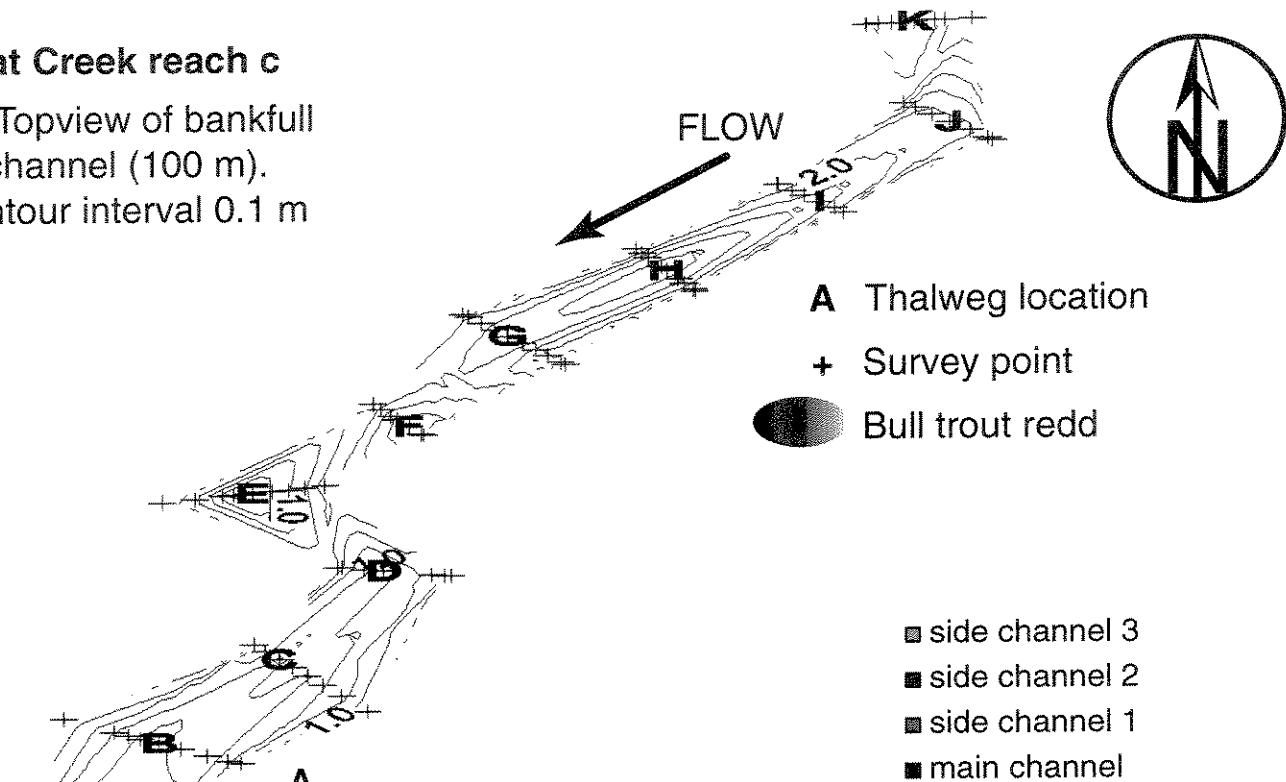
Goat Creek Reach B



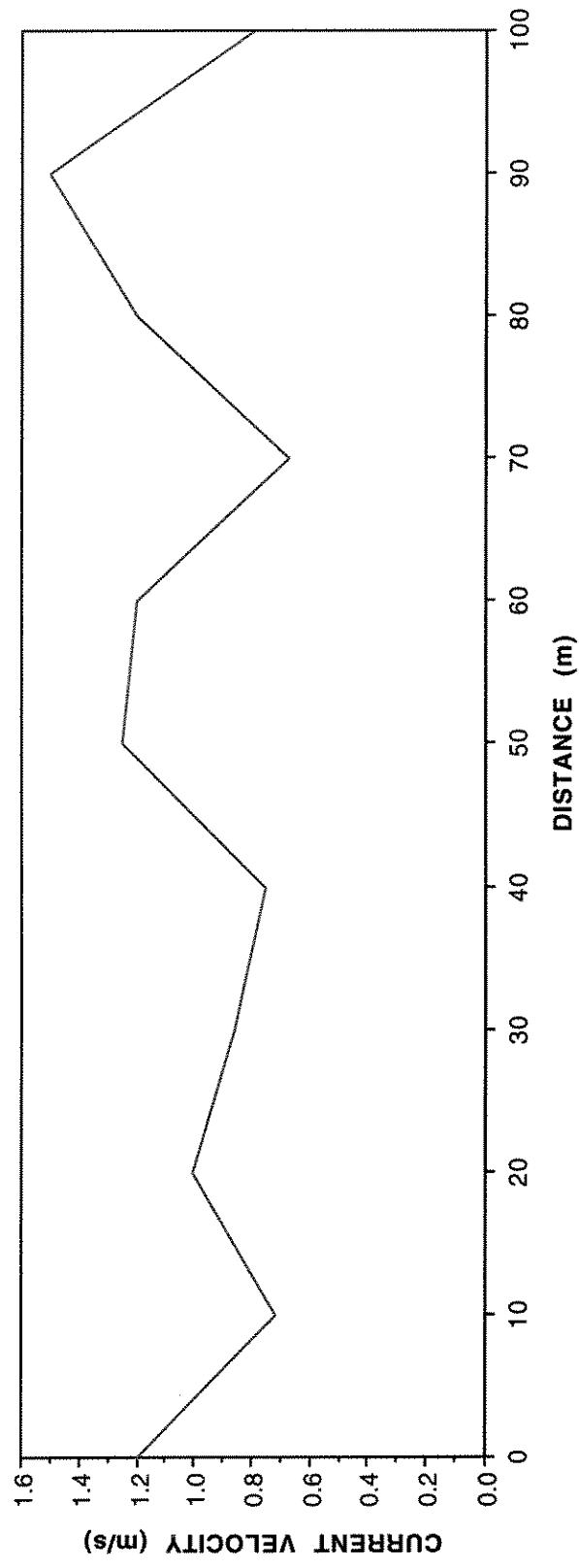
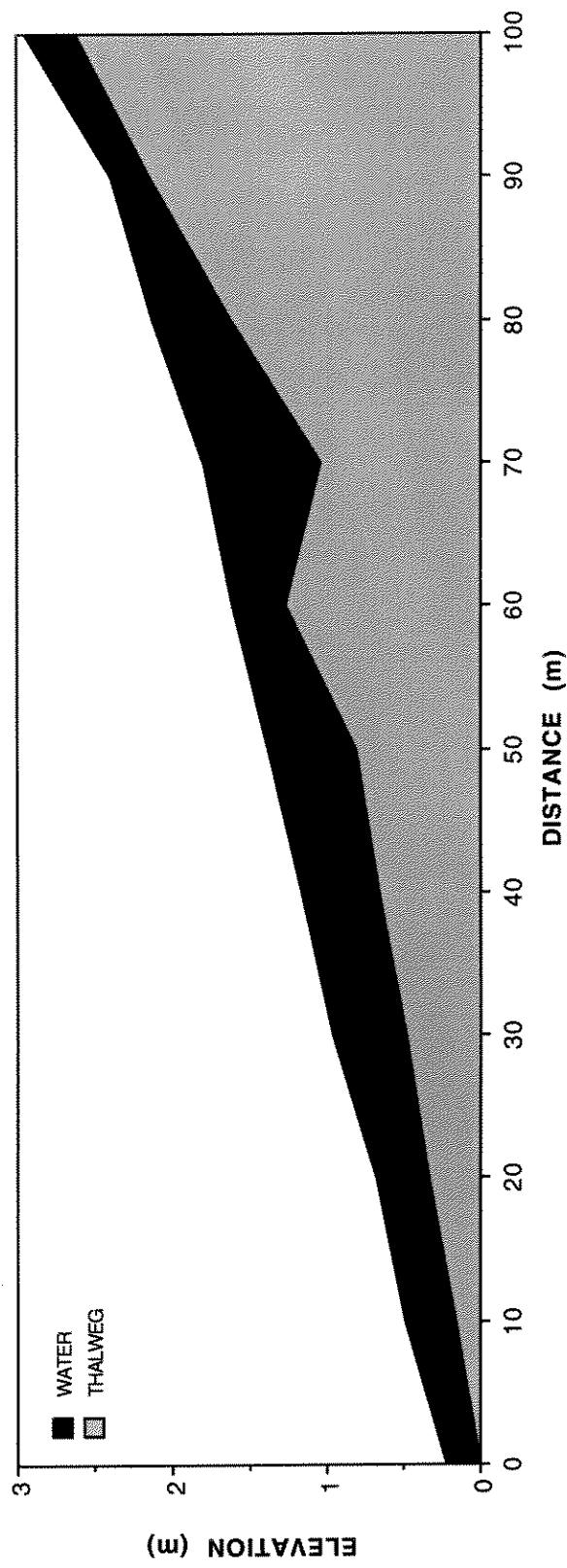


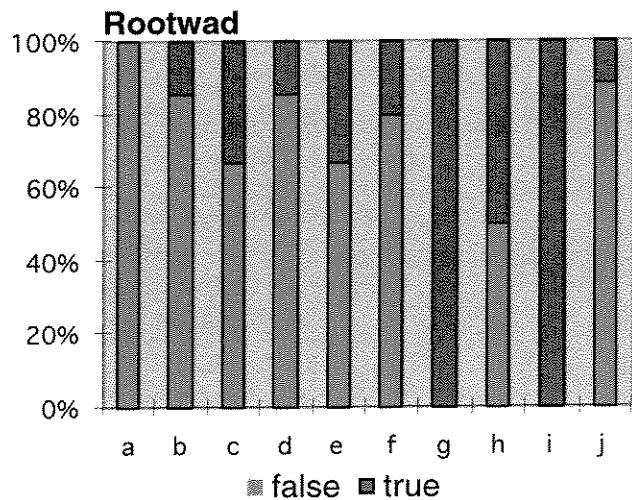
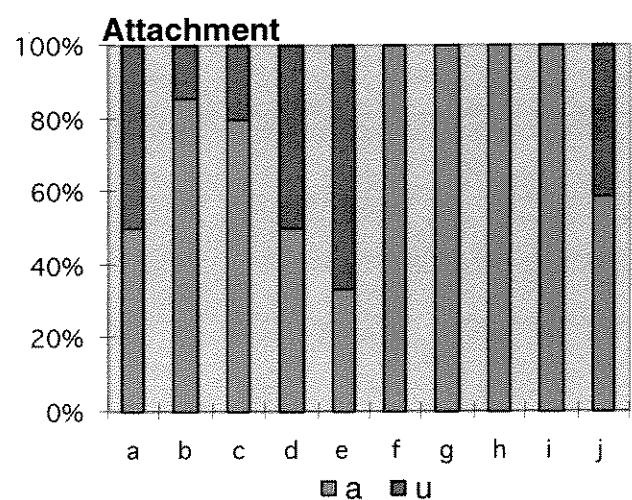
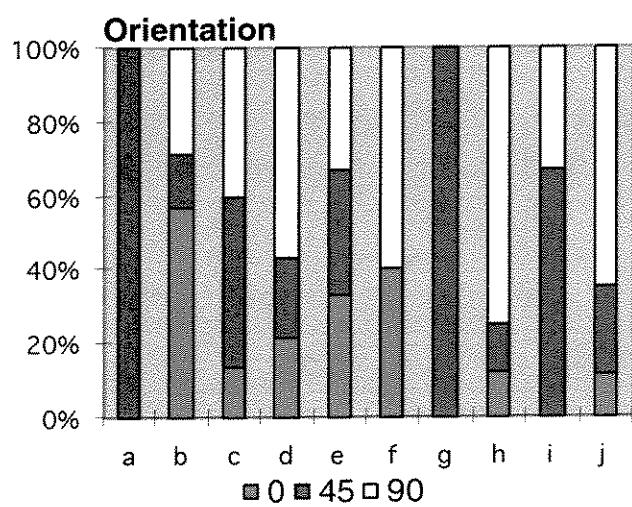
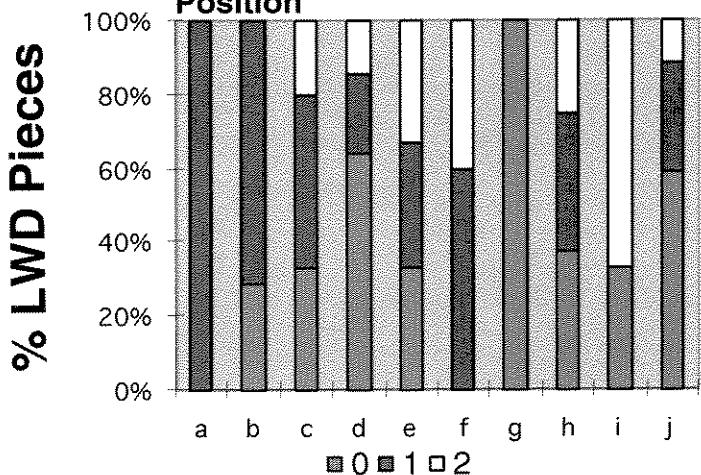
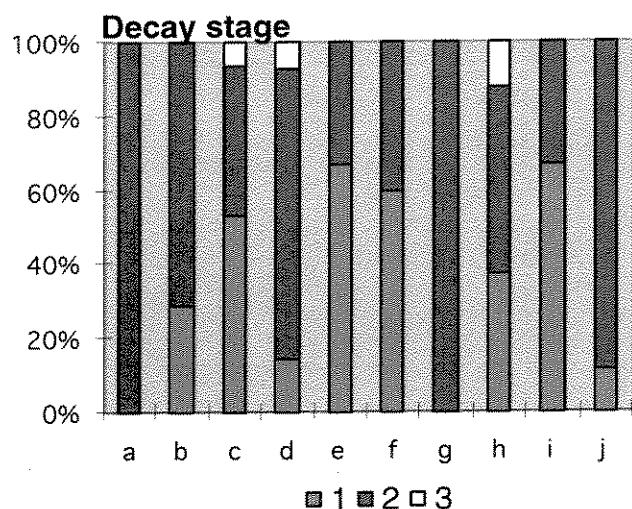
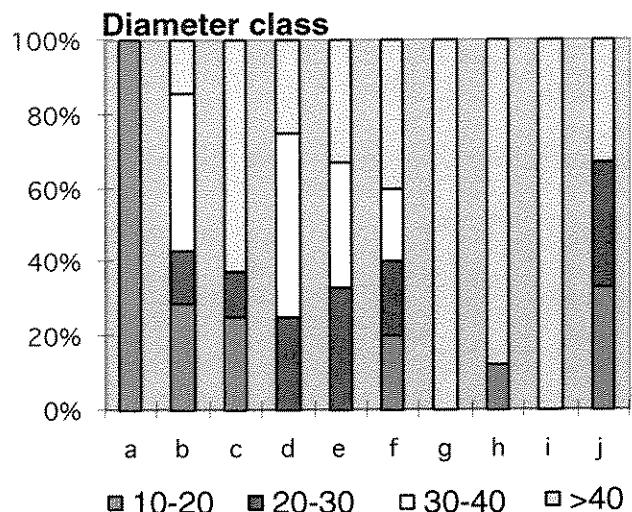
## Goat Creek reach c

A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



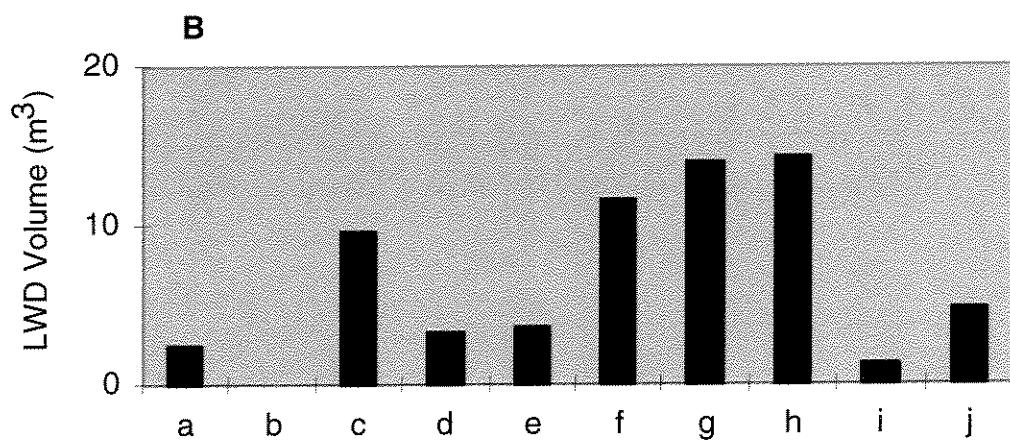
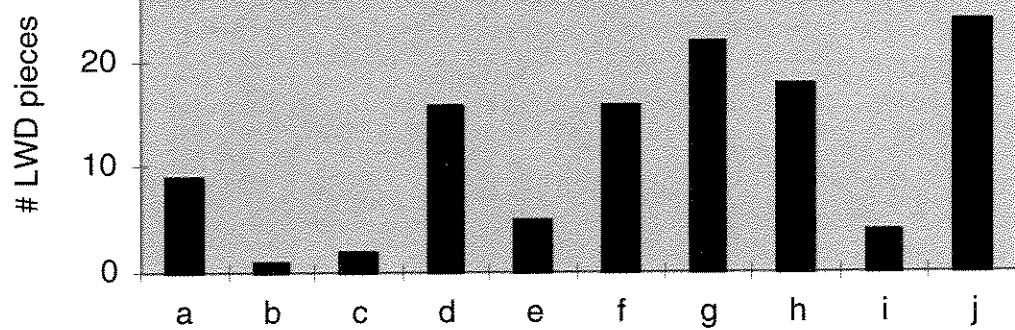
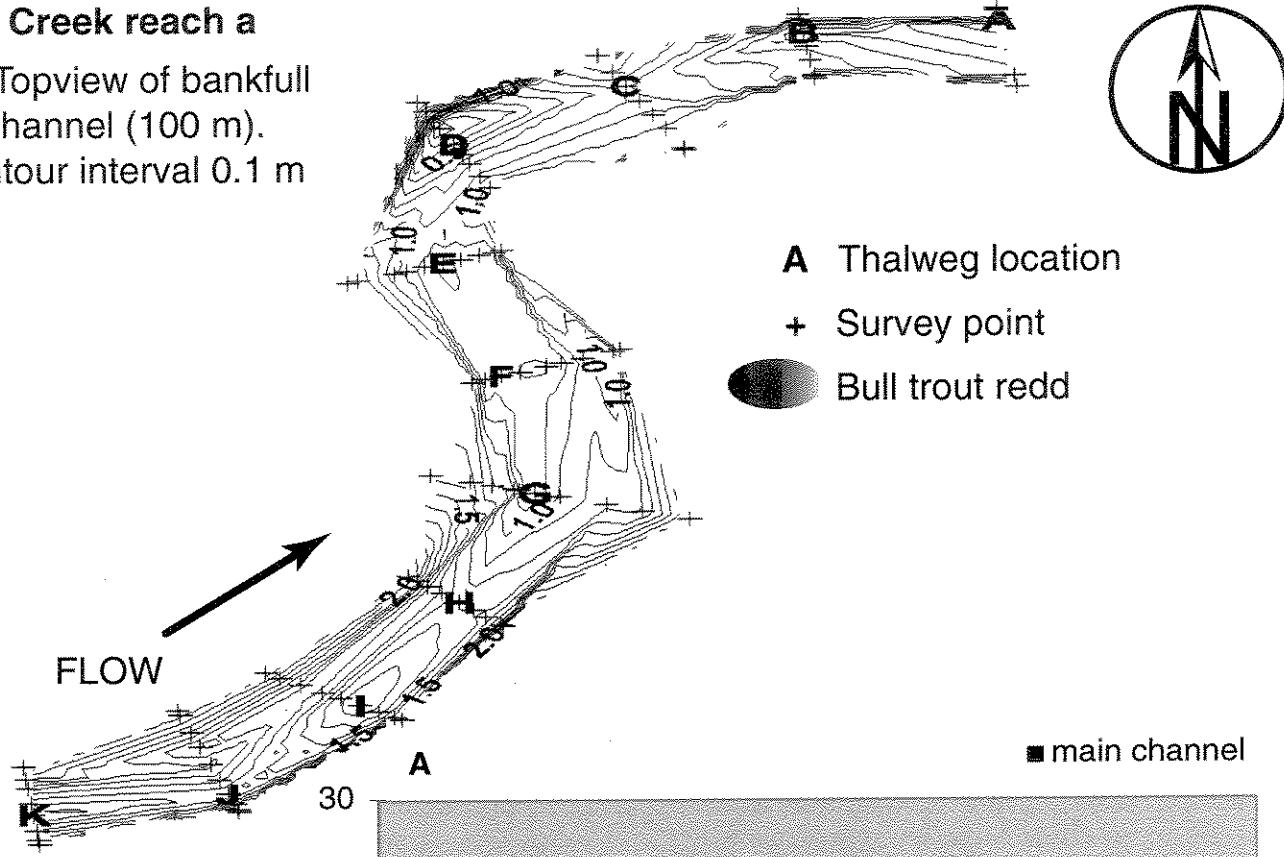
Goat Creek Reach C



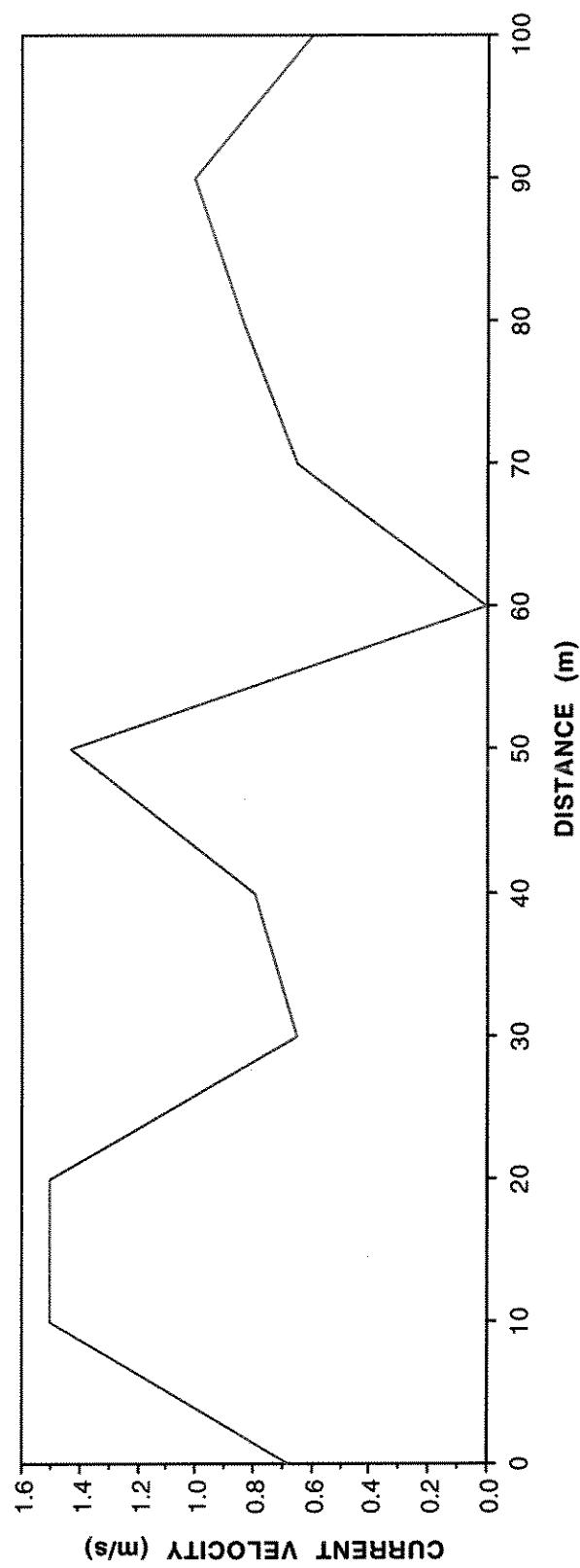
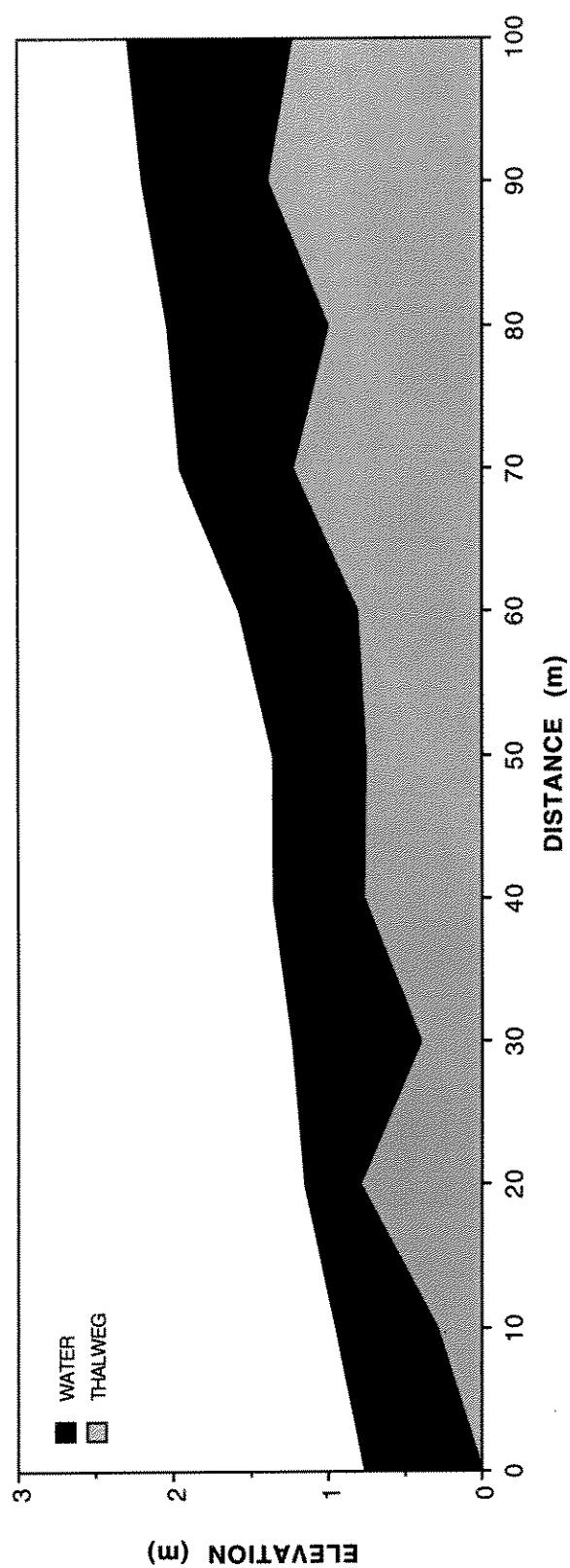


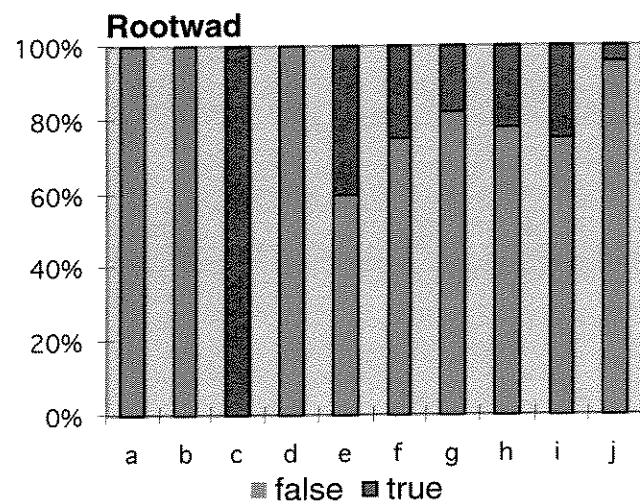
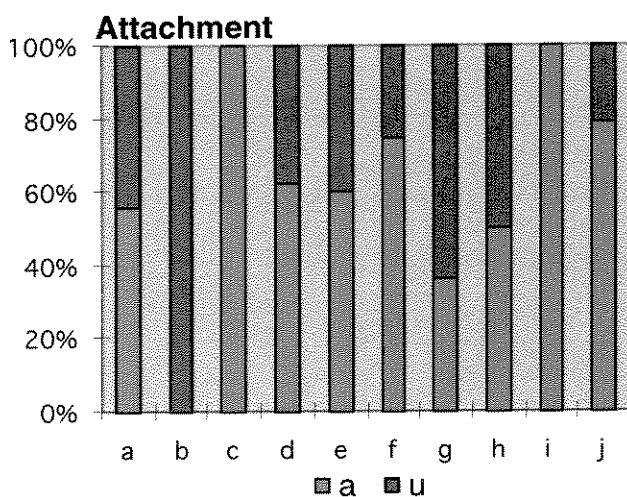
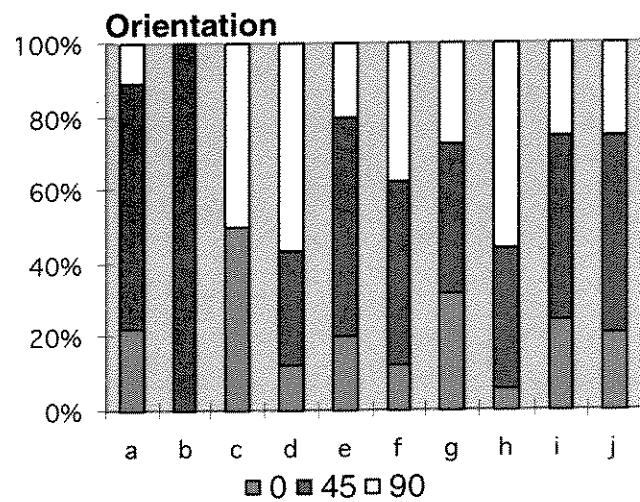
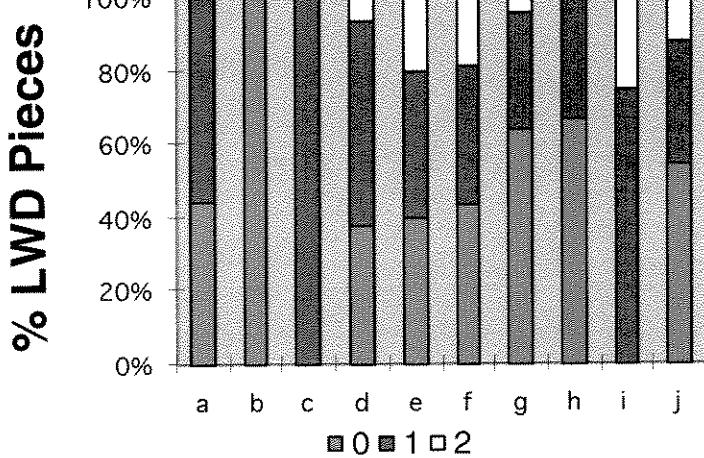
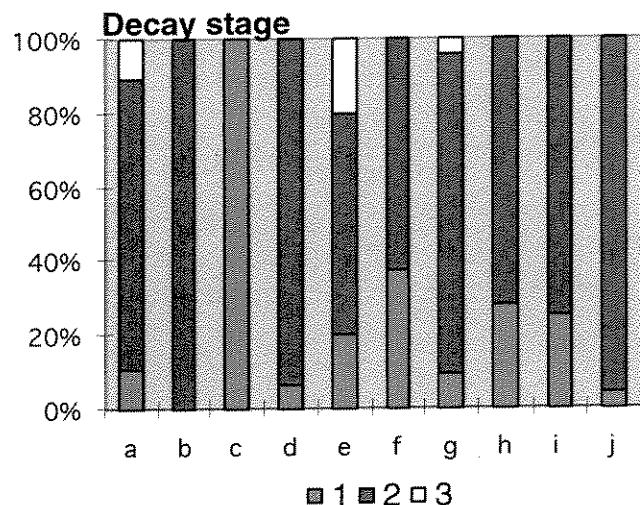
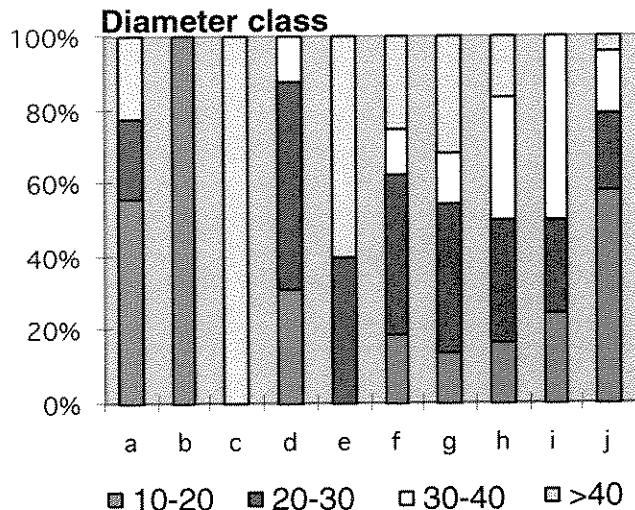
## Jim Creek reach a

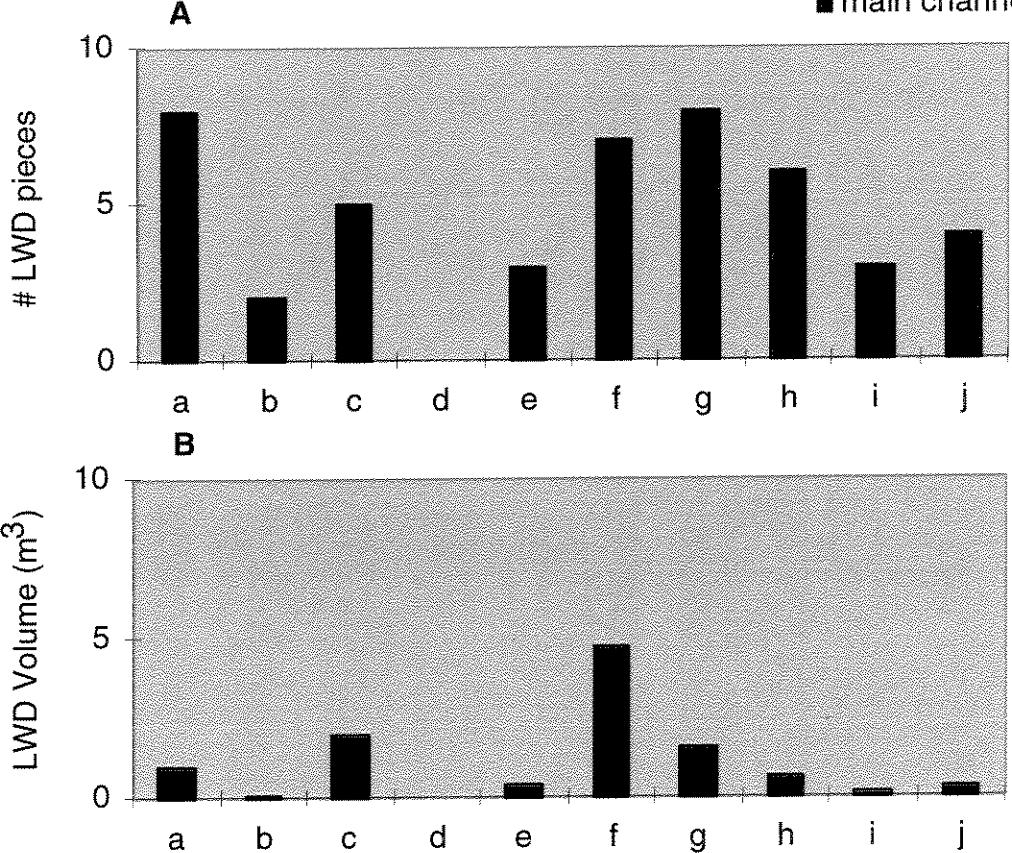
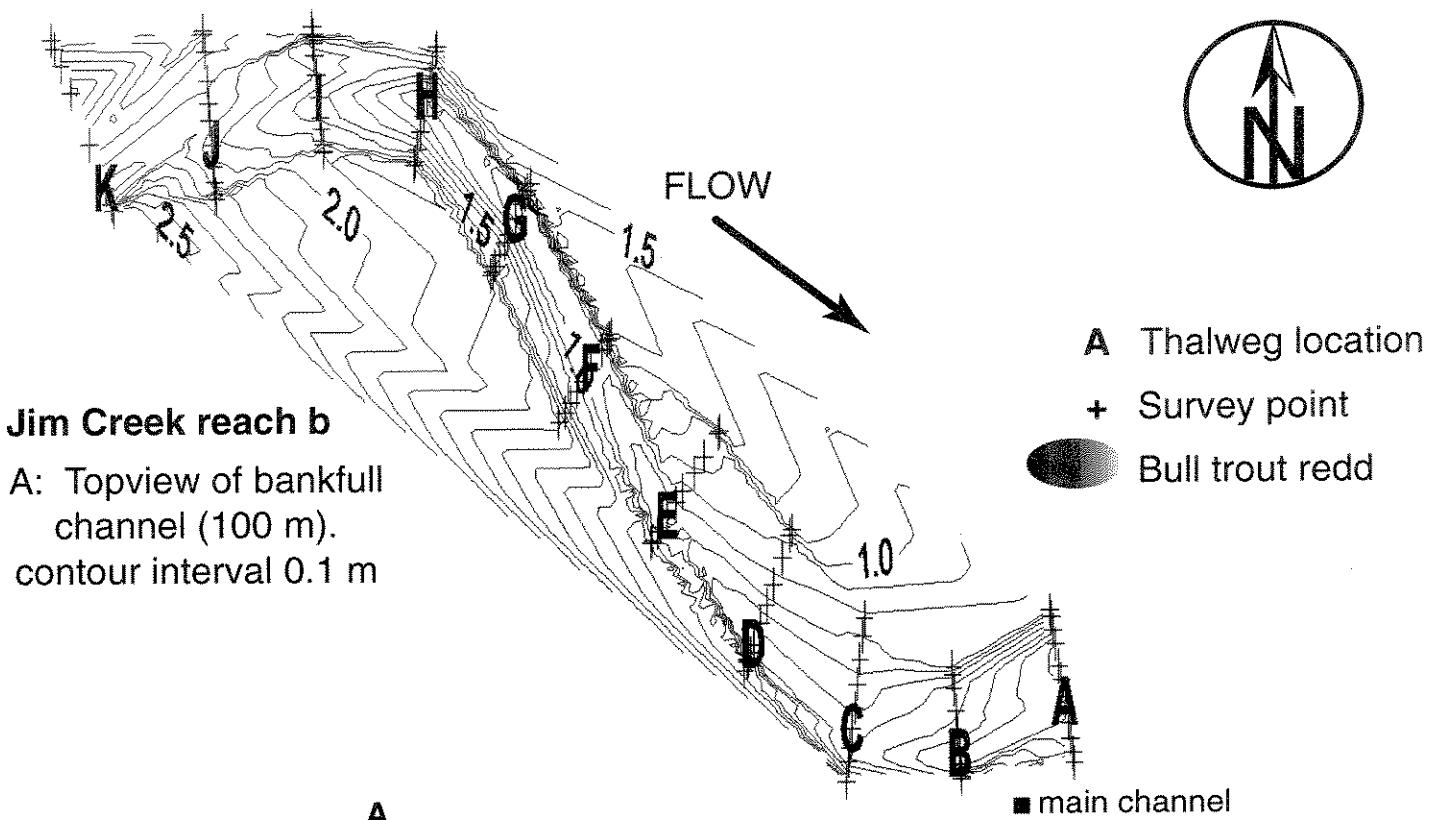
A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



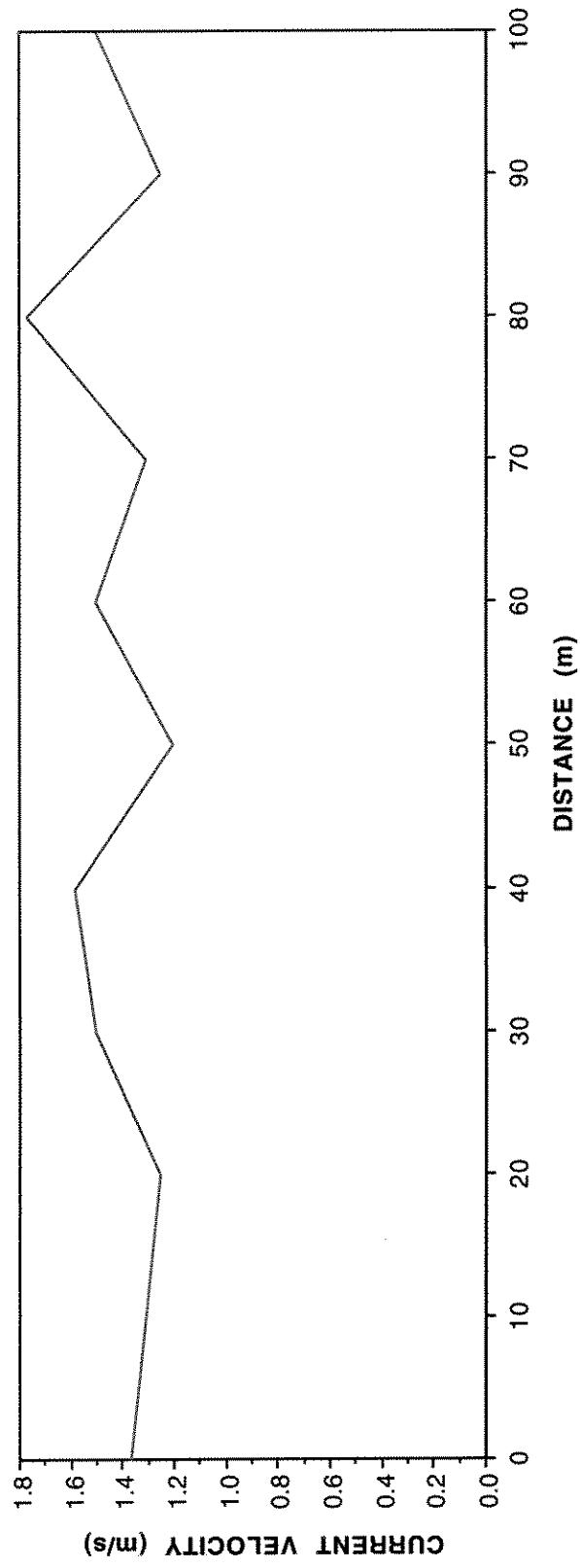
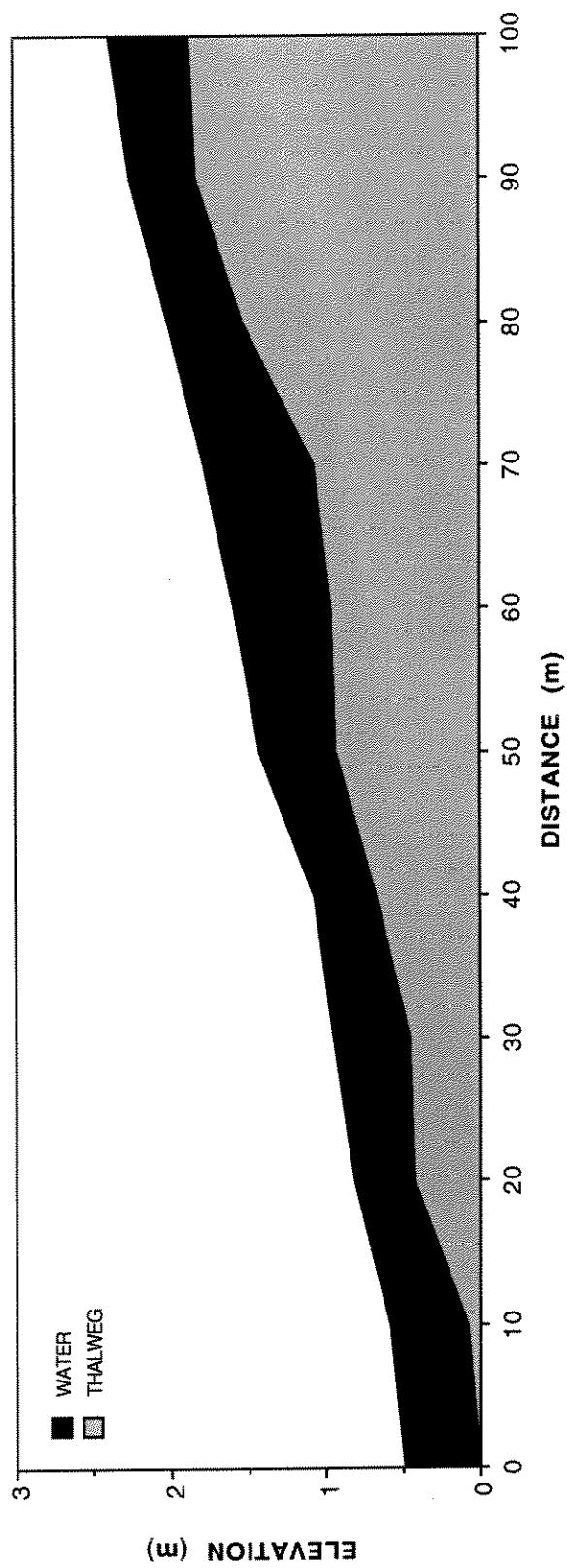
Jim Creek Reach A

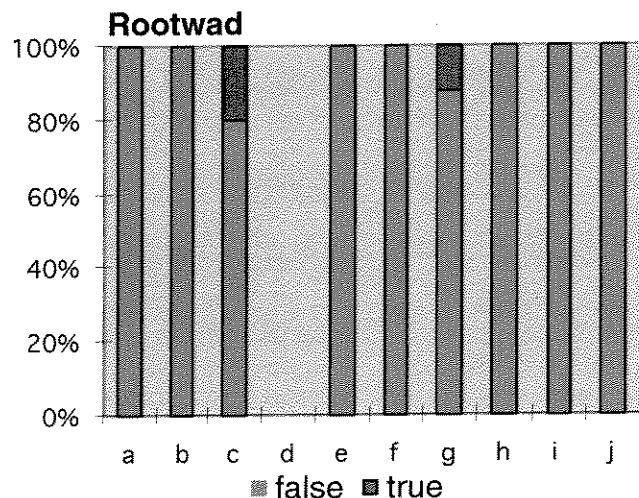
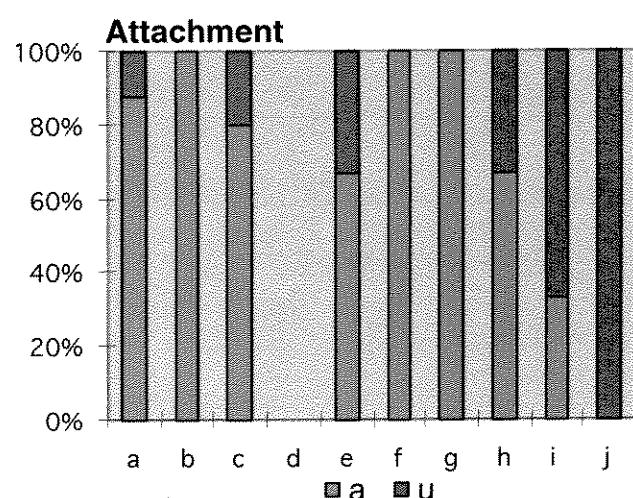
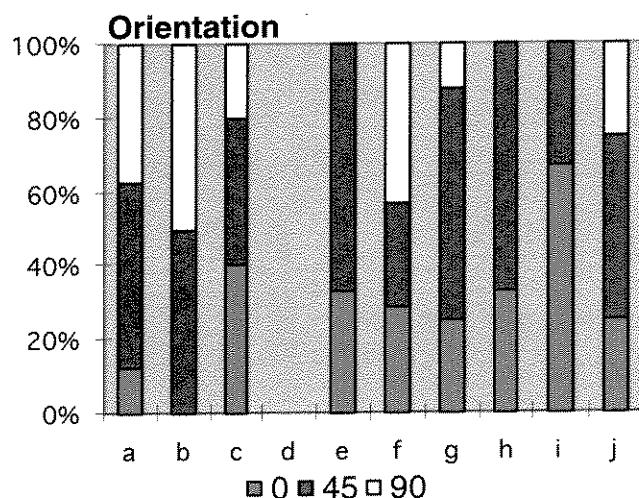
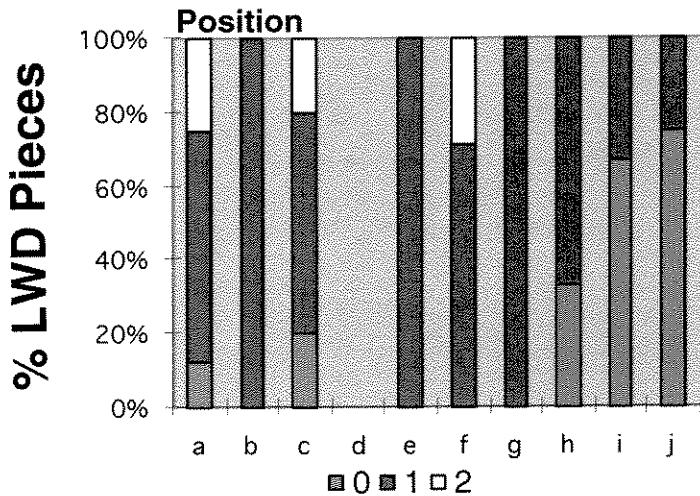
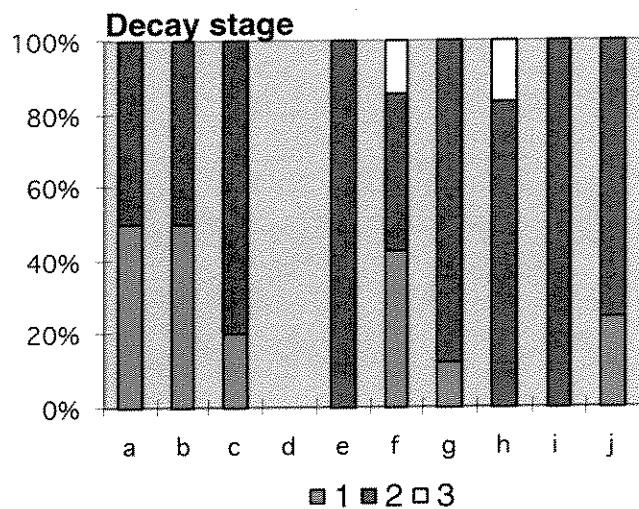
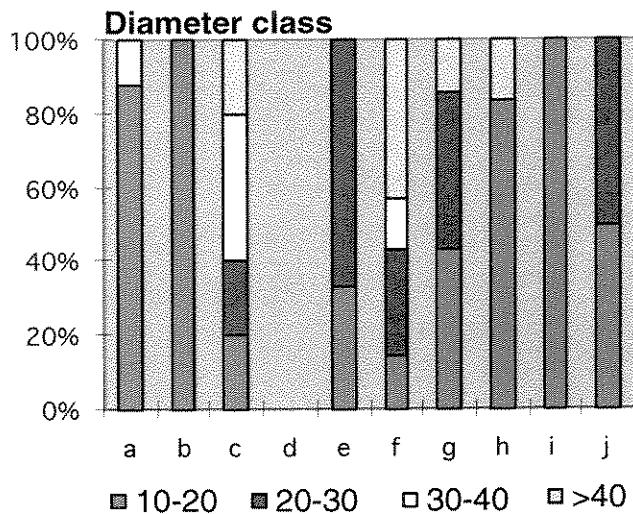






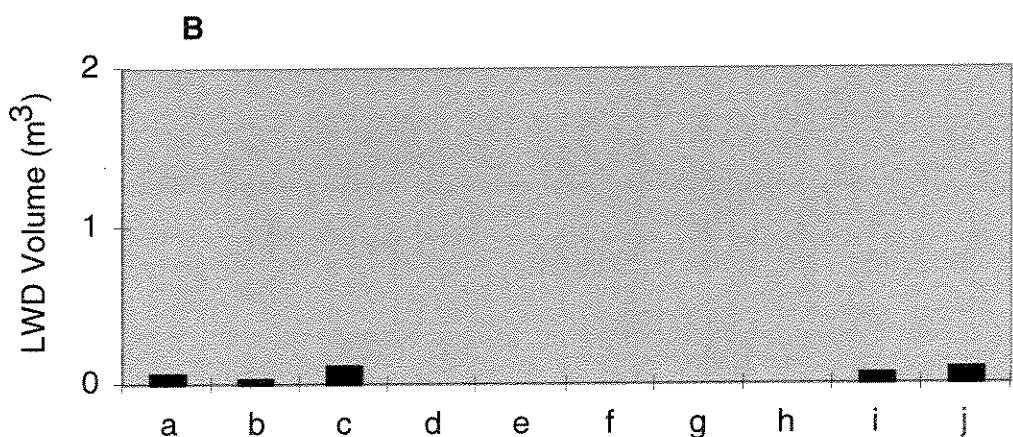
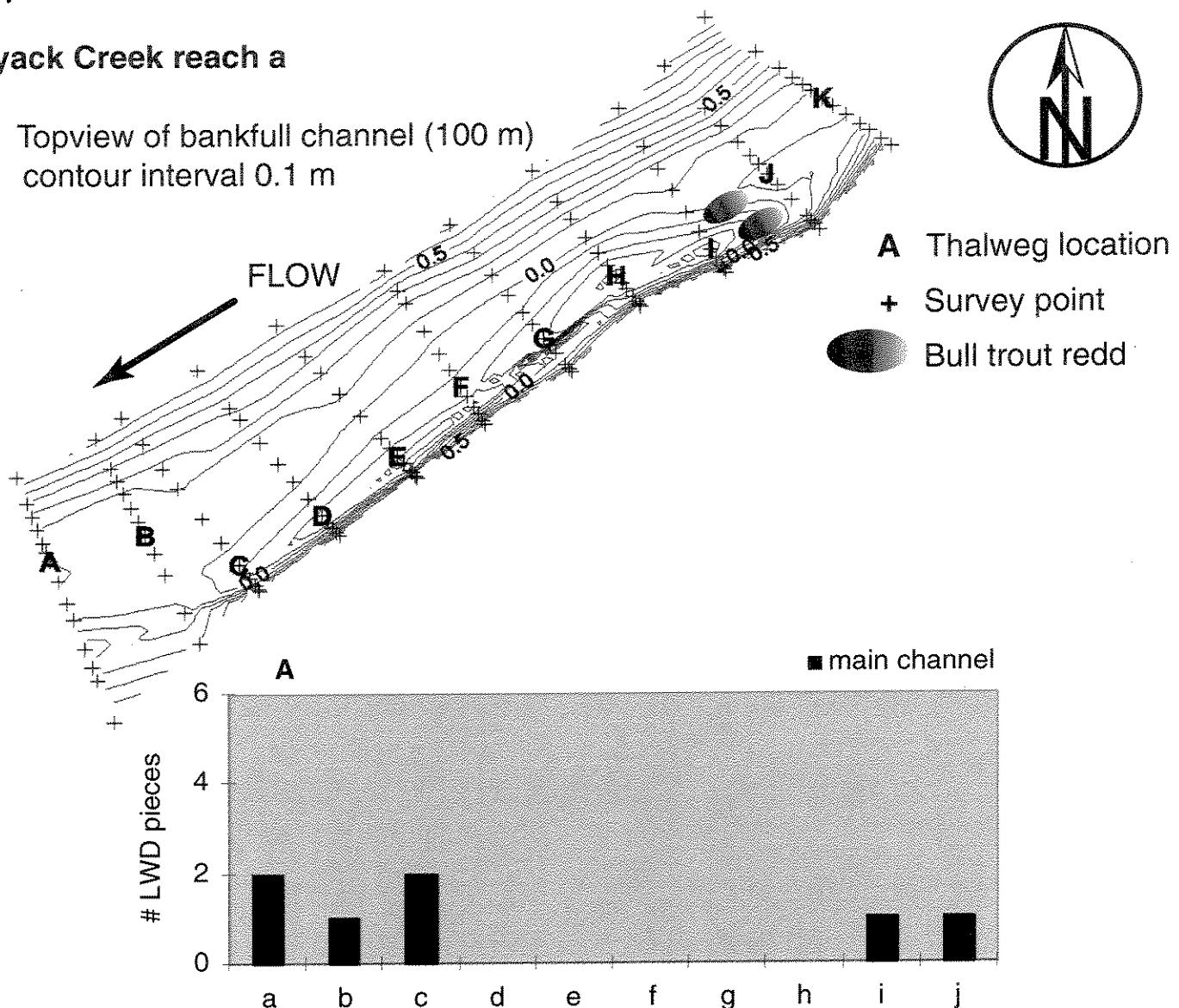
Jim Creek Reach B



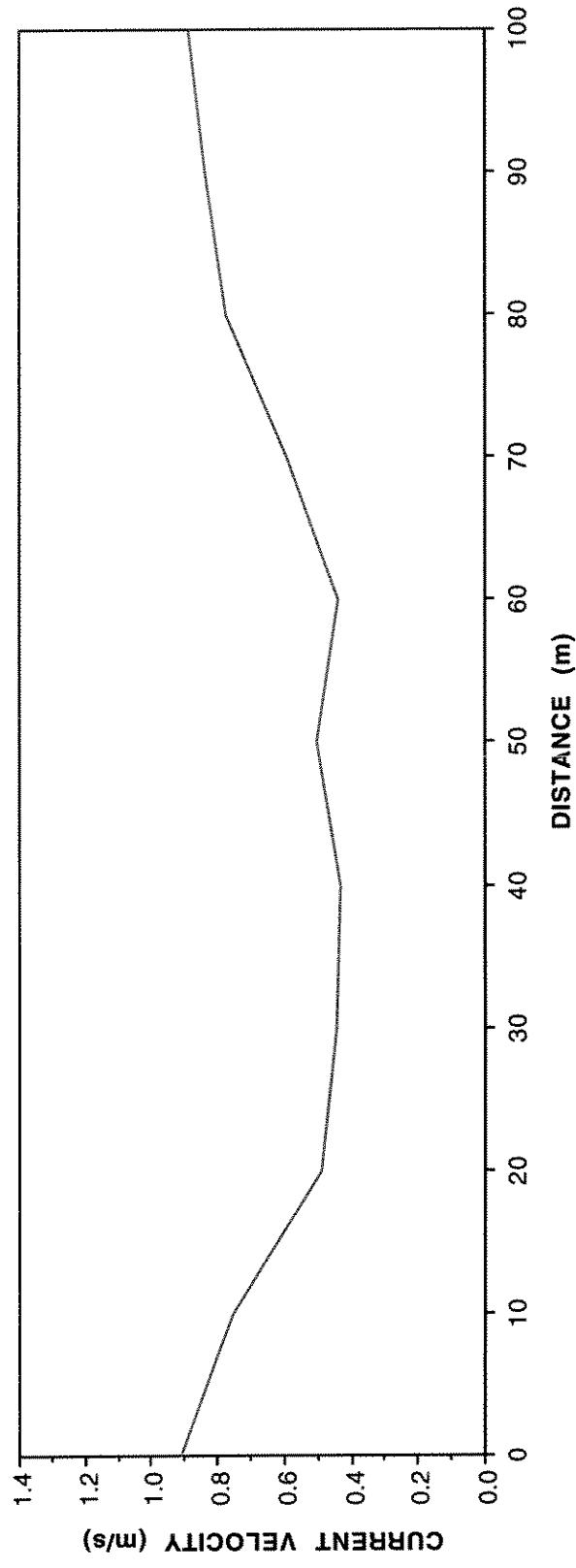
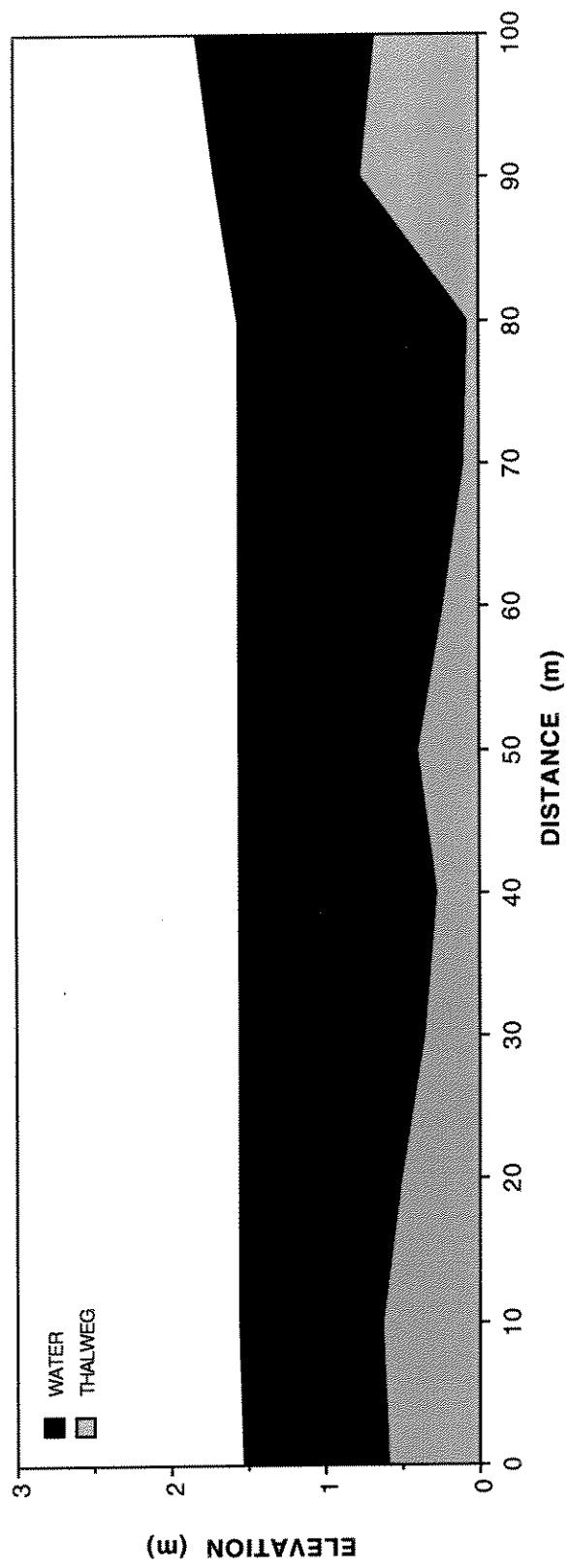


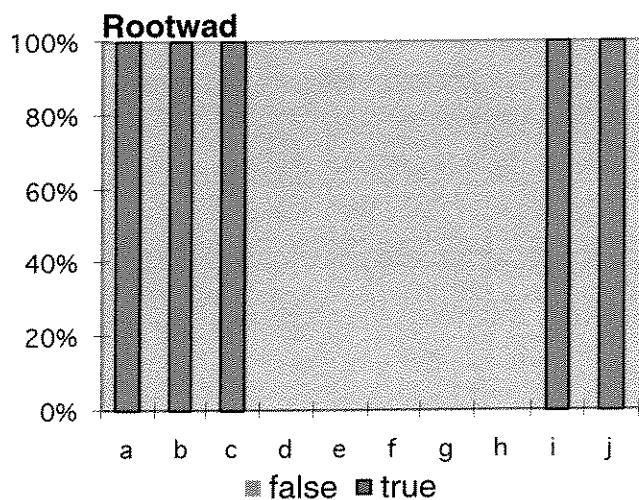
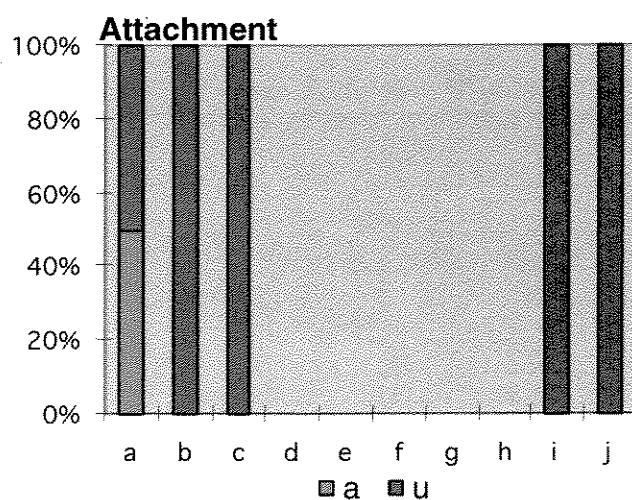
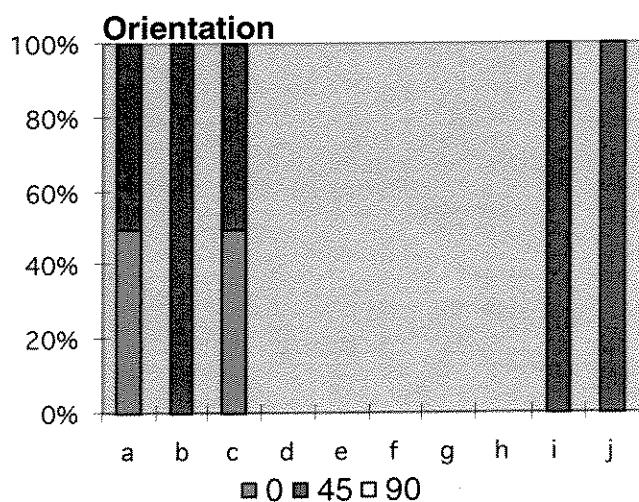
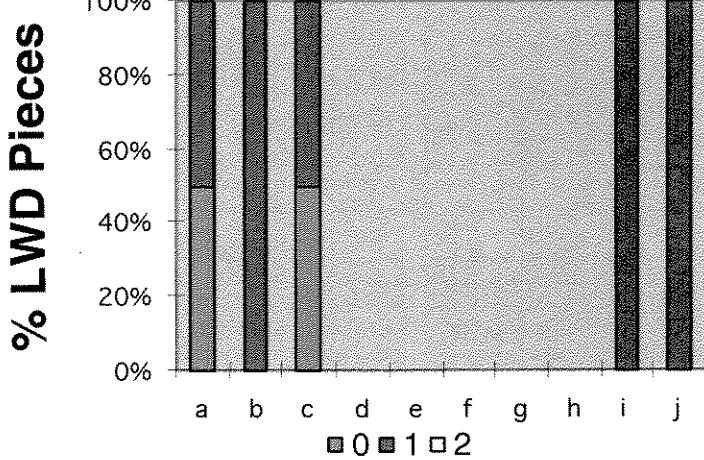
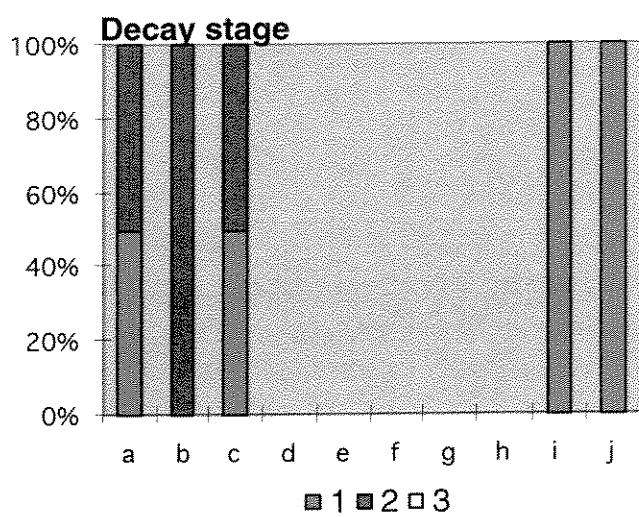
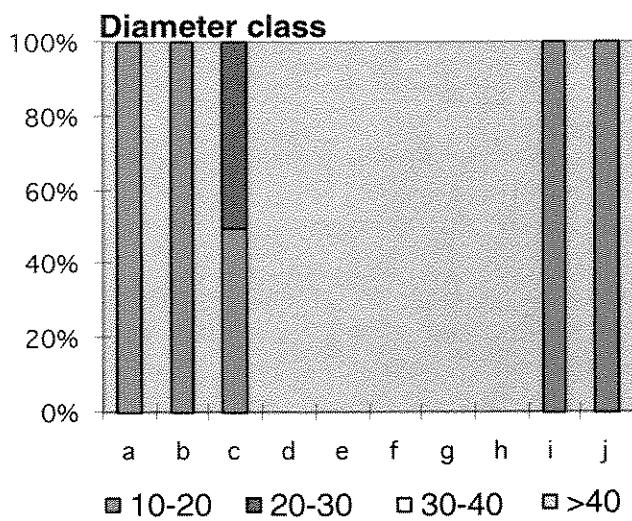
## Nyack Creek reach a

A: Topview of bankfull channel (100 m)  
contour interval 0.1 m



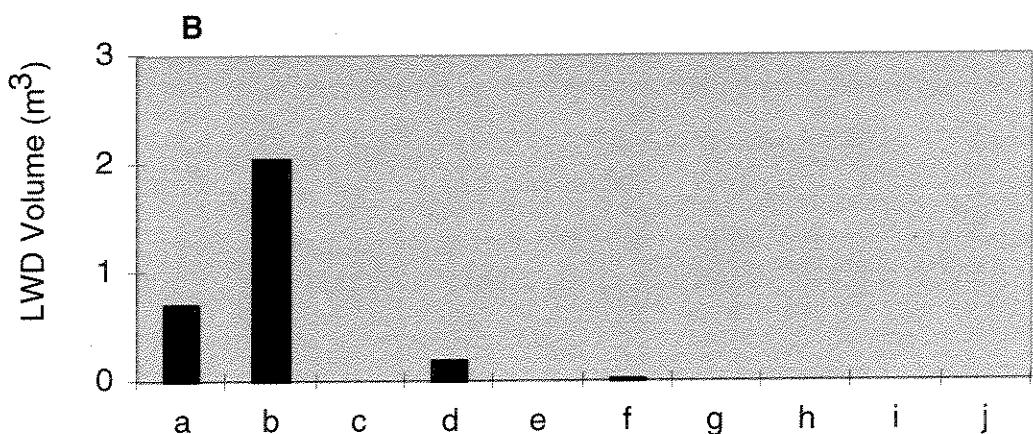
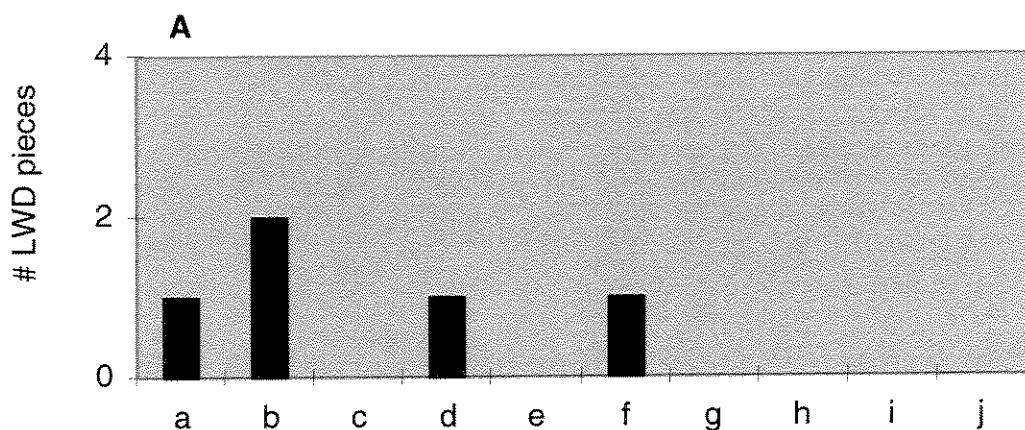
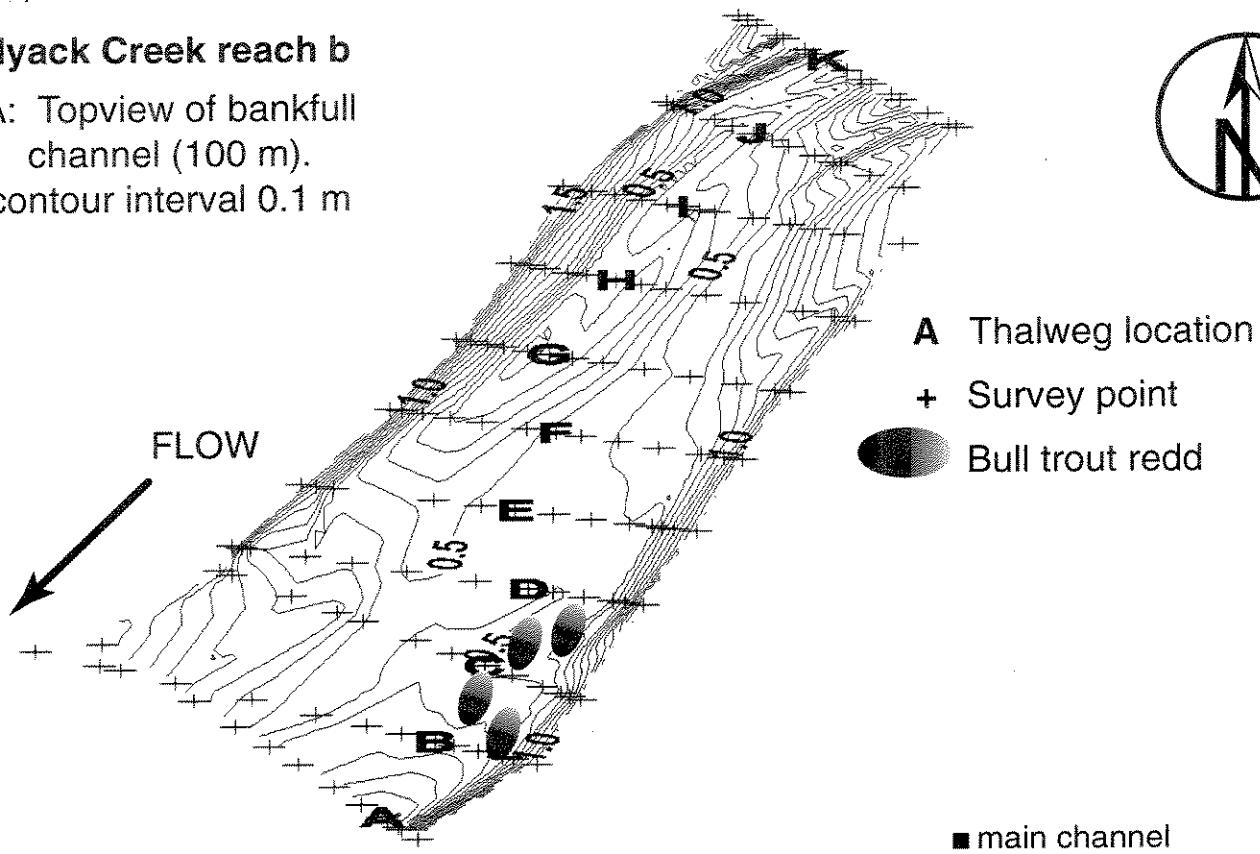
### Nyack Creek Reach A



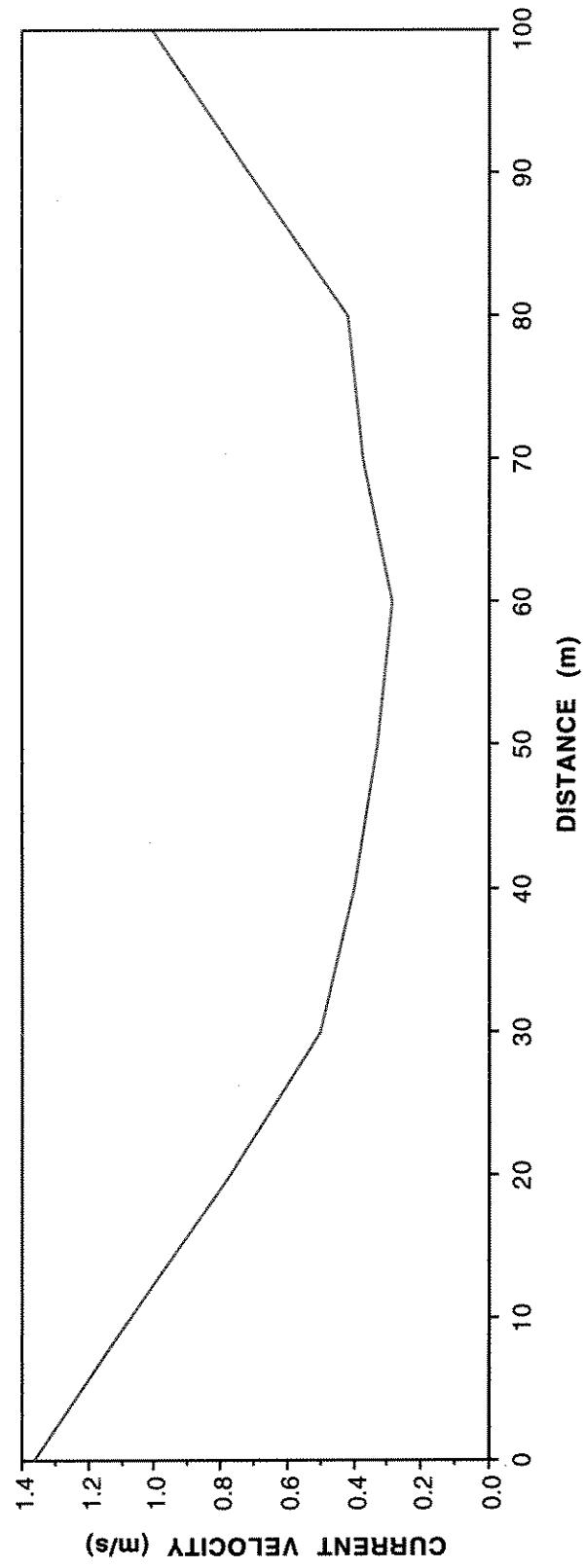
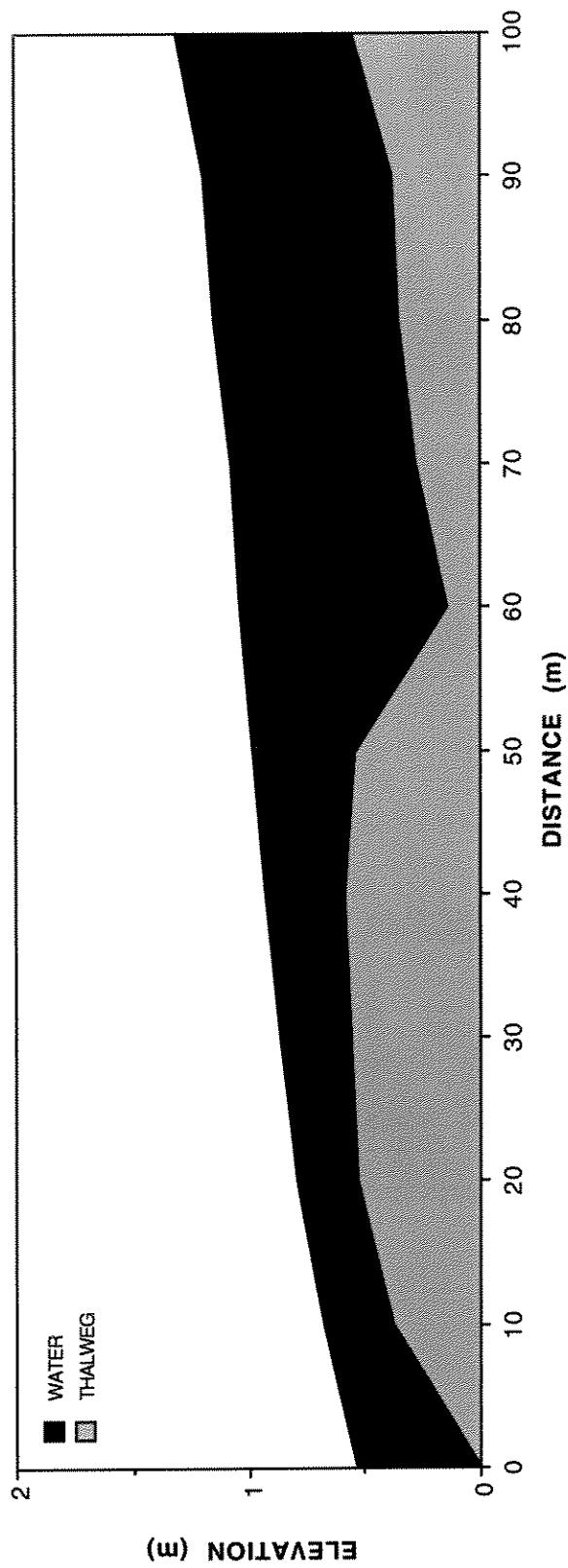


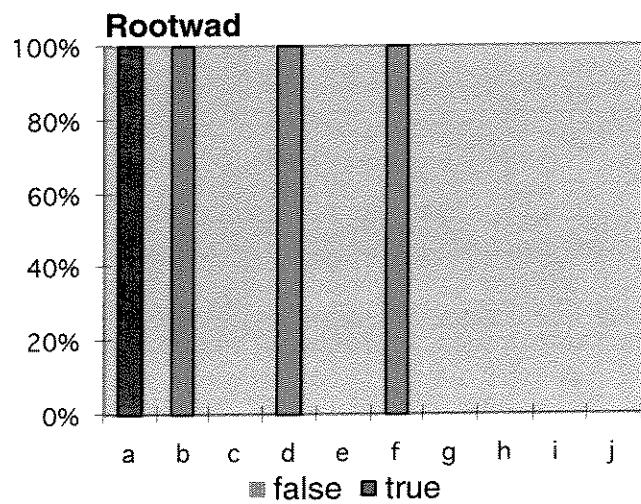
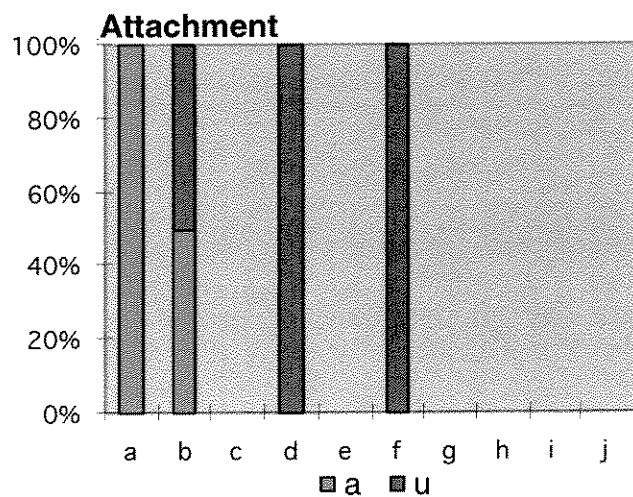
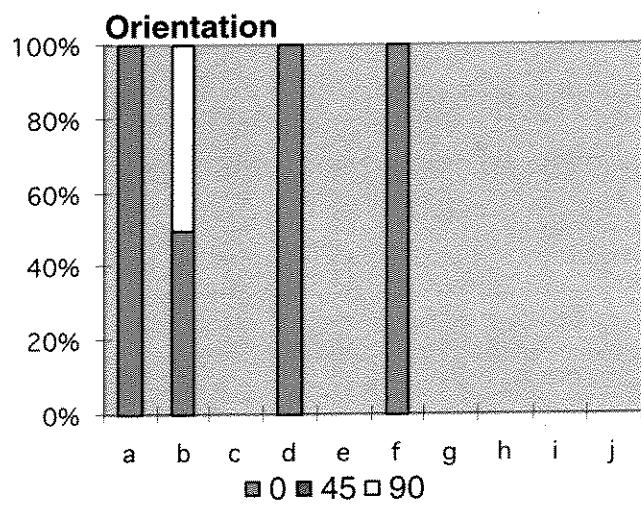
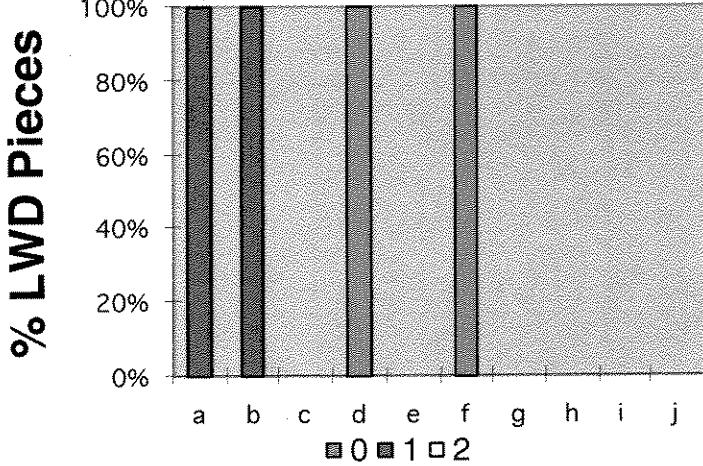
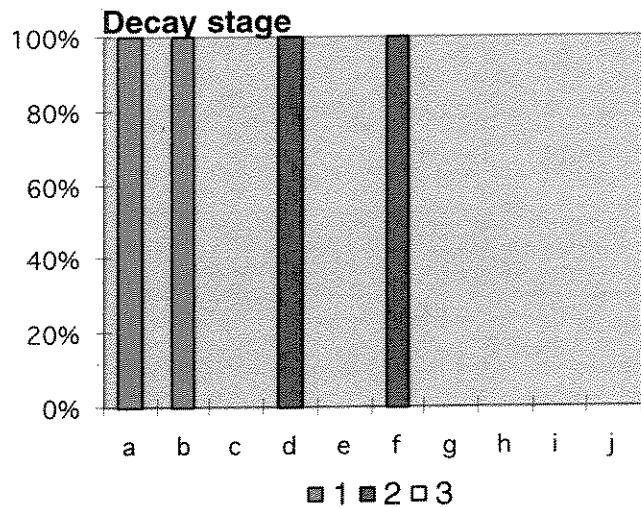
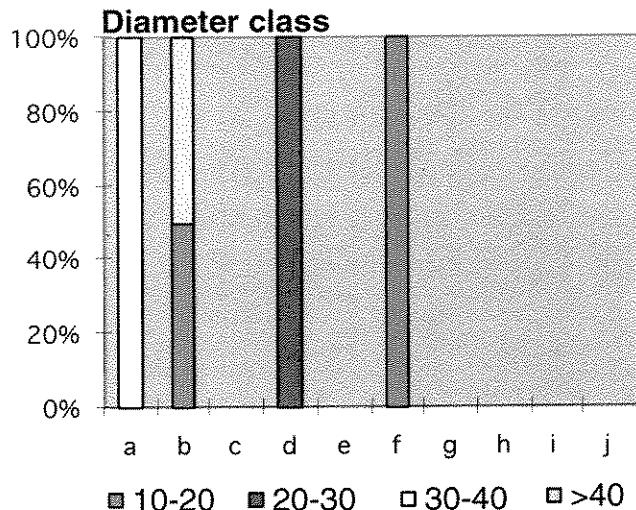
## Nyack Creek reach b

A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



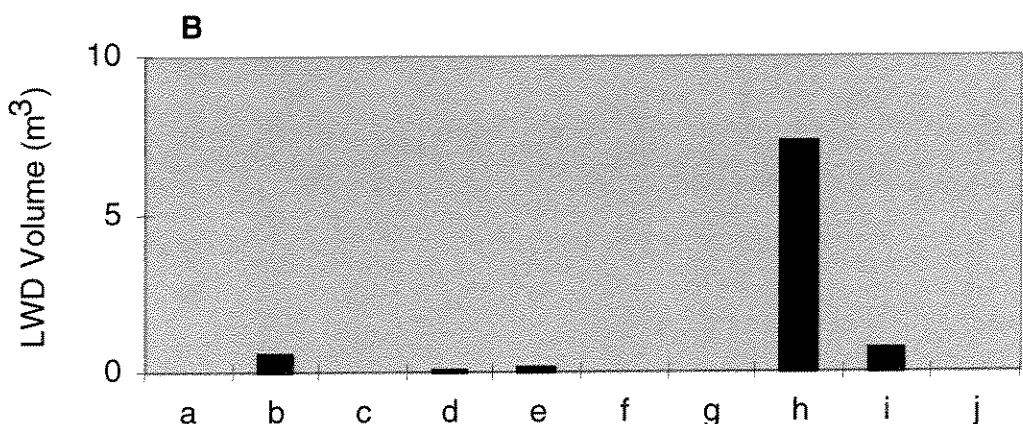
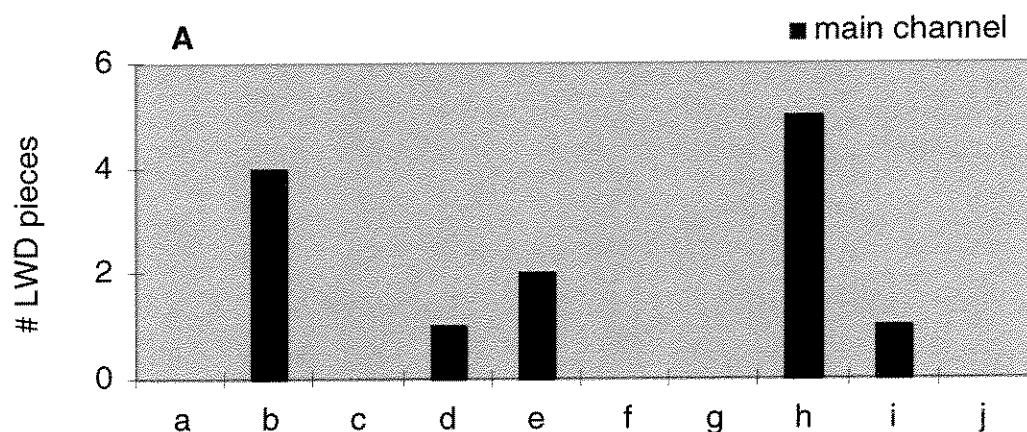
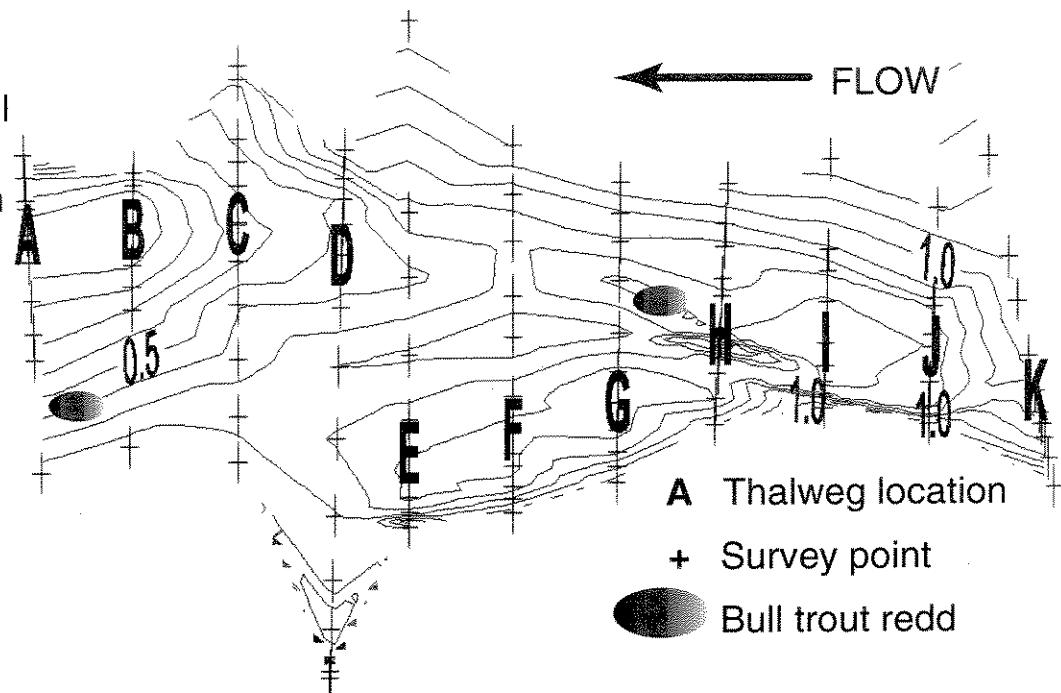
Nyack Creek Reach B



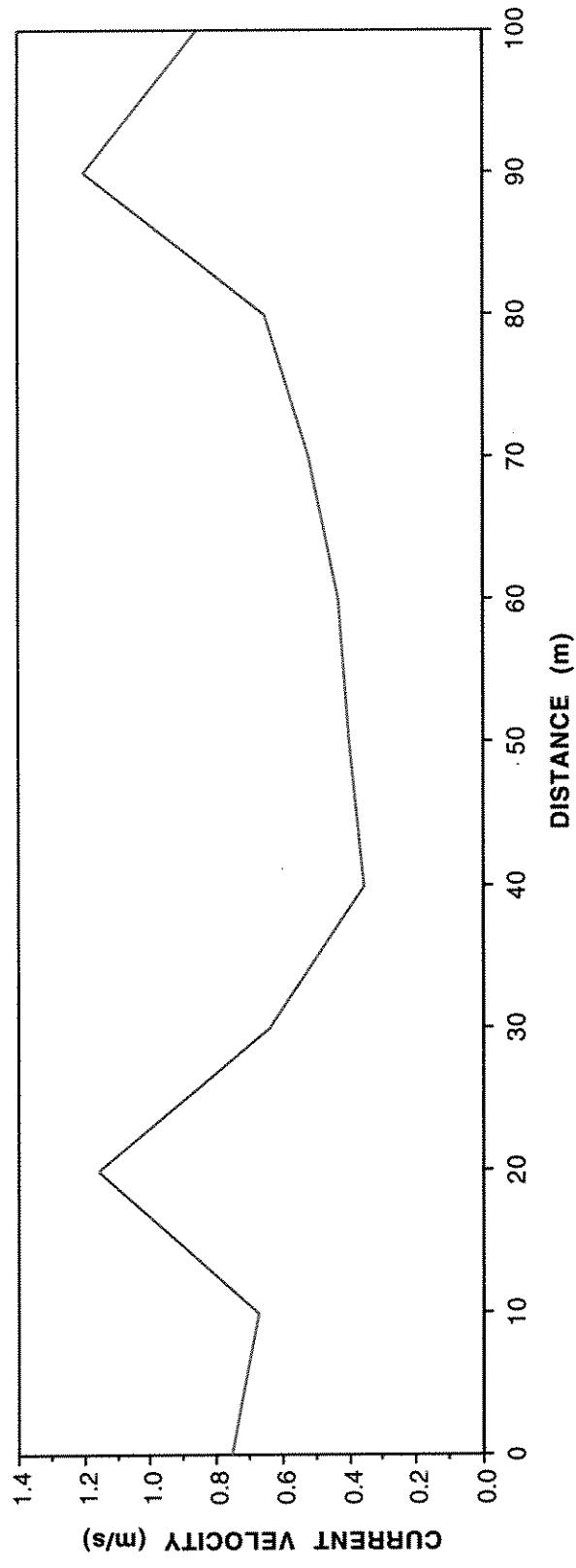
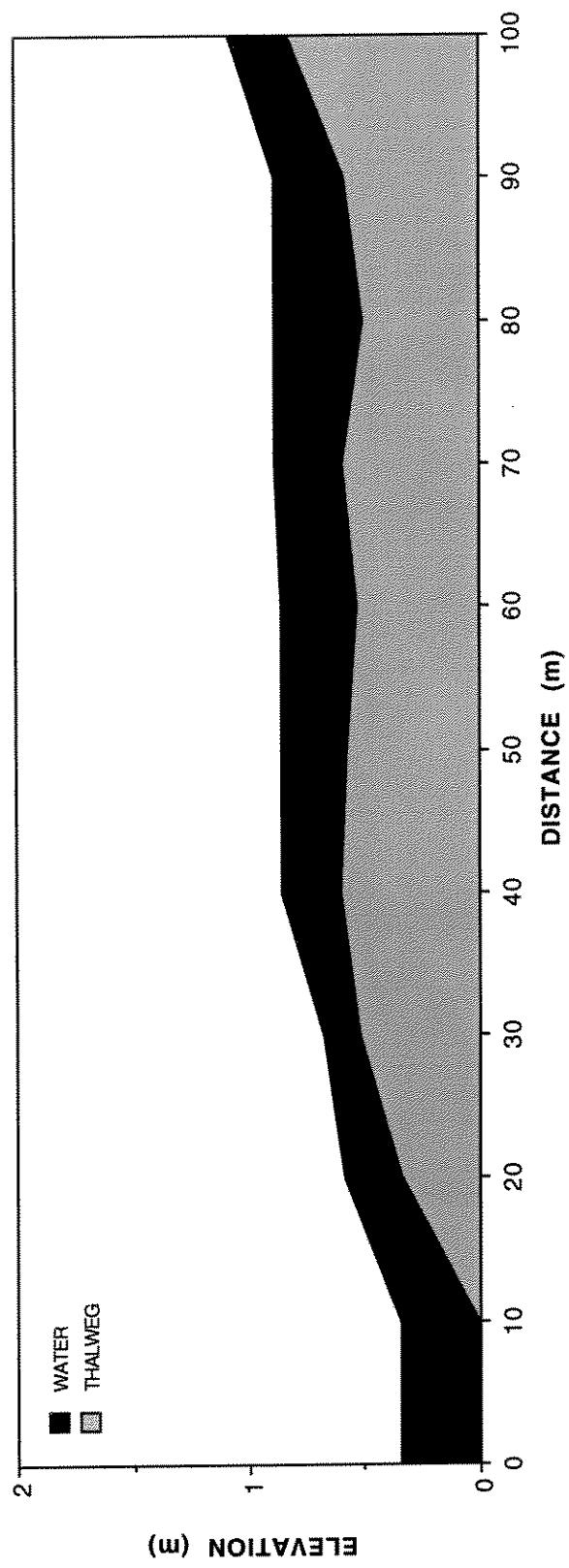


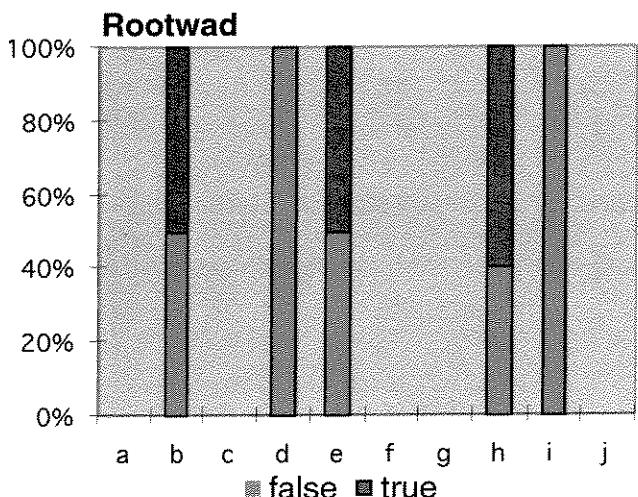
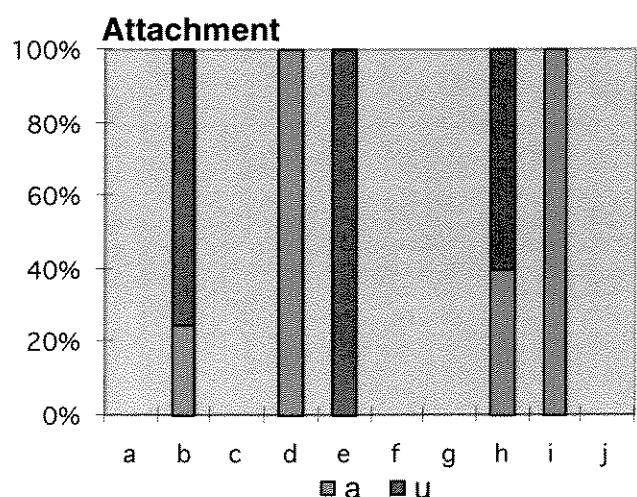
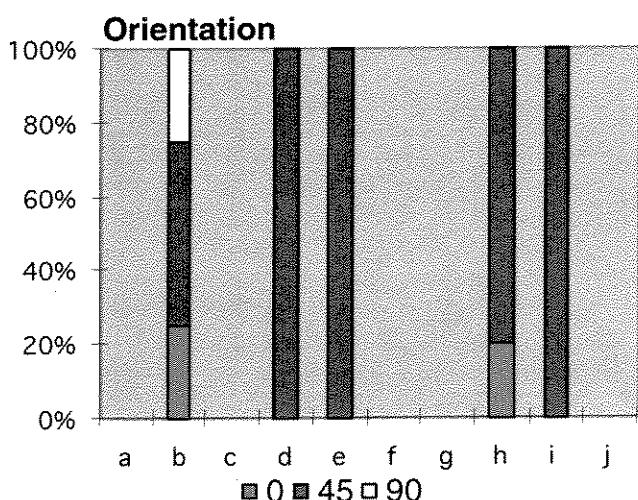
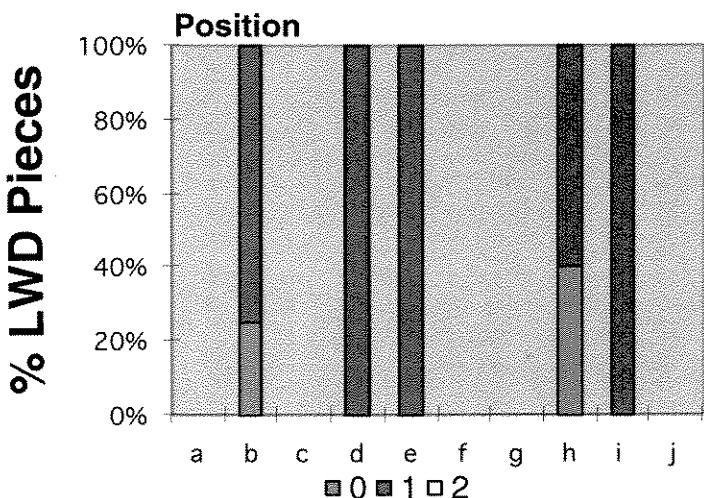
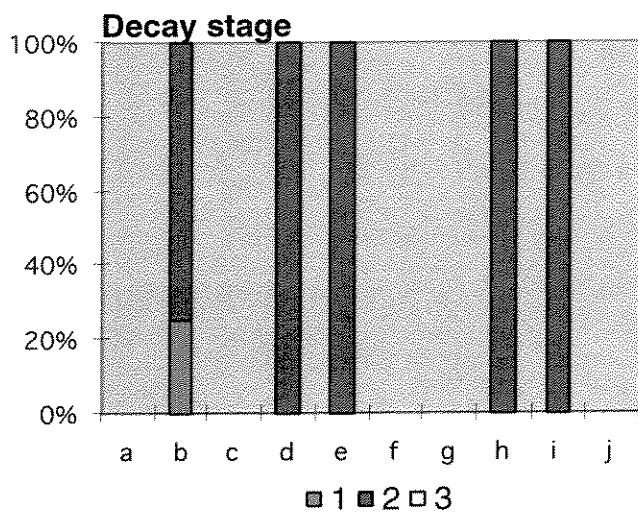
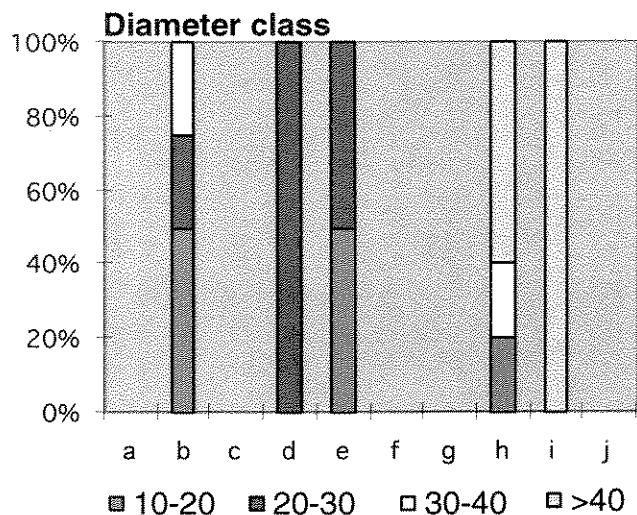
## Ole Creek reach a

A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



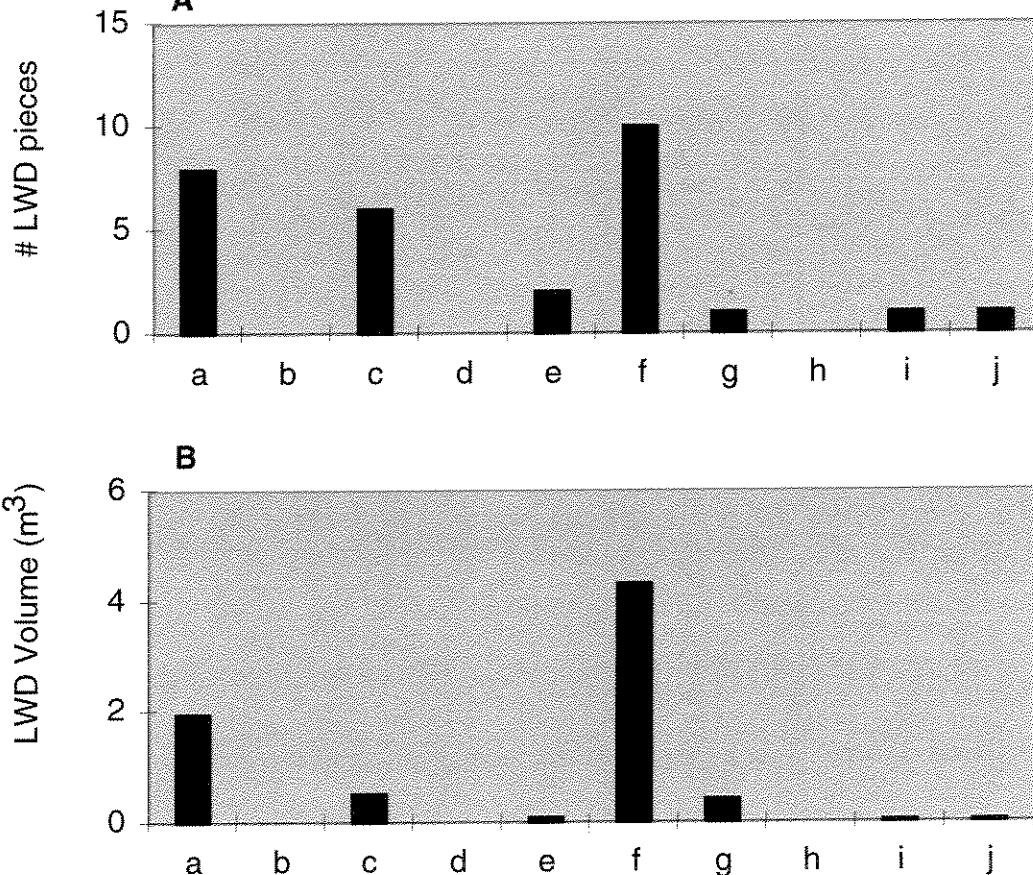
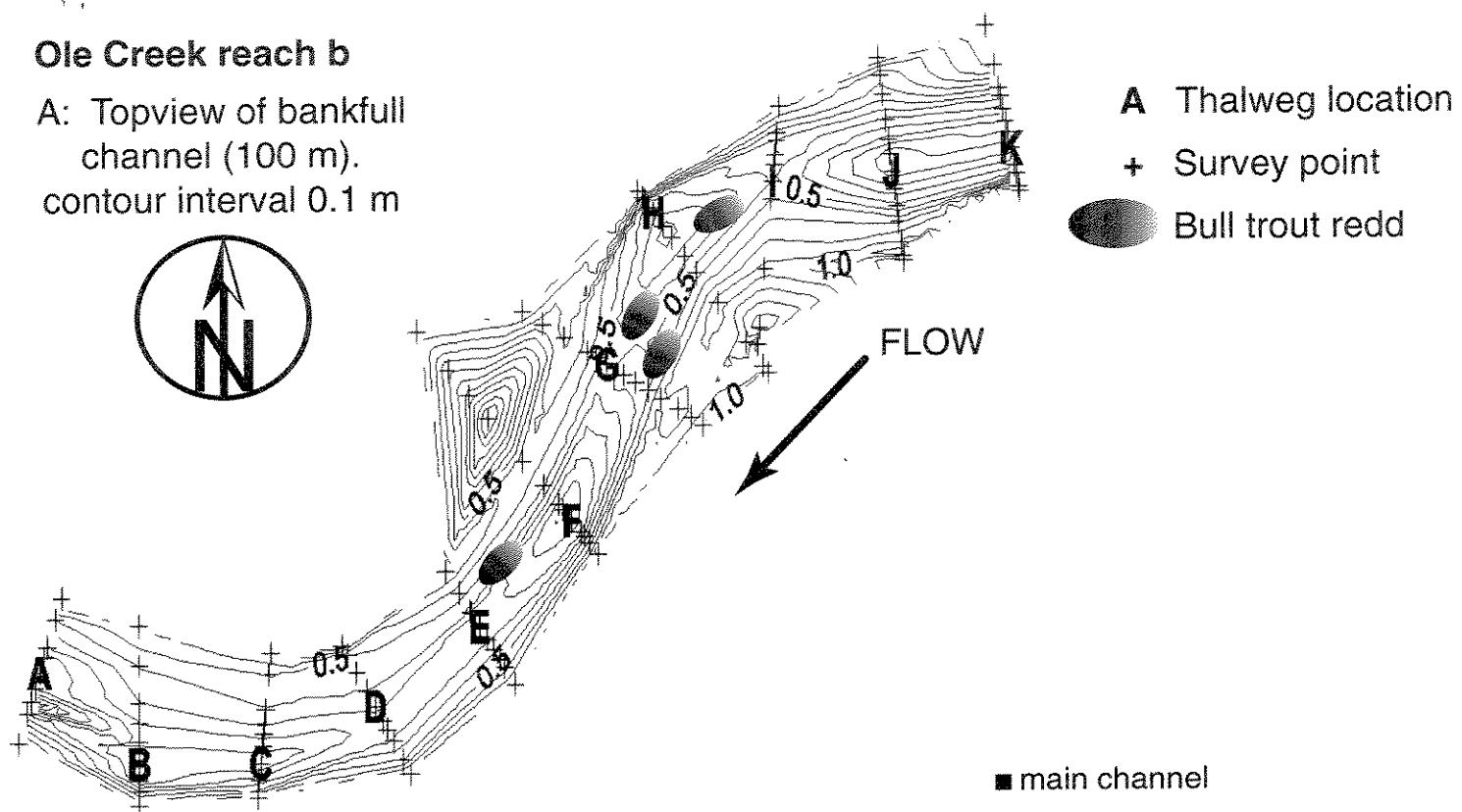
Ole Creek Reach A



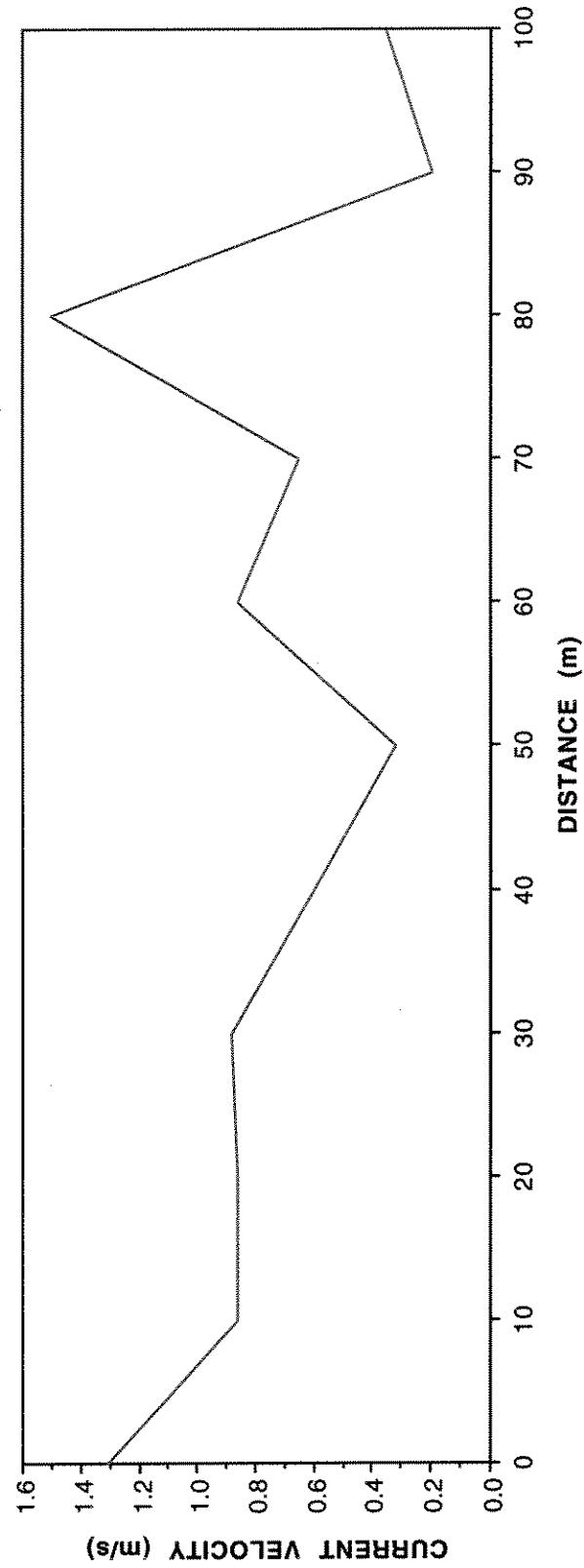
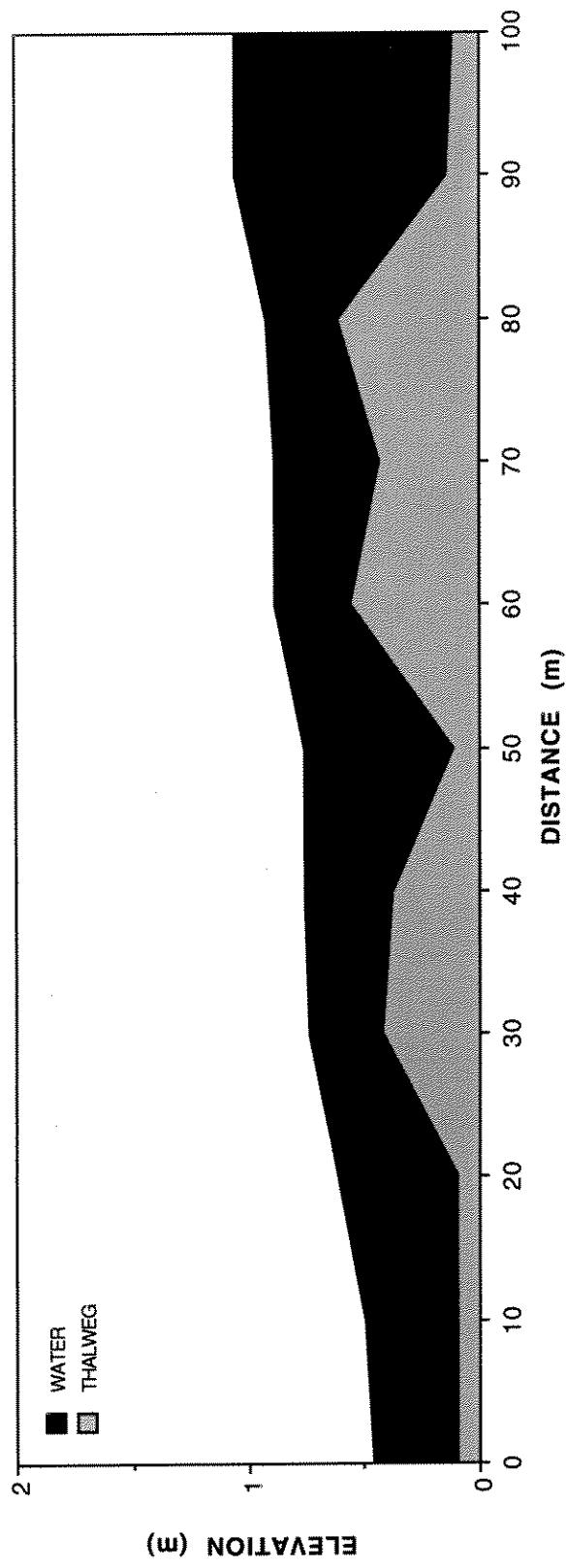


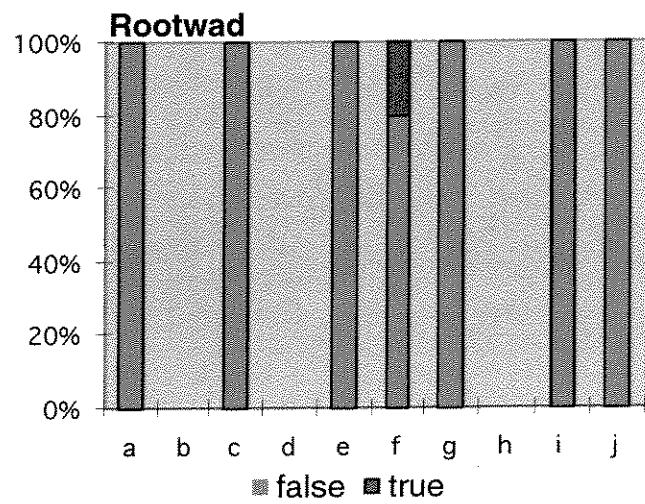
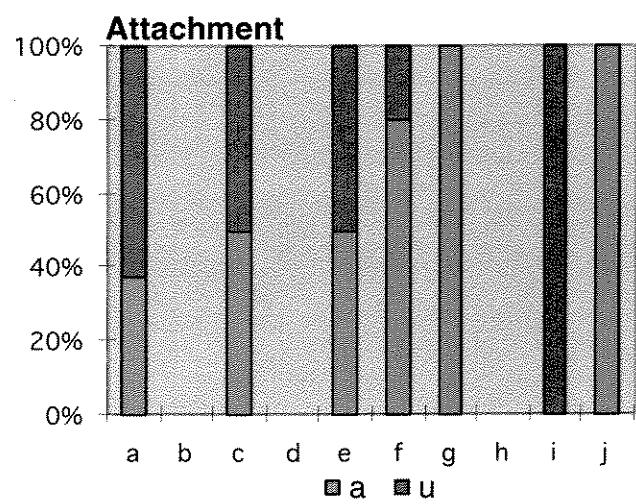
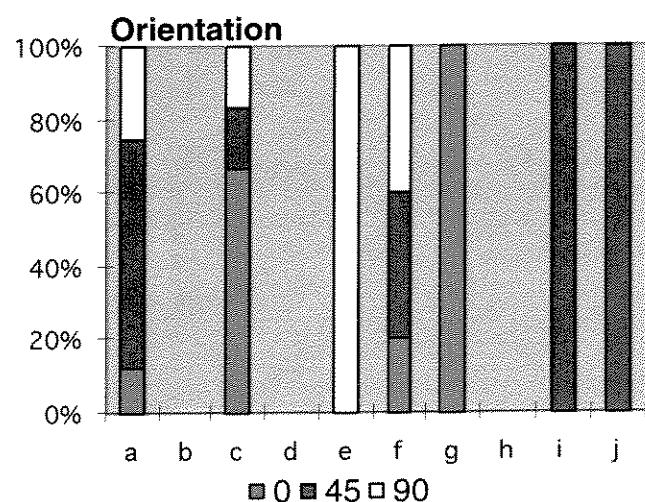
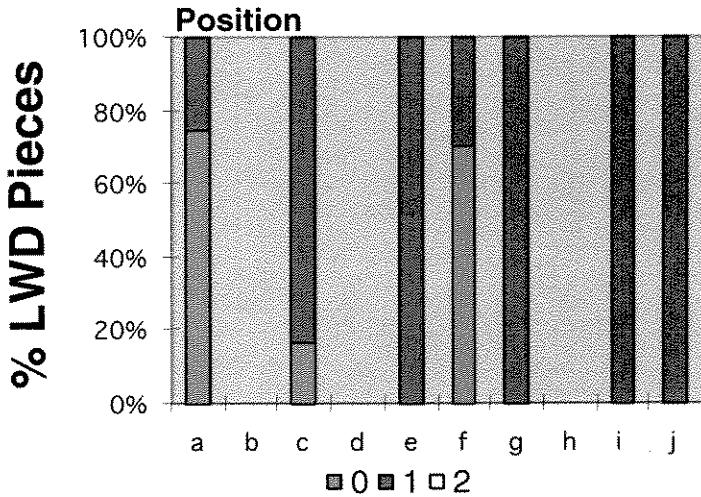
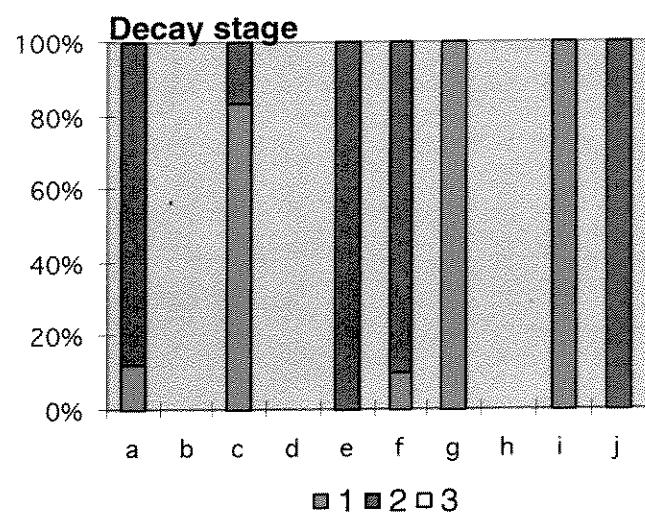
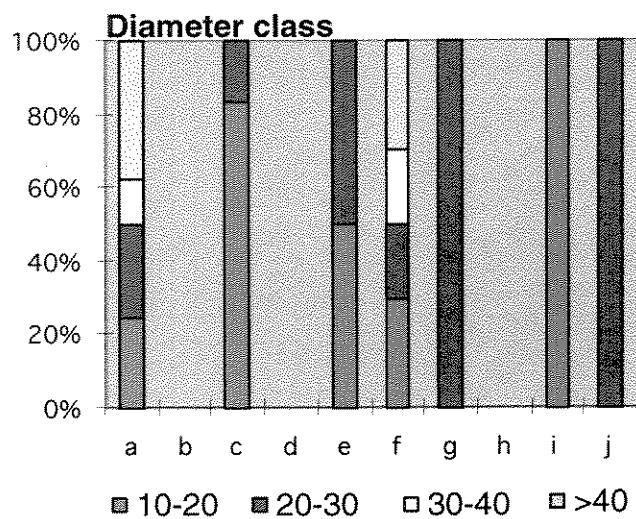
## Ole Creek reach b

A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



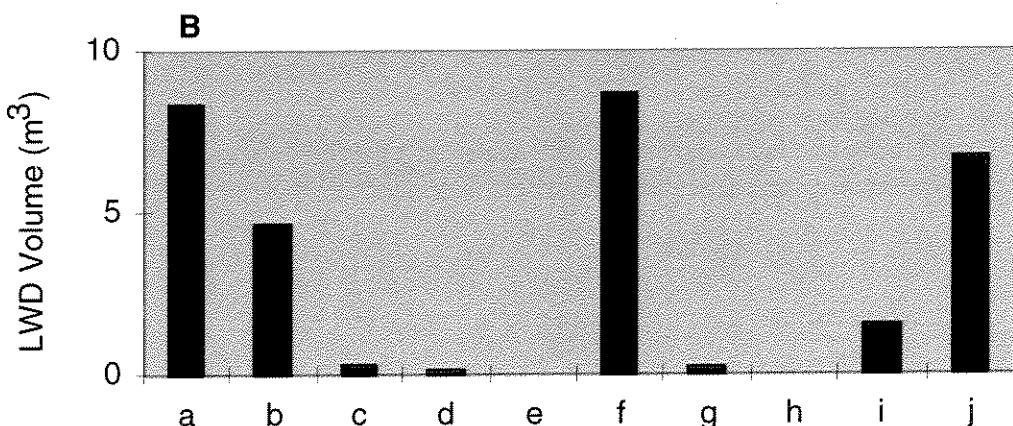
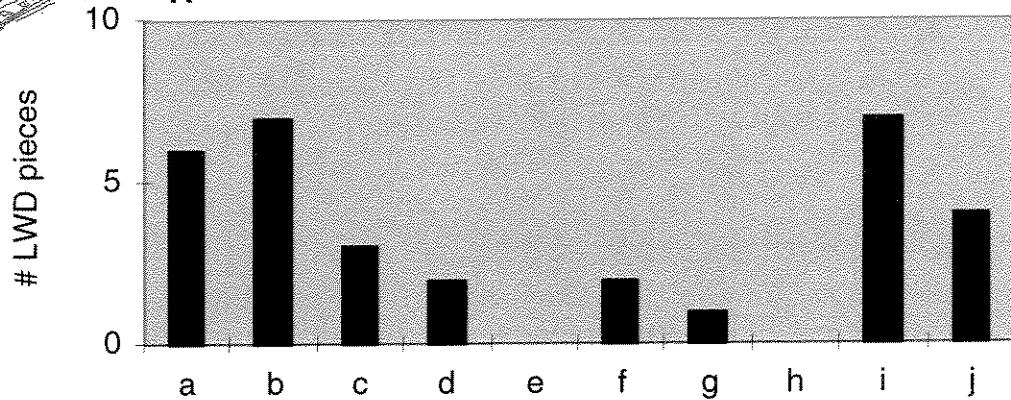
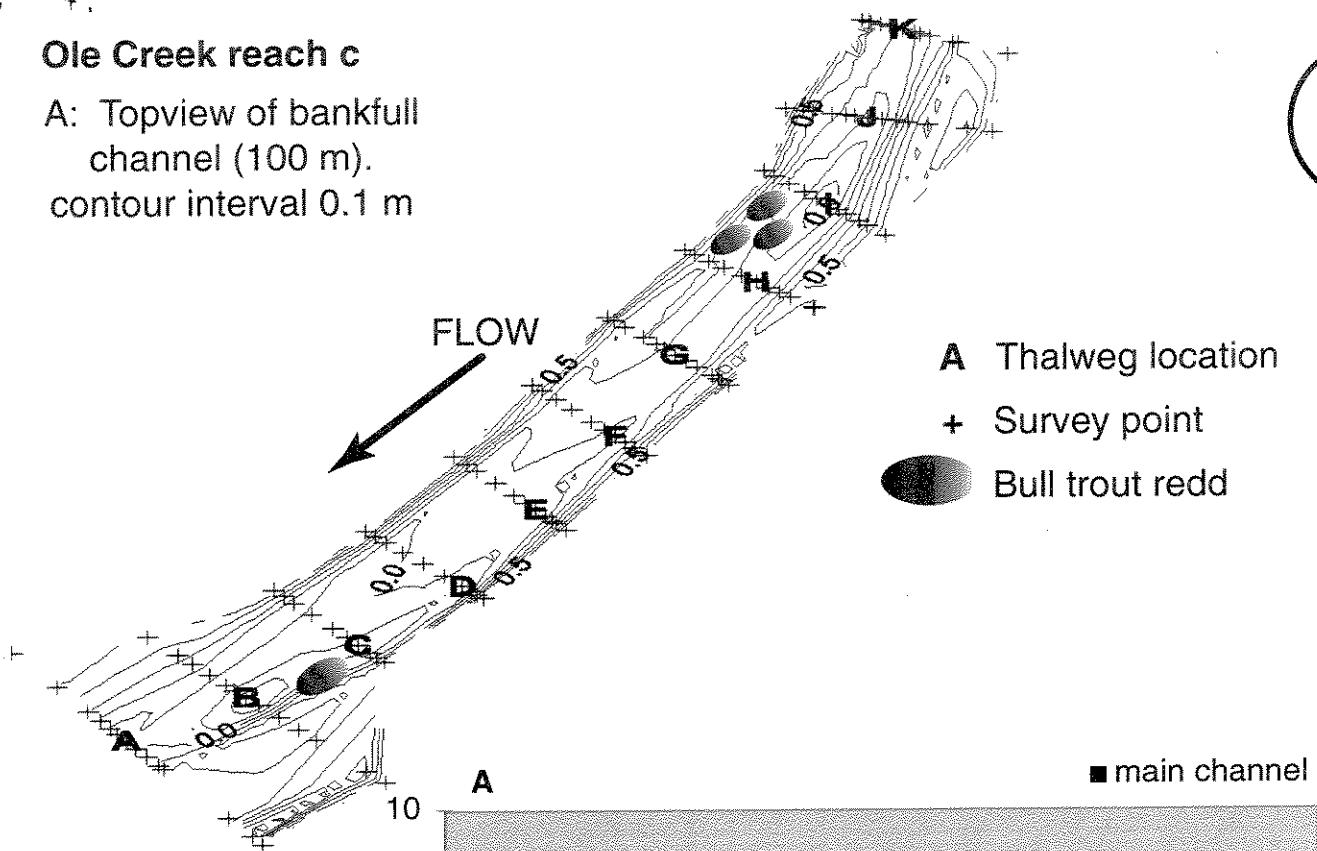
### Ole Creek Reach B



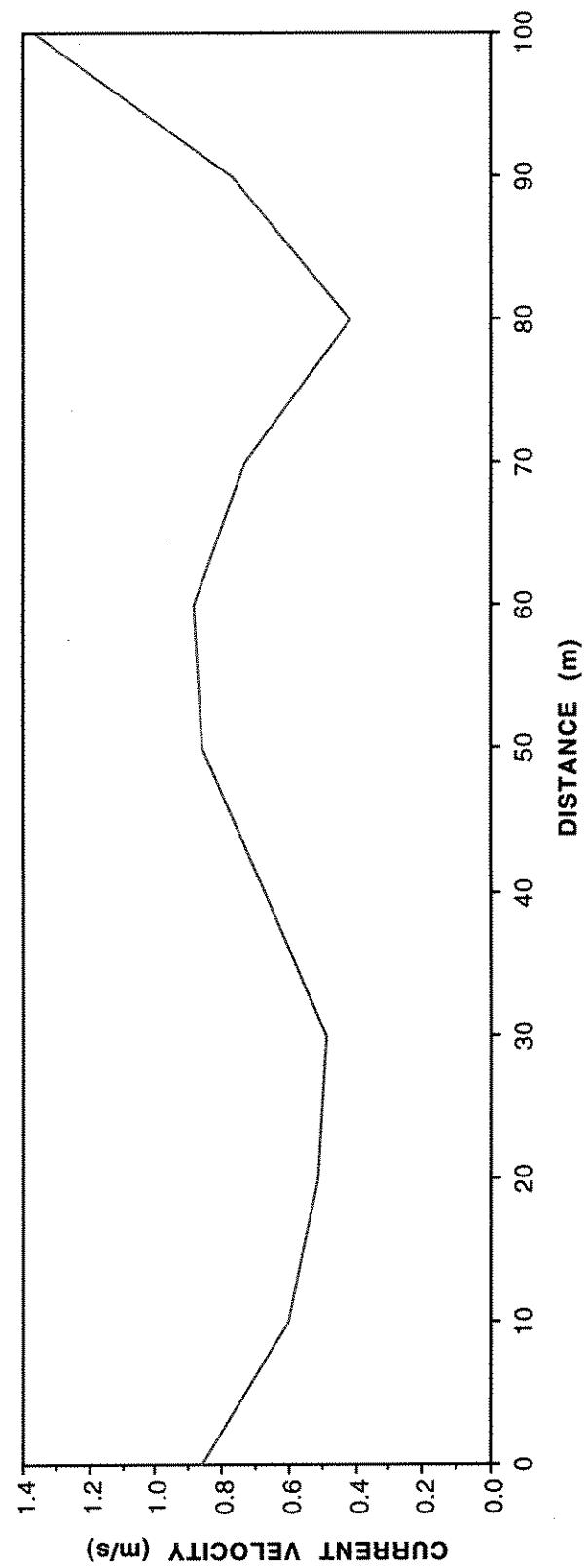
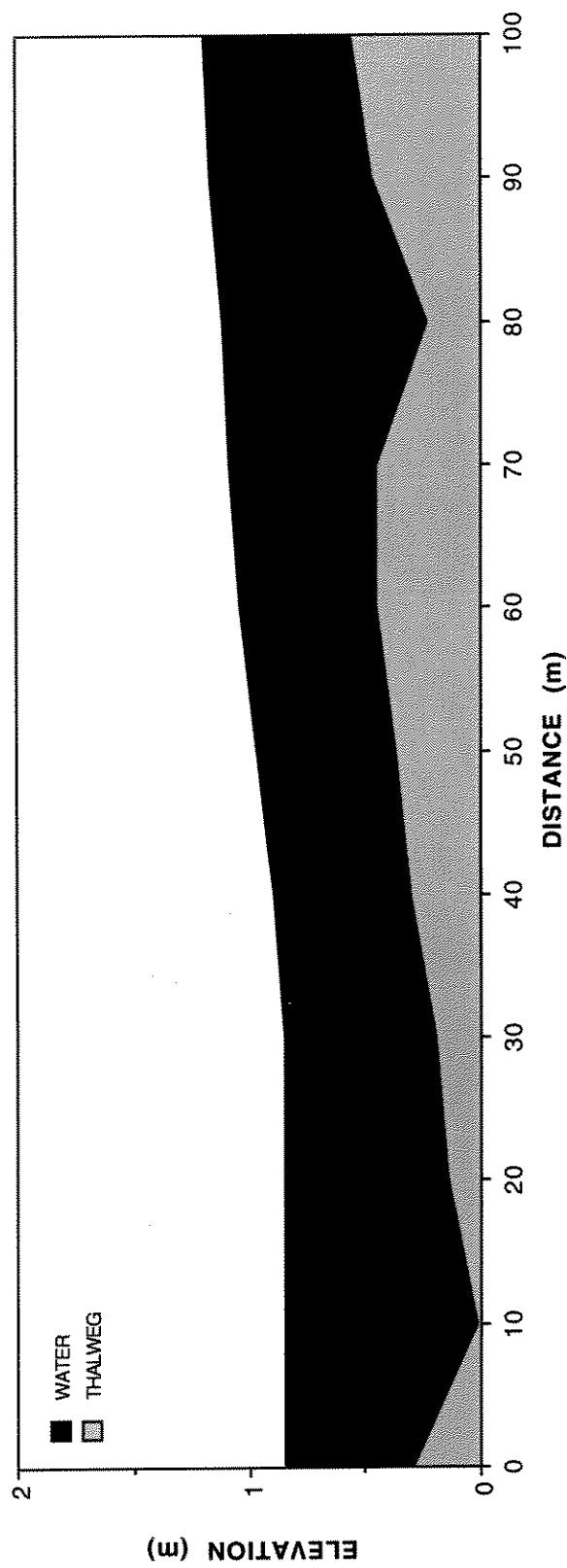


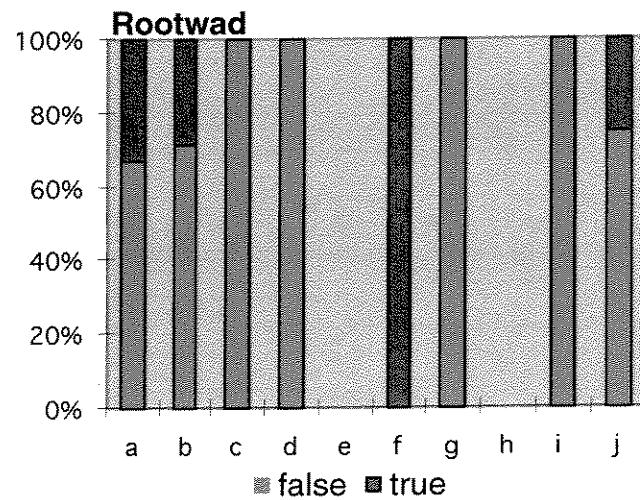
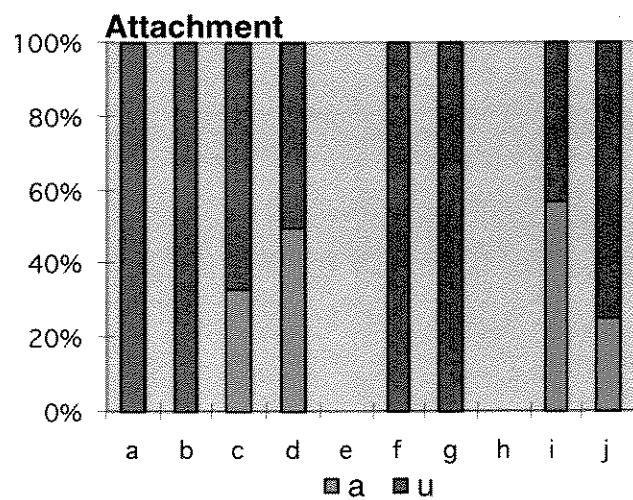
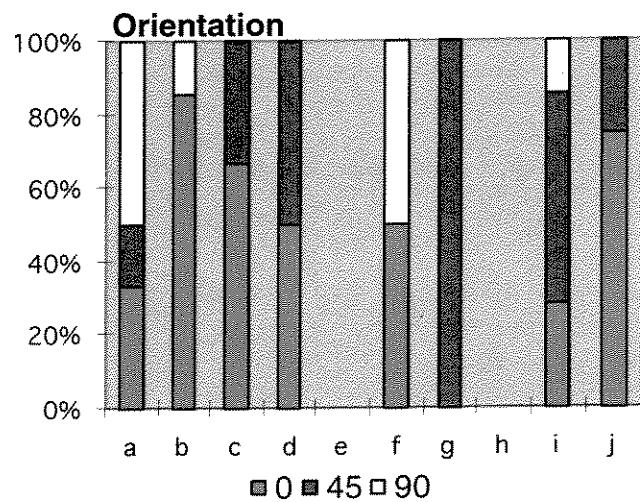
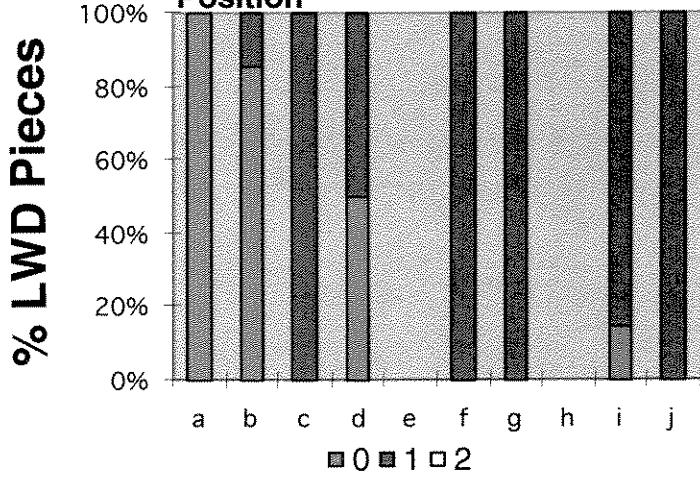
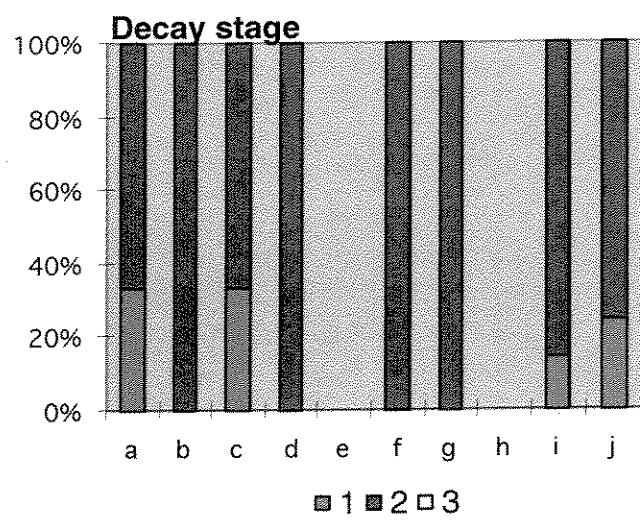
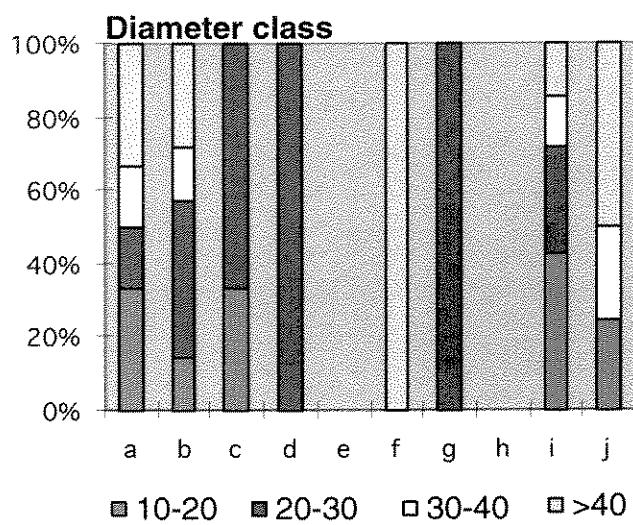
## Ole Creek reach c

A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



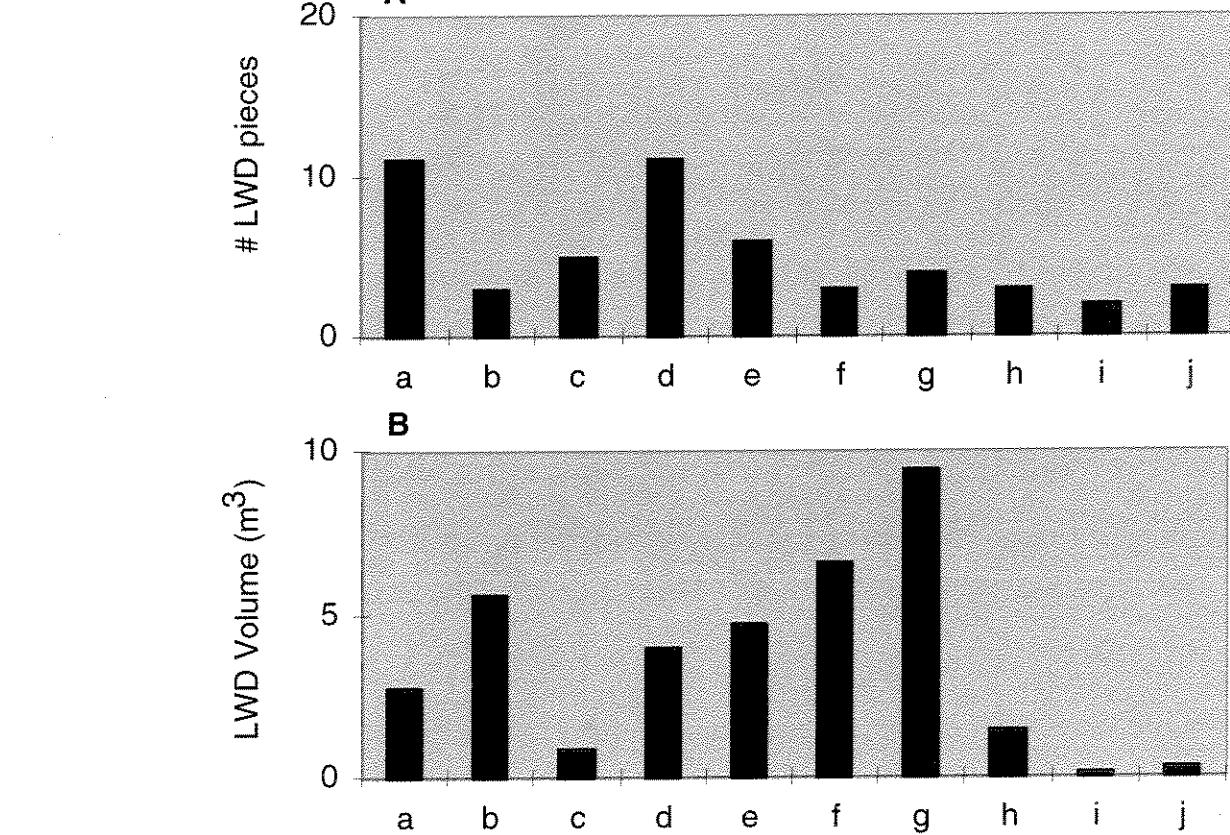
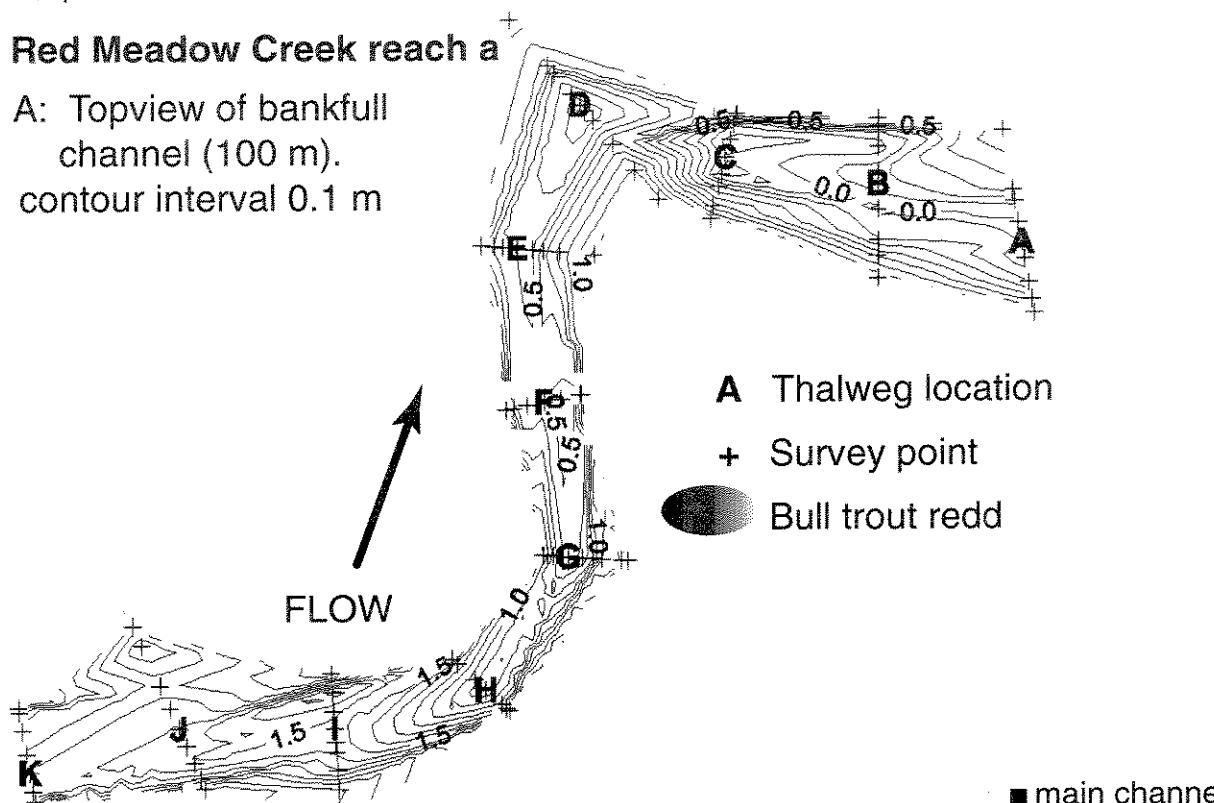
Ole Creek Reach C



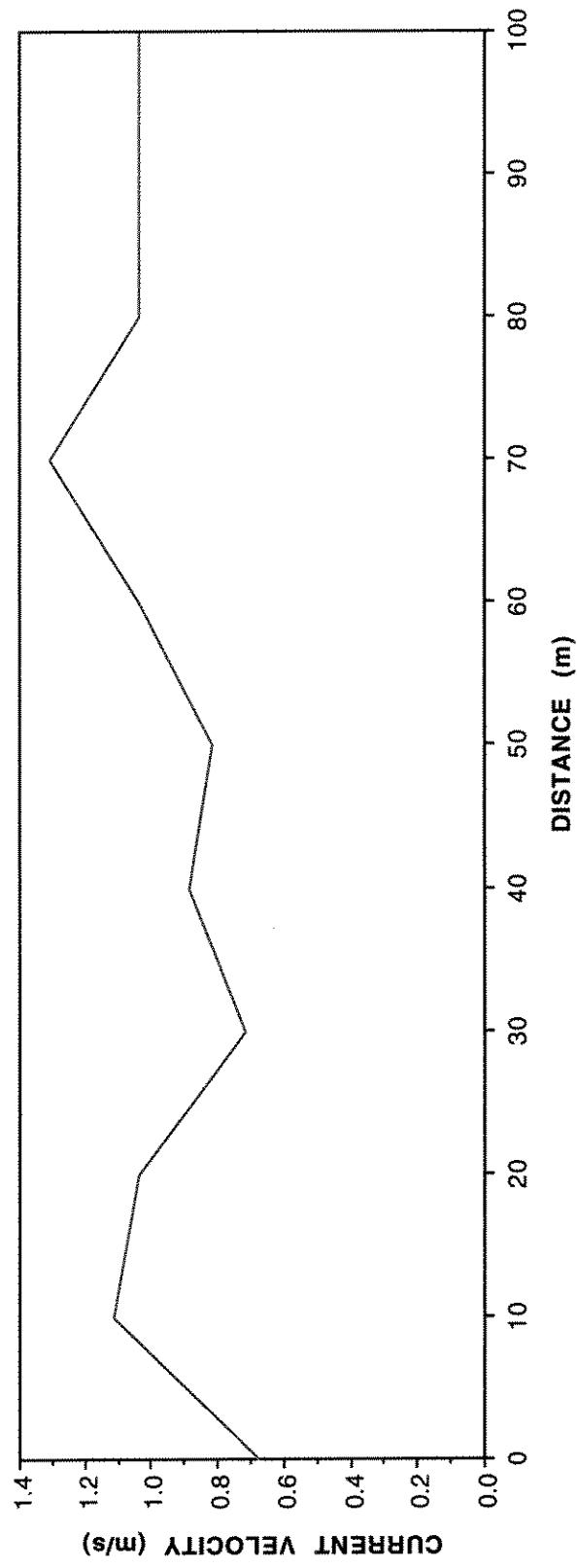
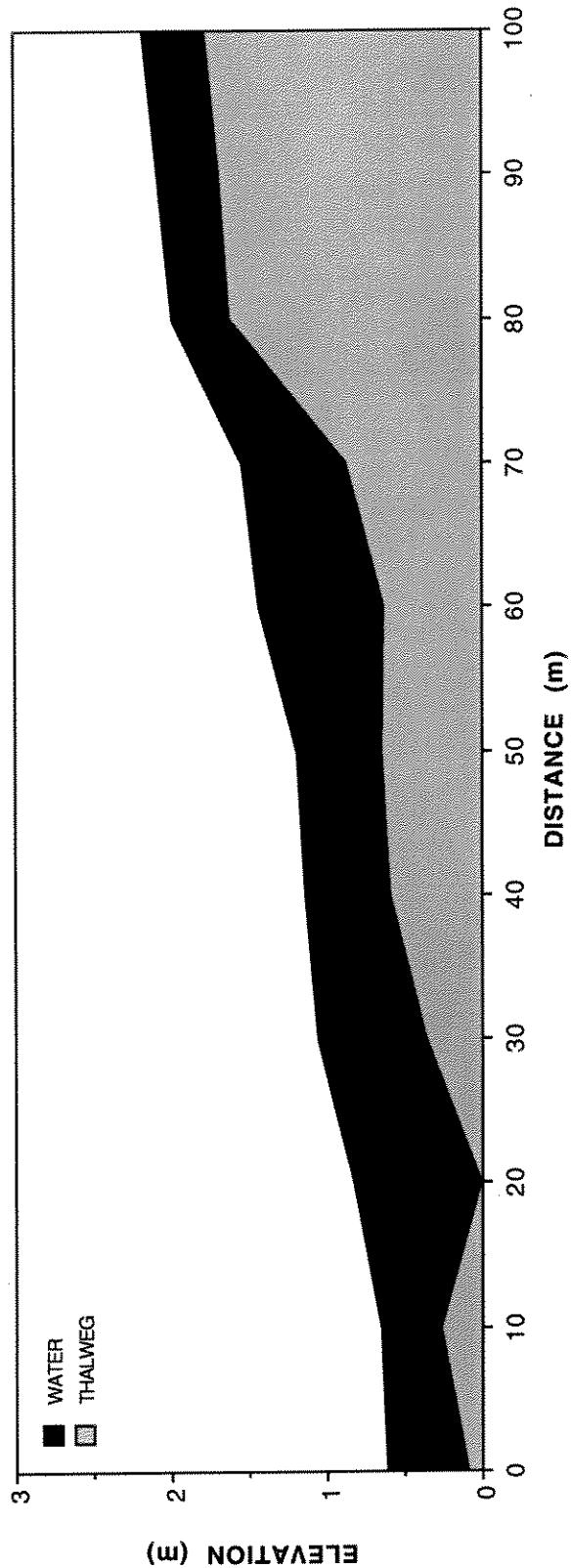


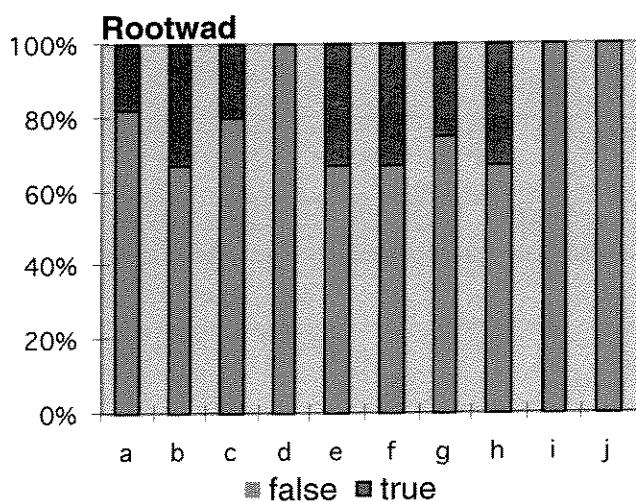
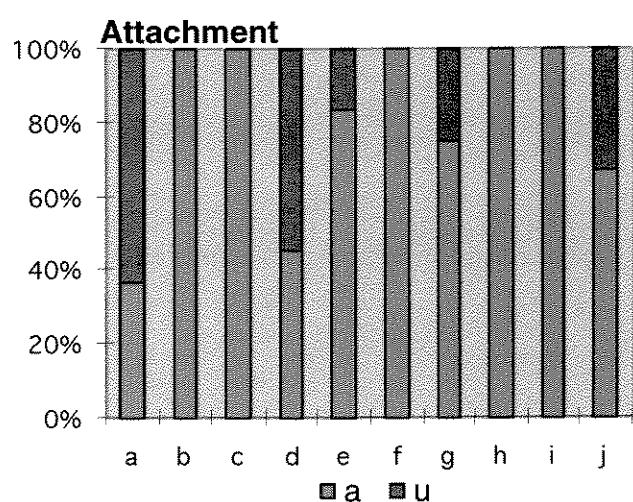
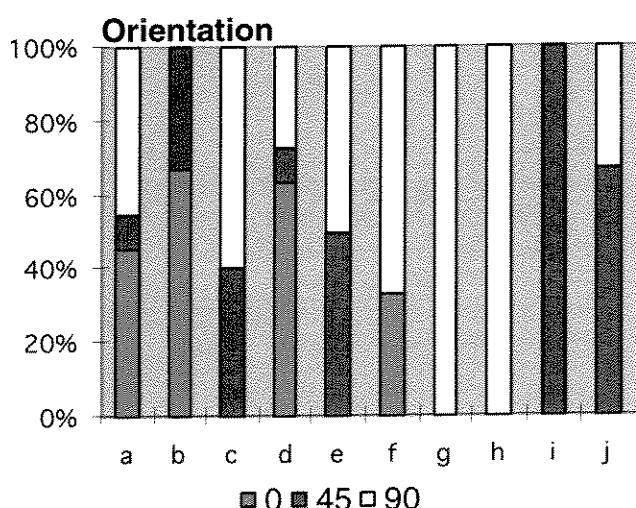
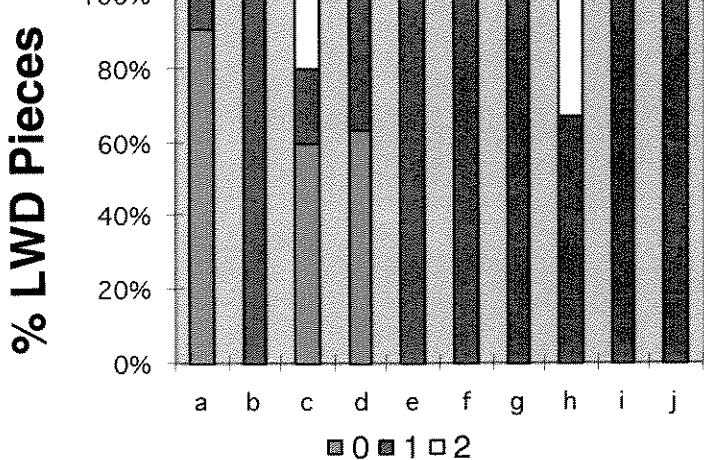
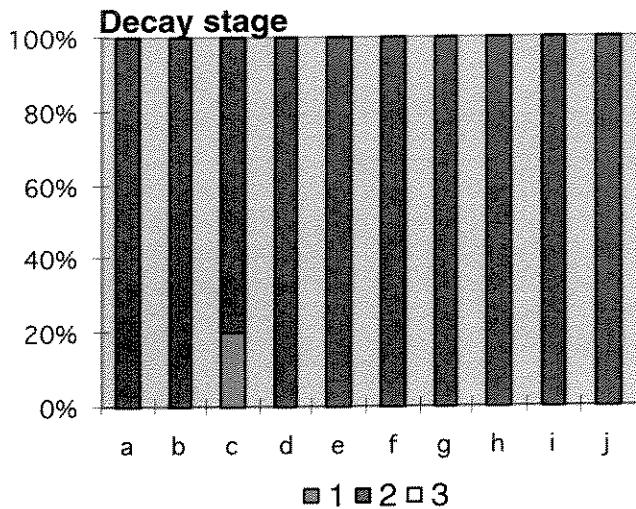
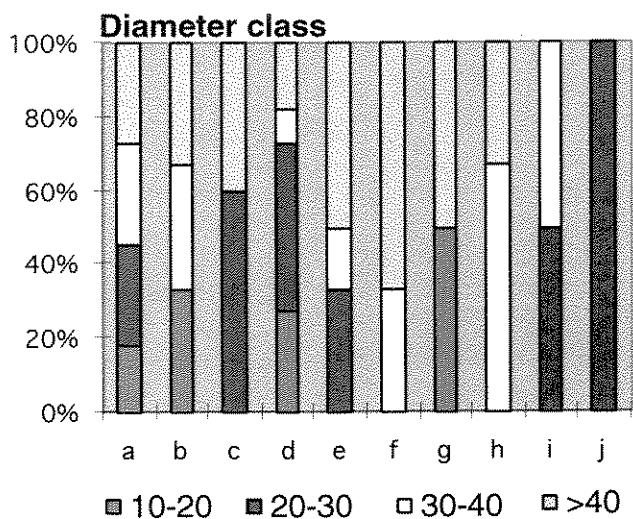
## Red Meadow Creek reach a

A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



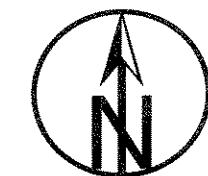
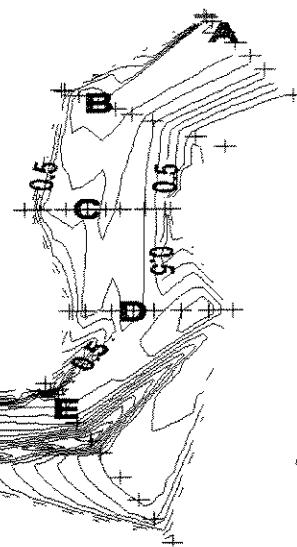
Red Meadow Creek Reach A





## Red Meadow Creek reach b

A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



- A Thalweg location
- + Survey point
- Bull trout redd

■ main channel

# LWD pieces

20  
0

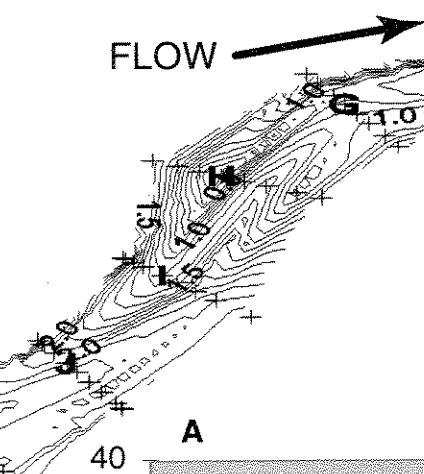
a b c d e f g h i j

B

LWD Volume ( $m^3$ )

40  
20  
0

a b c d e f g h i j



K

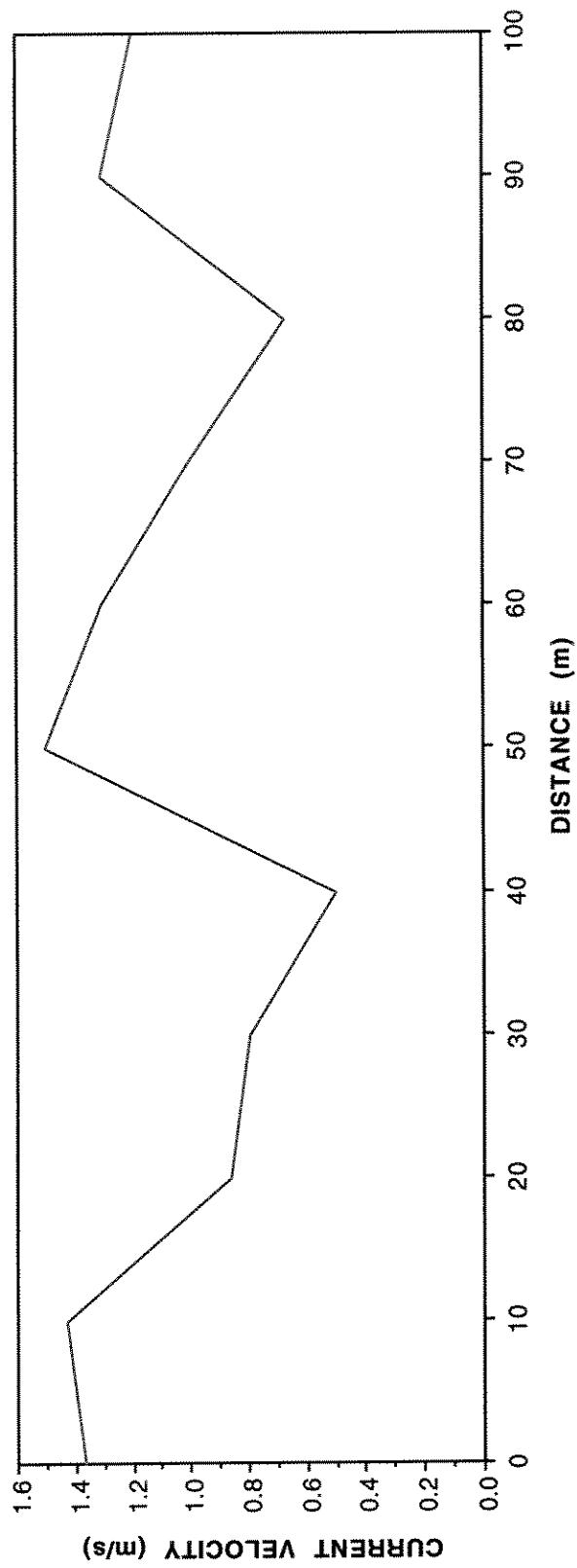
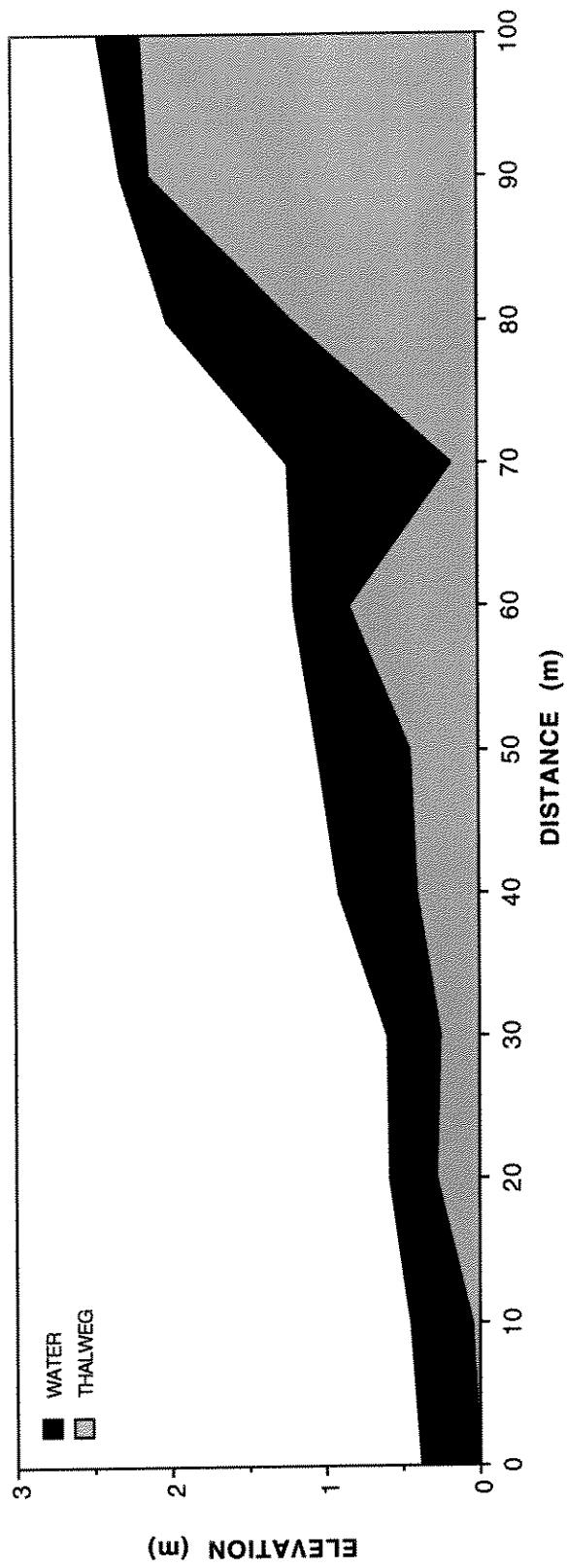
40

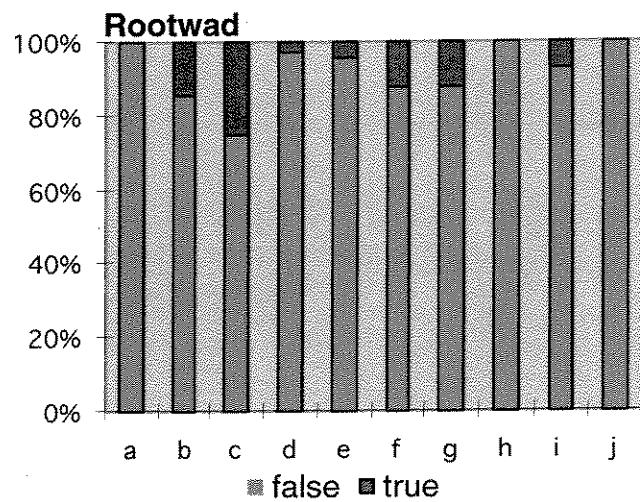
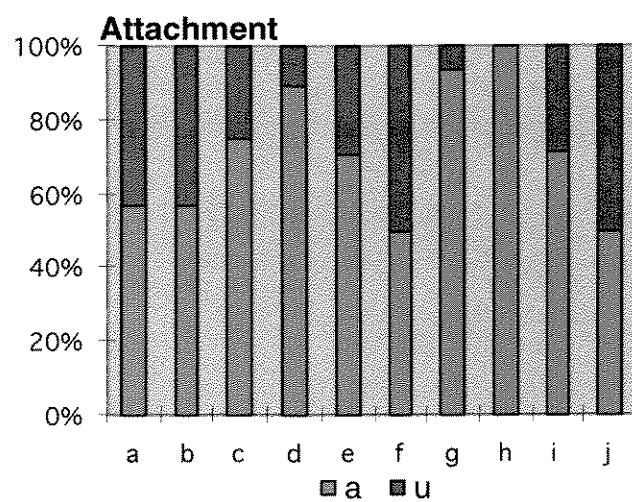
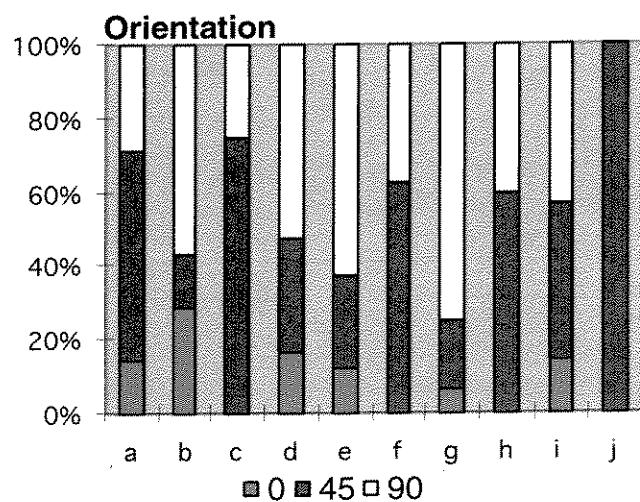
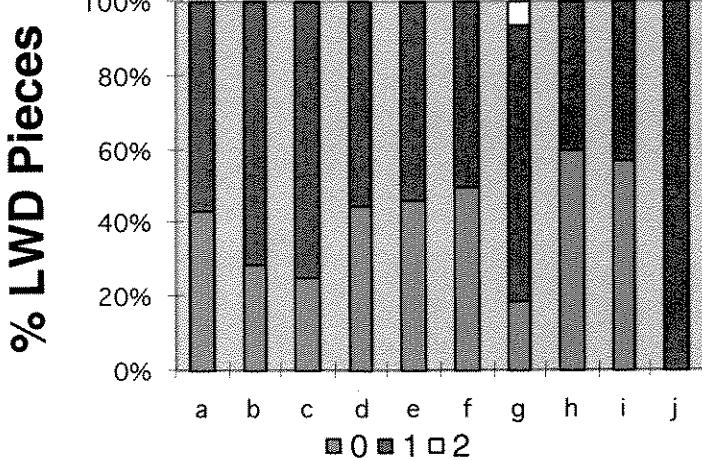
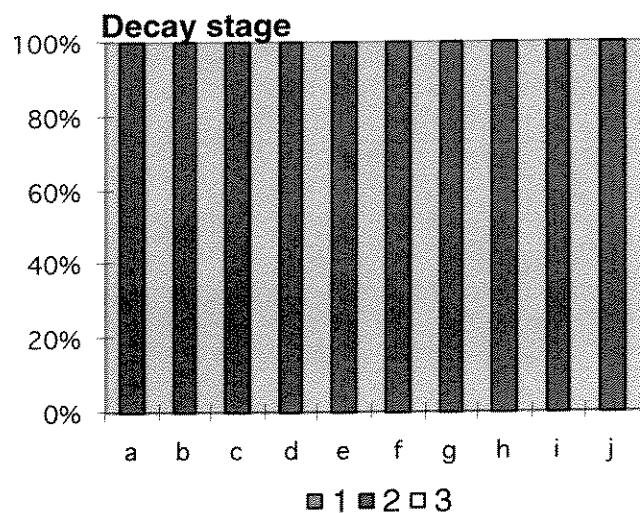
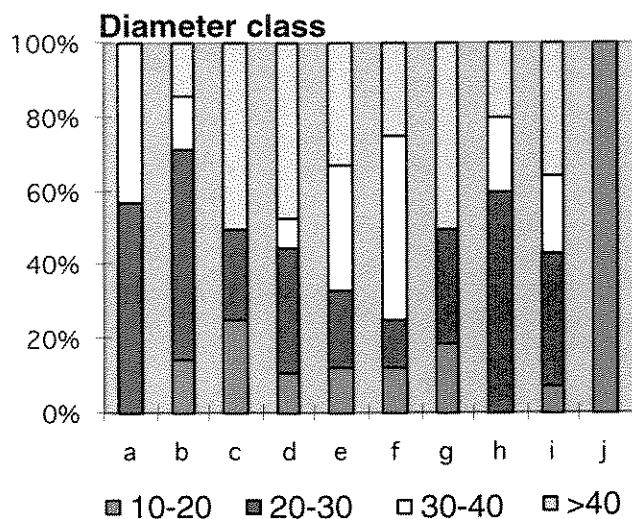
A

40  
20  
0

B

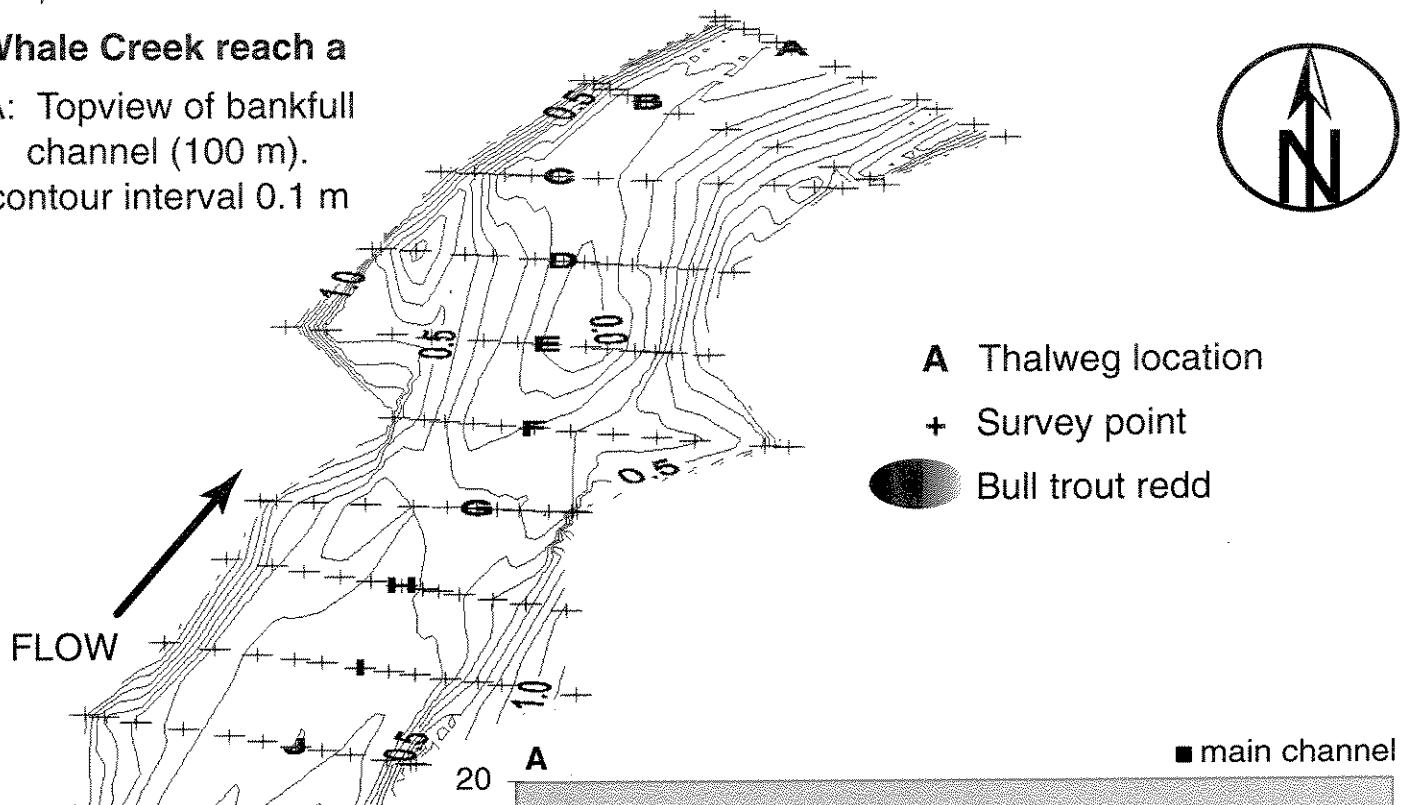
Red Meadow Creek Reach B





## Whale Creek reach a

A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



**A** Thalweg location

+

 Survey point

Bull trout redd

■ main channel

# LWD pieces

10  
0

a b c d e f g h i j

**B**

LWD Volume ( $m^3$ )

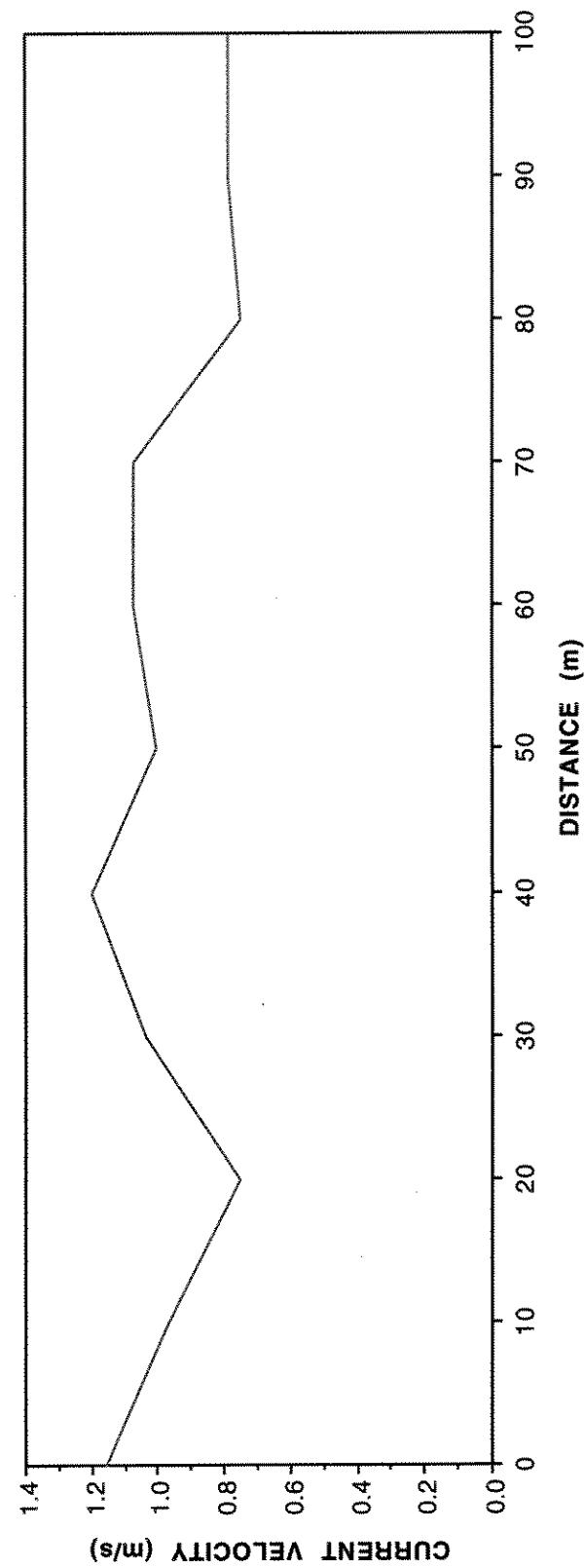
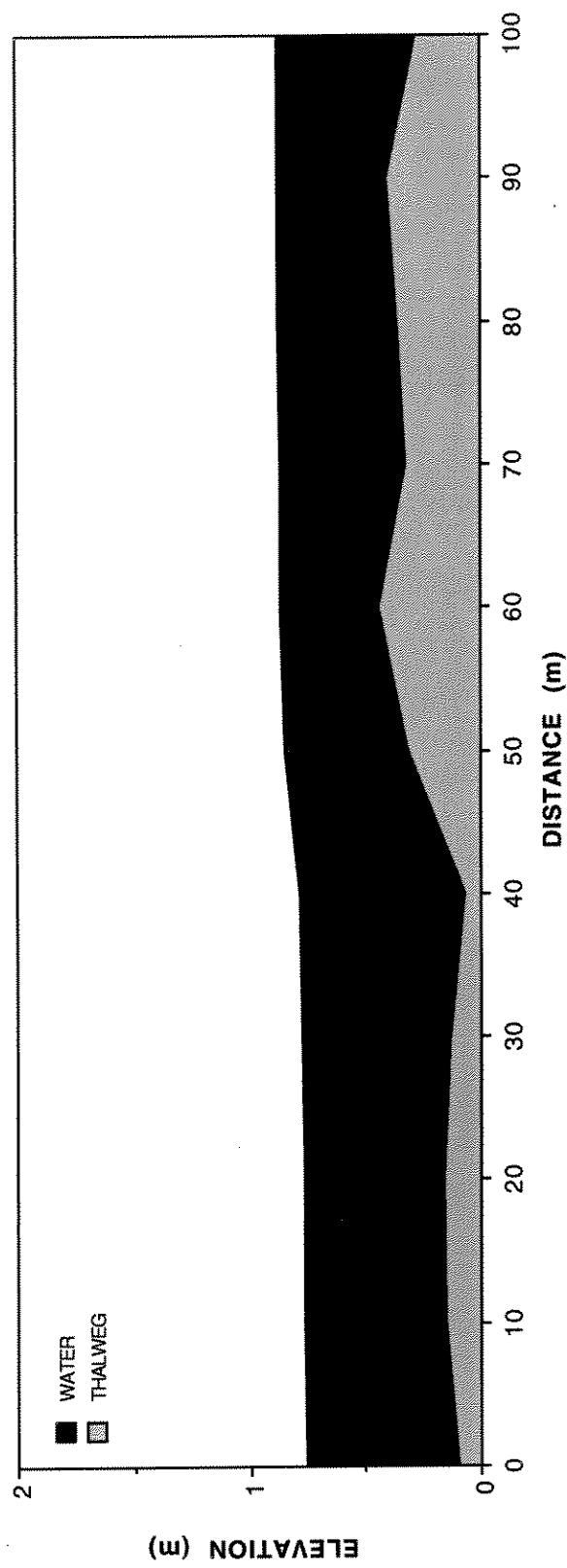
10  
5  
0

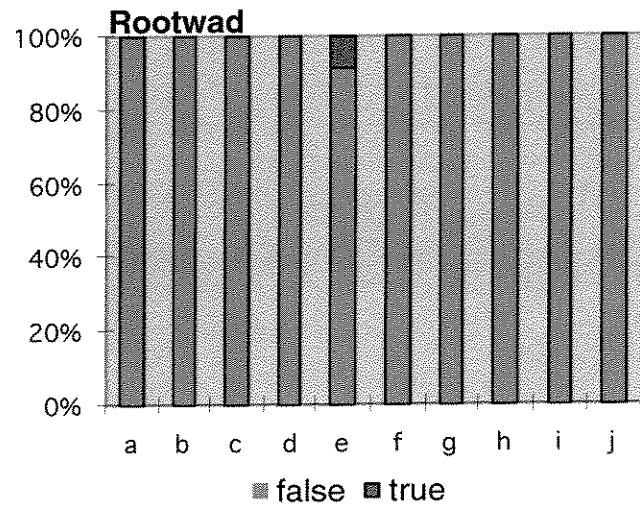
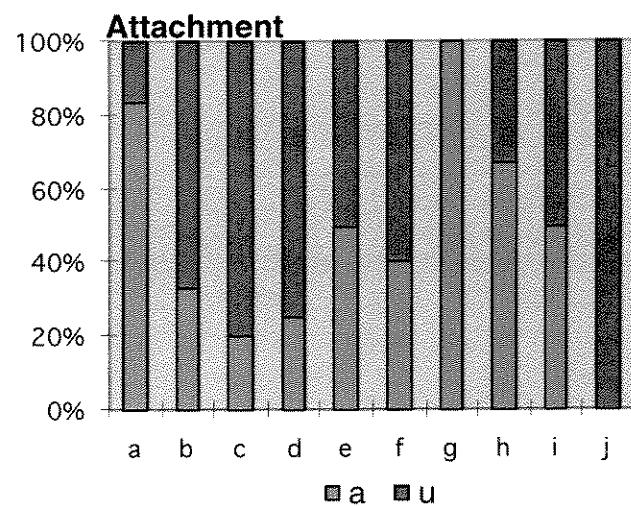
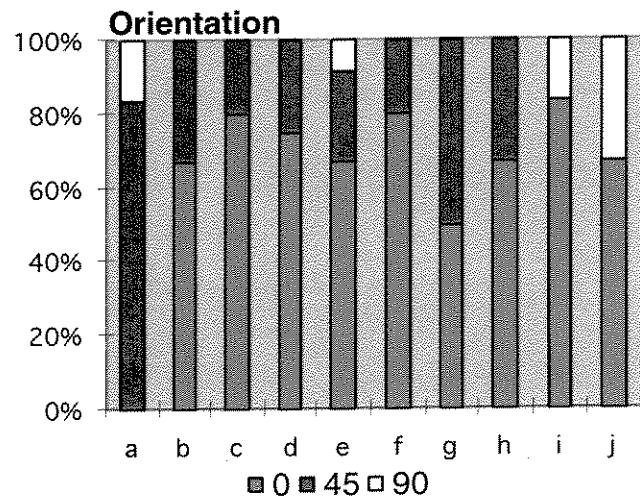
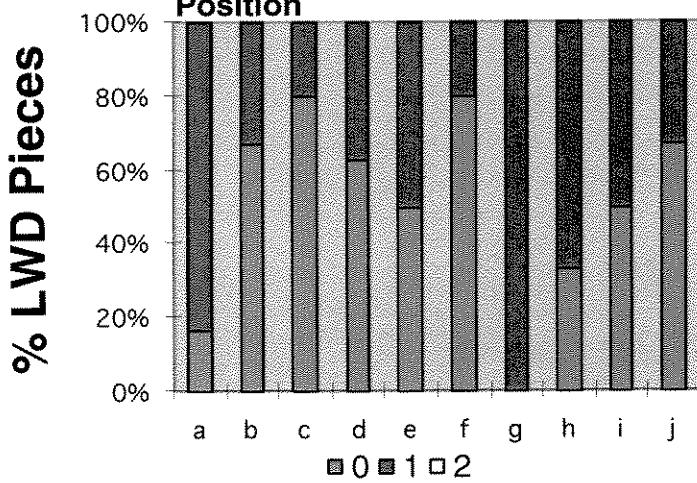
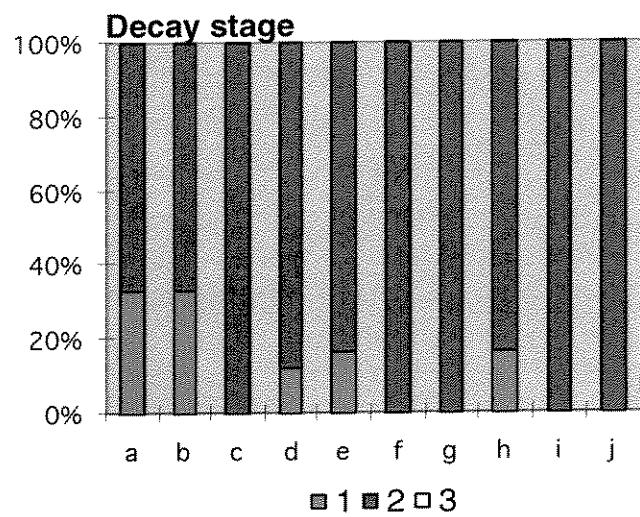
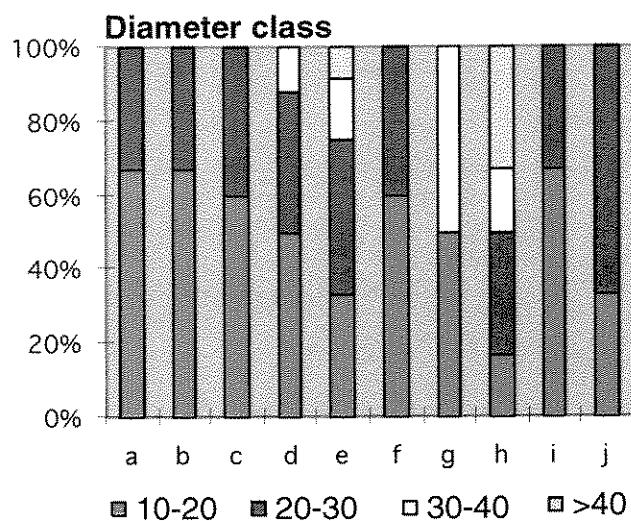
a b c d e f g h i j

■ main channel

2  
1  
0

**Whale Creek Reach A**





## Whale Creek reach b

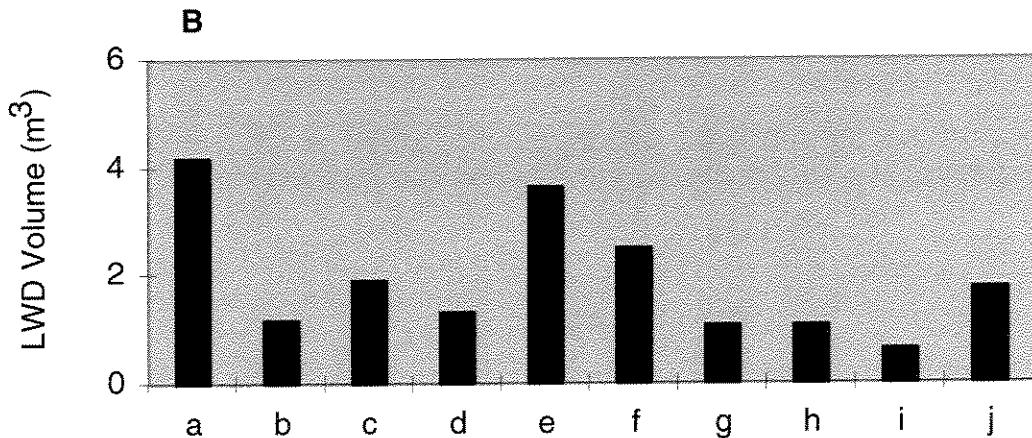
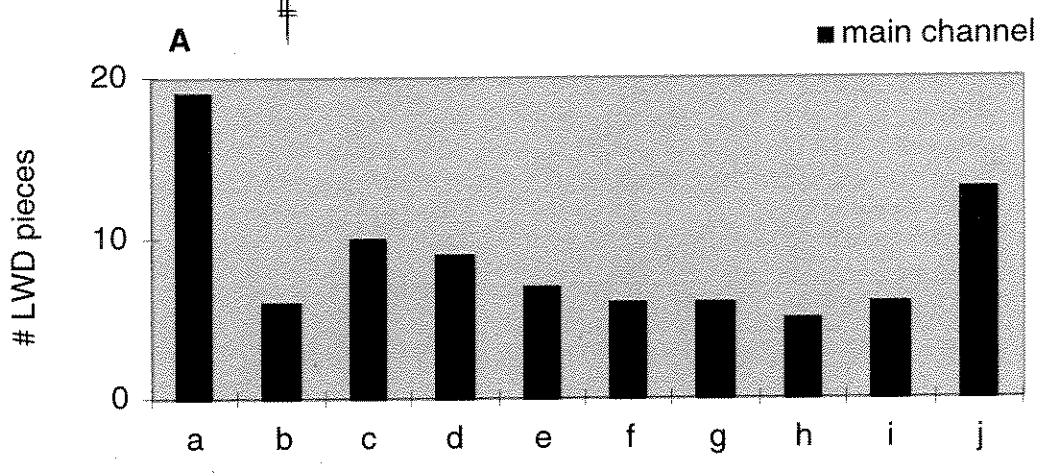
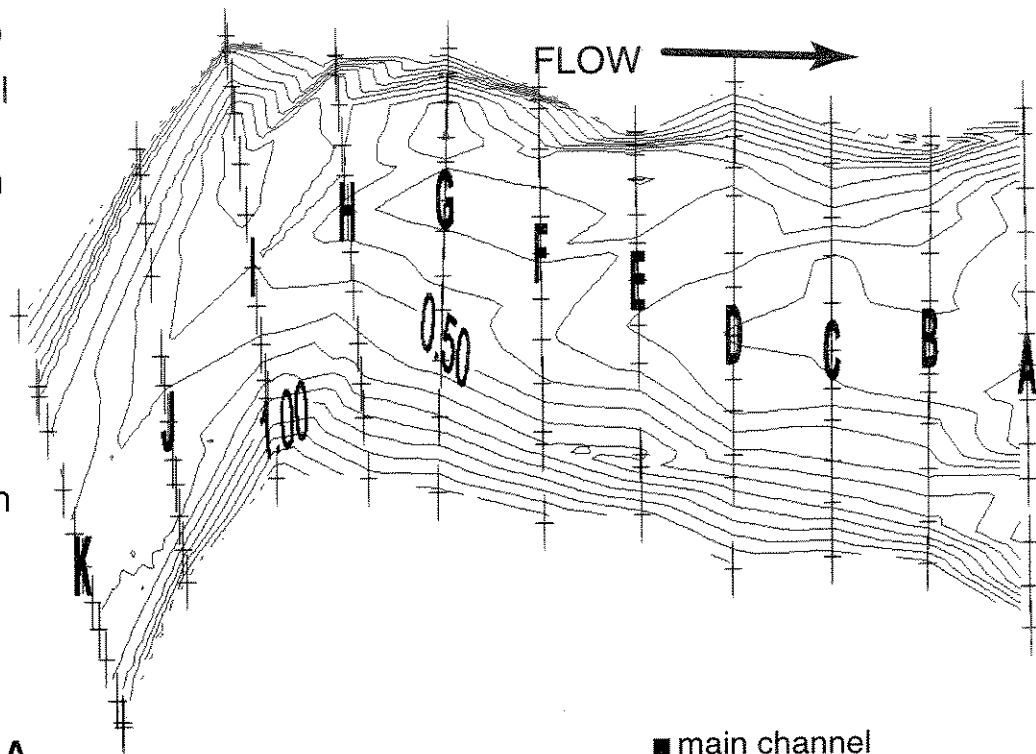
A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



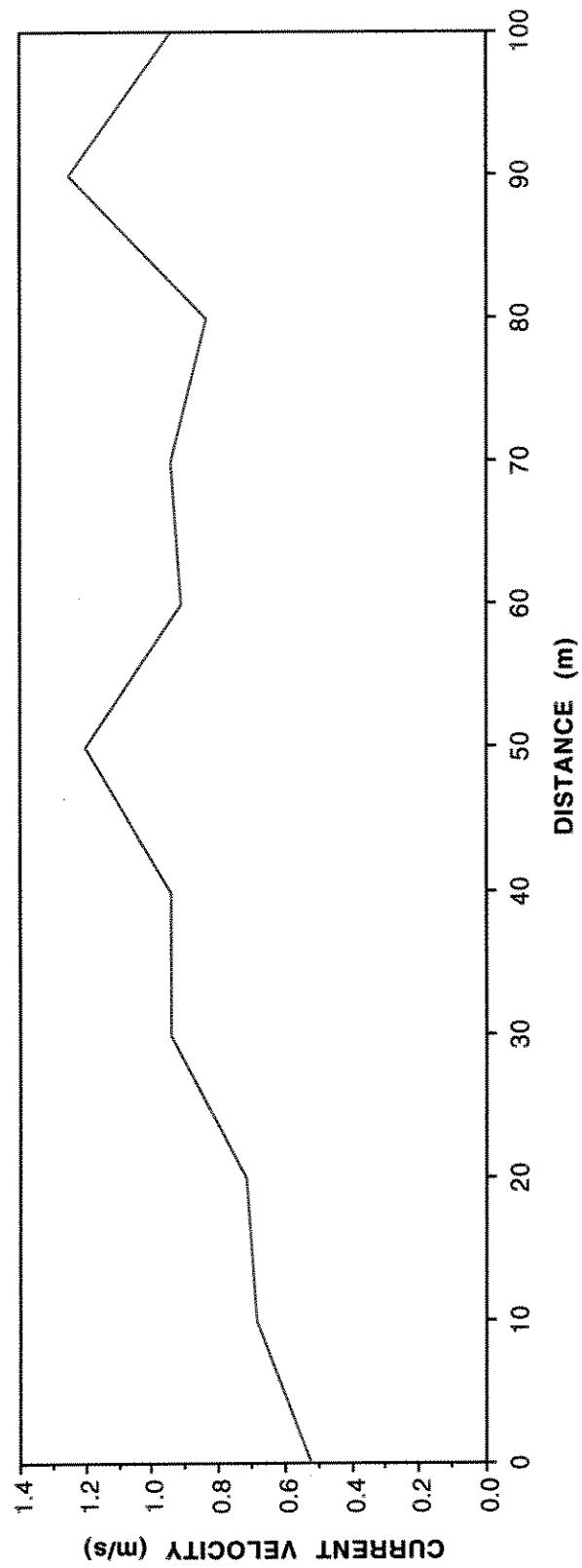
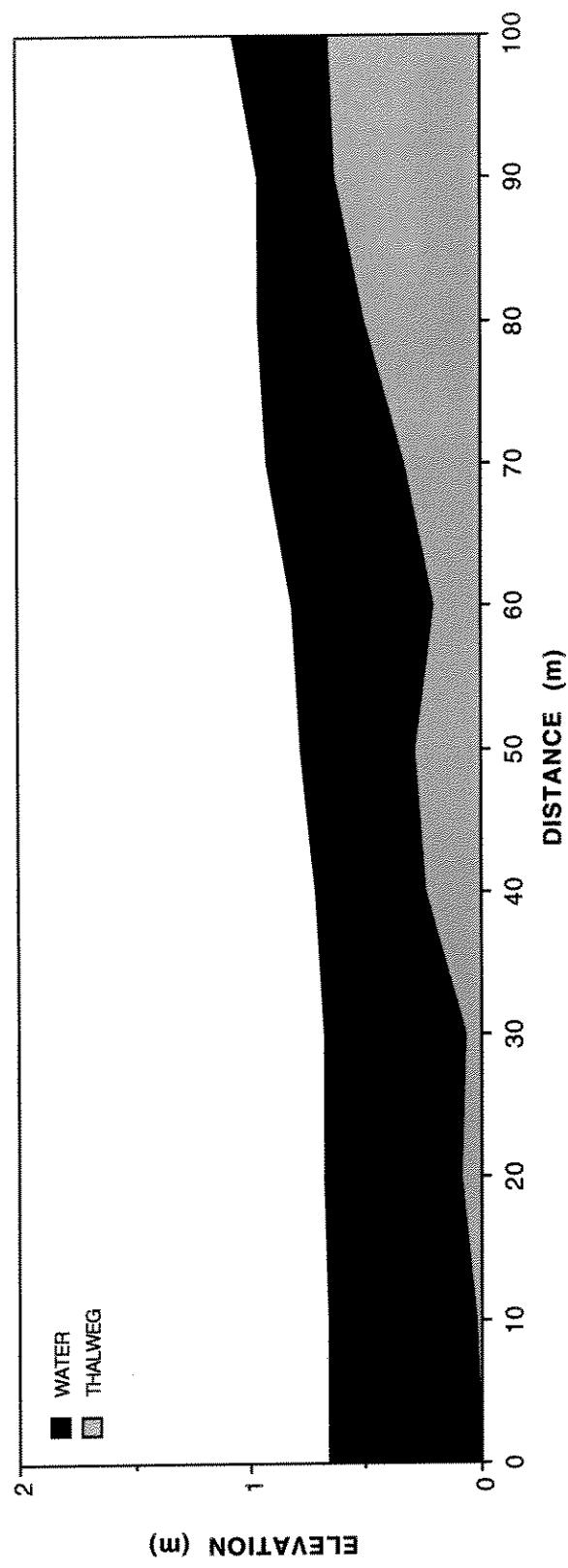
A Thalweg location

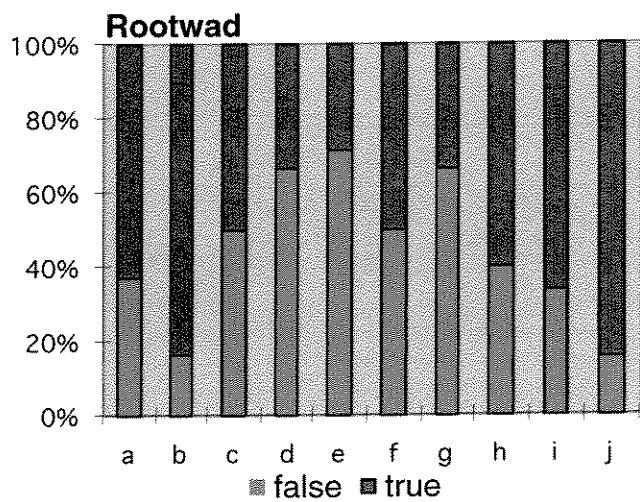
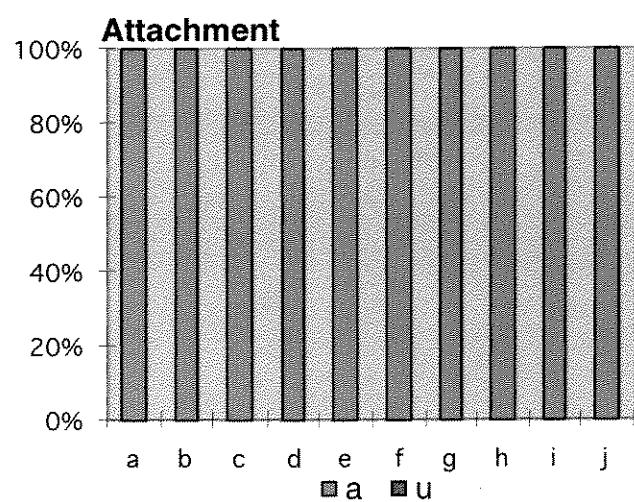
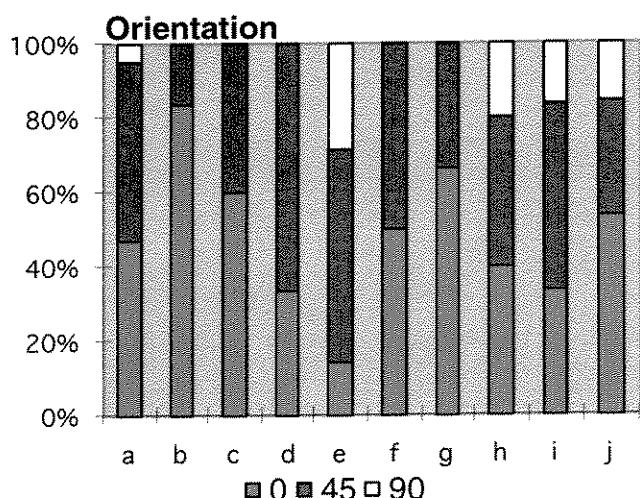
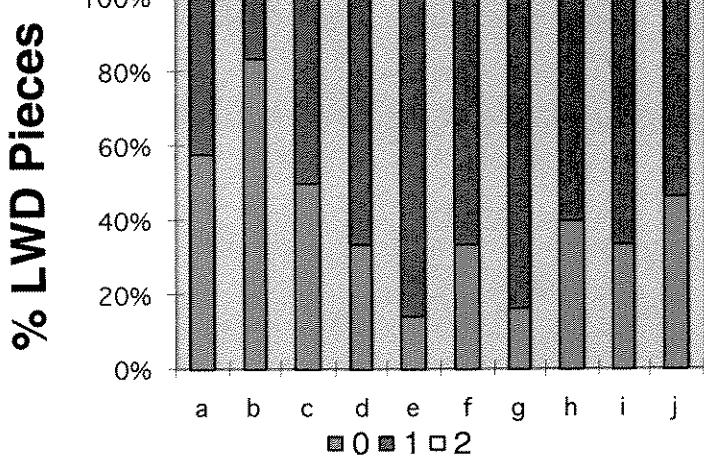
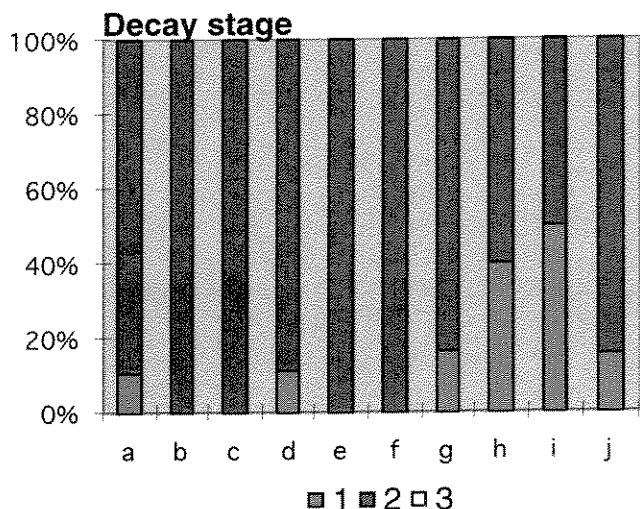
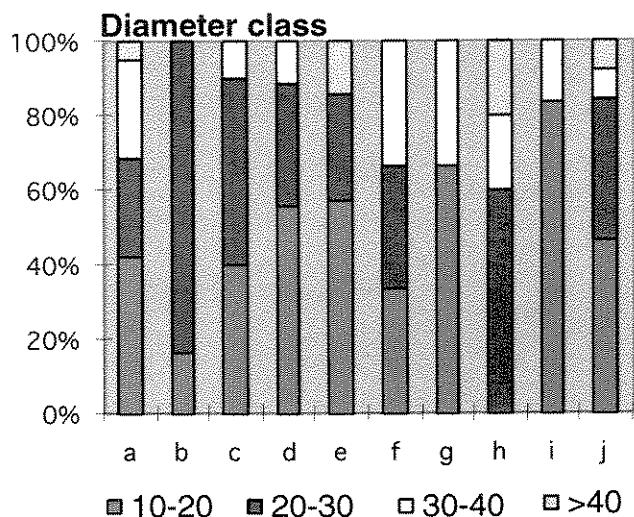
+ Survey point

Bull trout redd



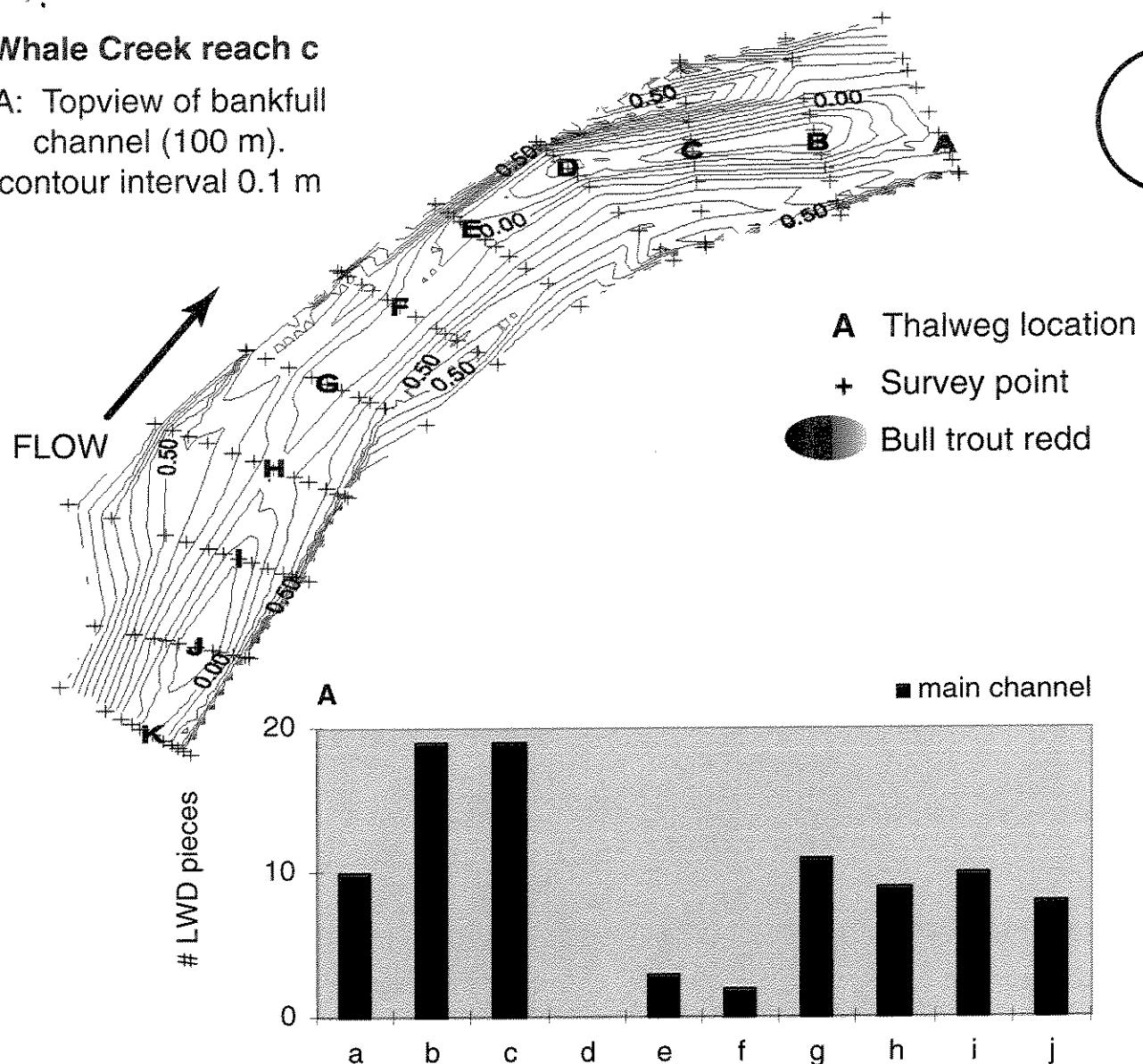
Whale Creek Reach B





## Whale Creek reach c

A: Topview of bankfull channel (100 m).  
channel (100 m).  
contour interval 0.1 m



■ main channel

# LWD pieces

20  
10  
0

a b c d e f g h i j

LWD Volume ( $m^3$ )

20  
10  
0

a b c d e f g h i j

FLOW

A

B

LWD Volume ( $m^3$ )

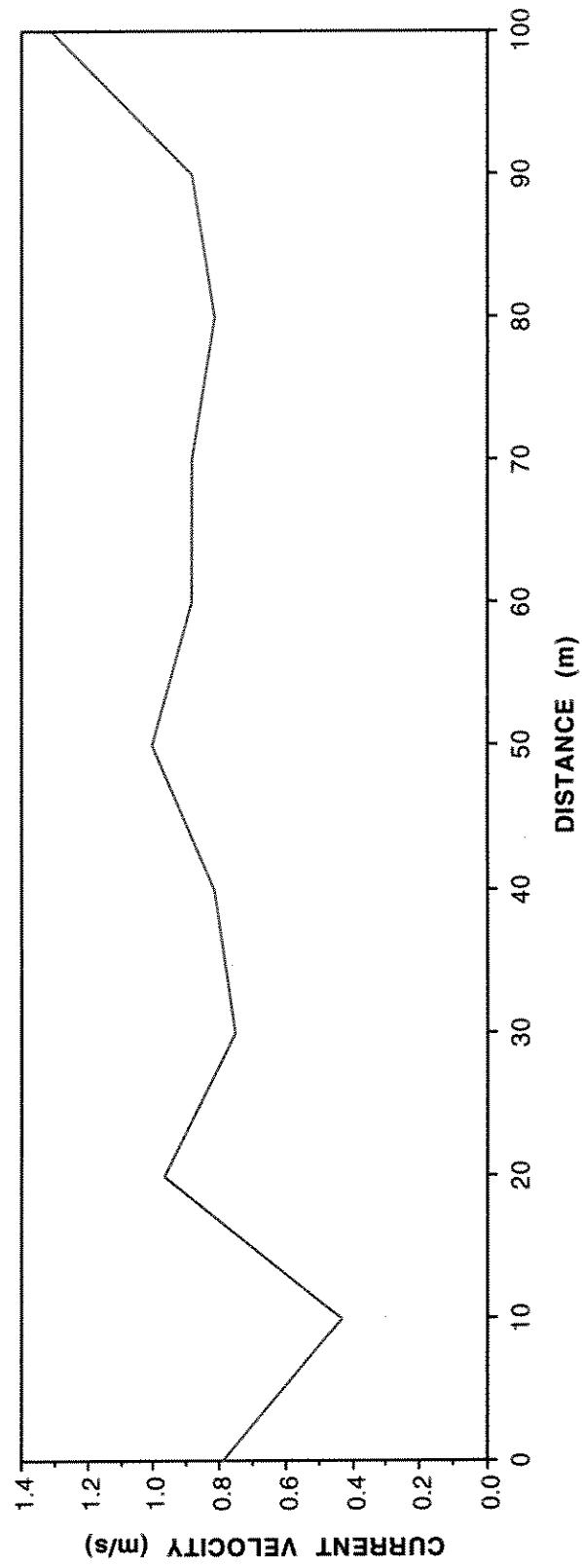
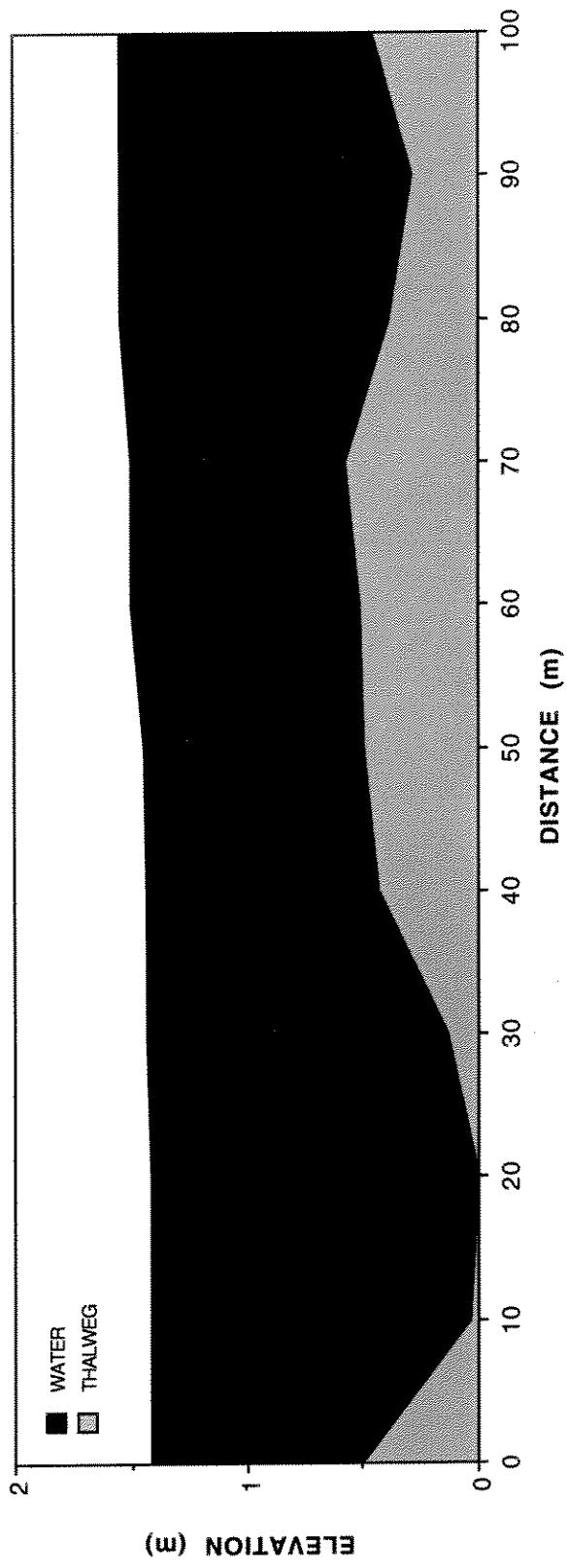
20  
10  
0

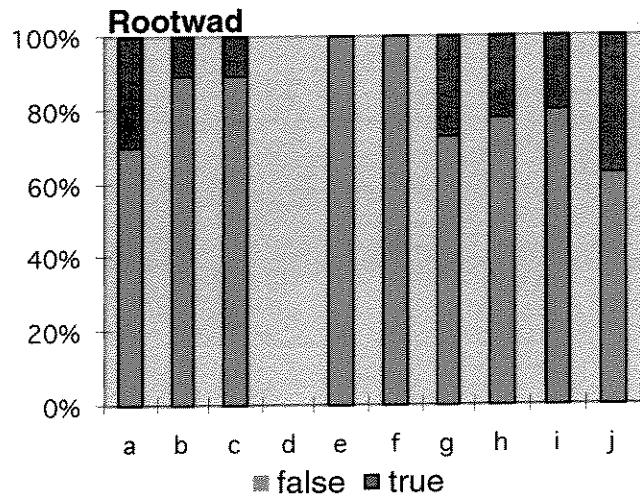
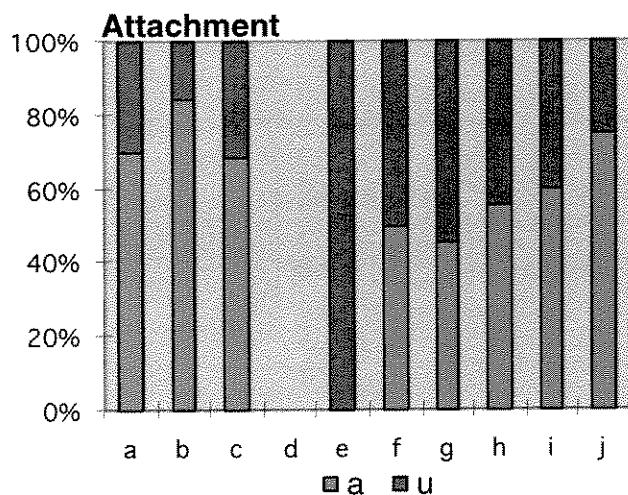
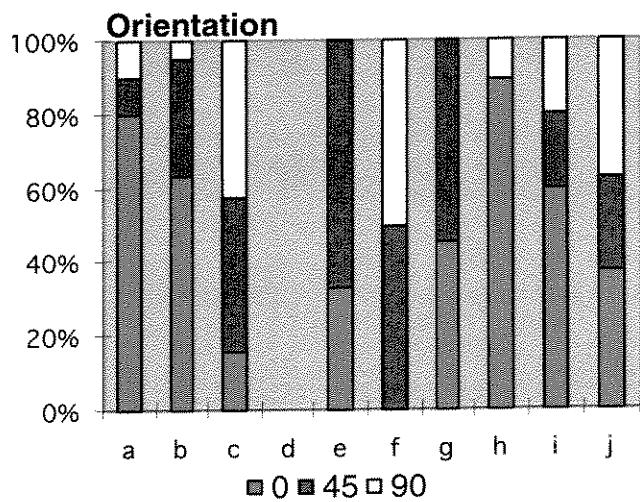
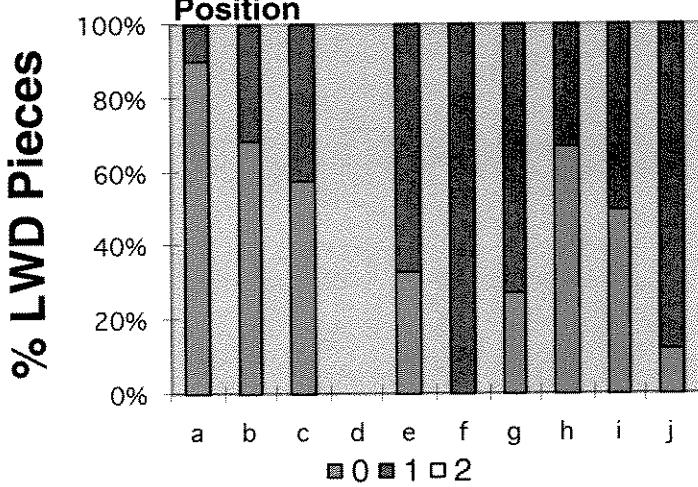
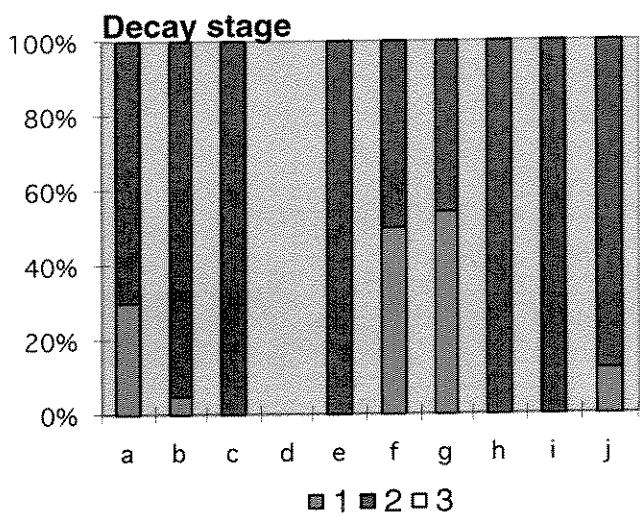
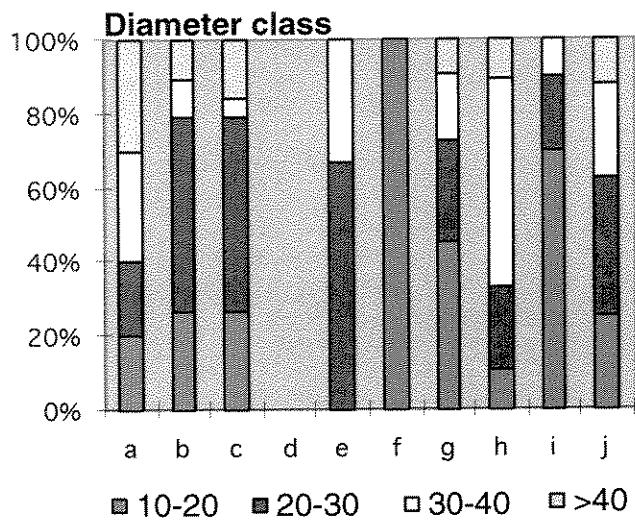
a b c d e f g h i j

A

B

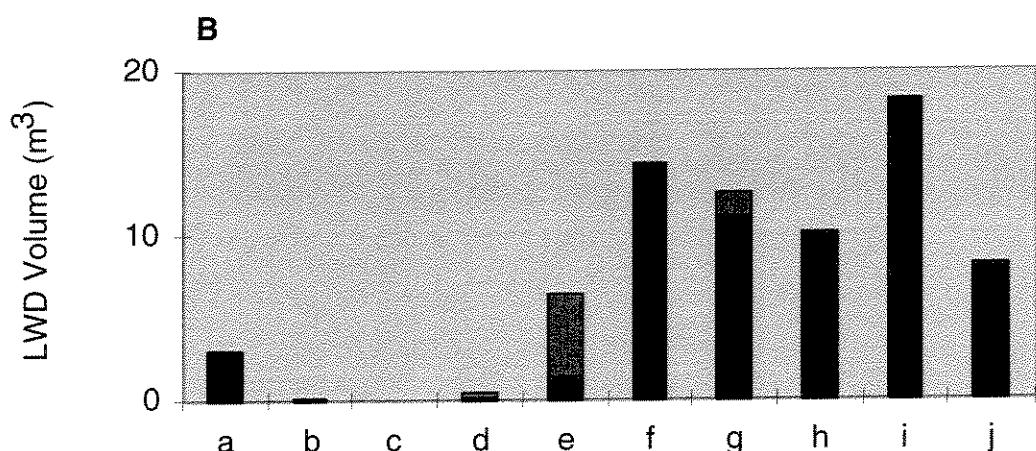
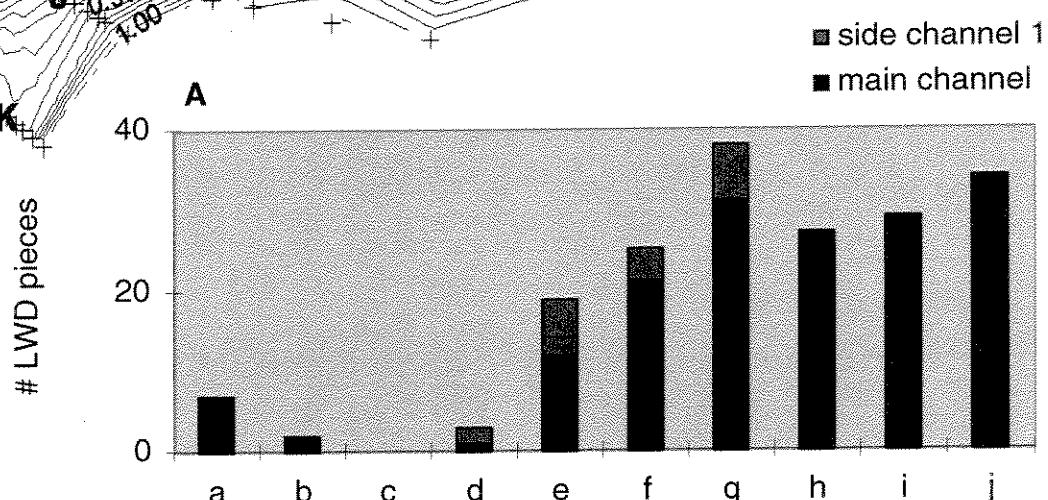
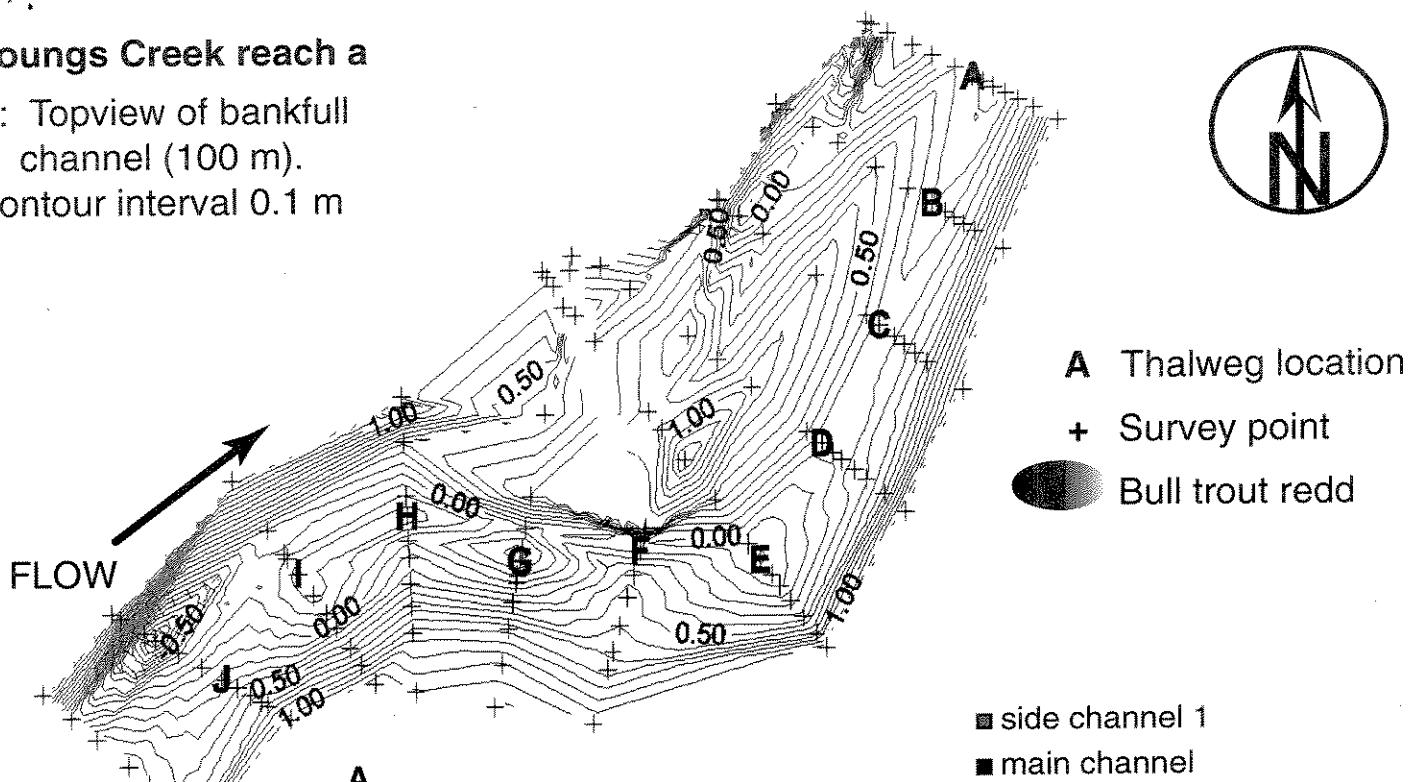
Whale Creek Reach C



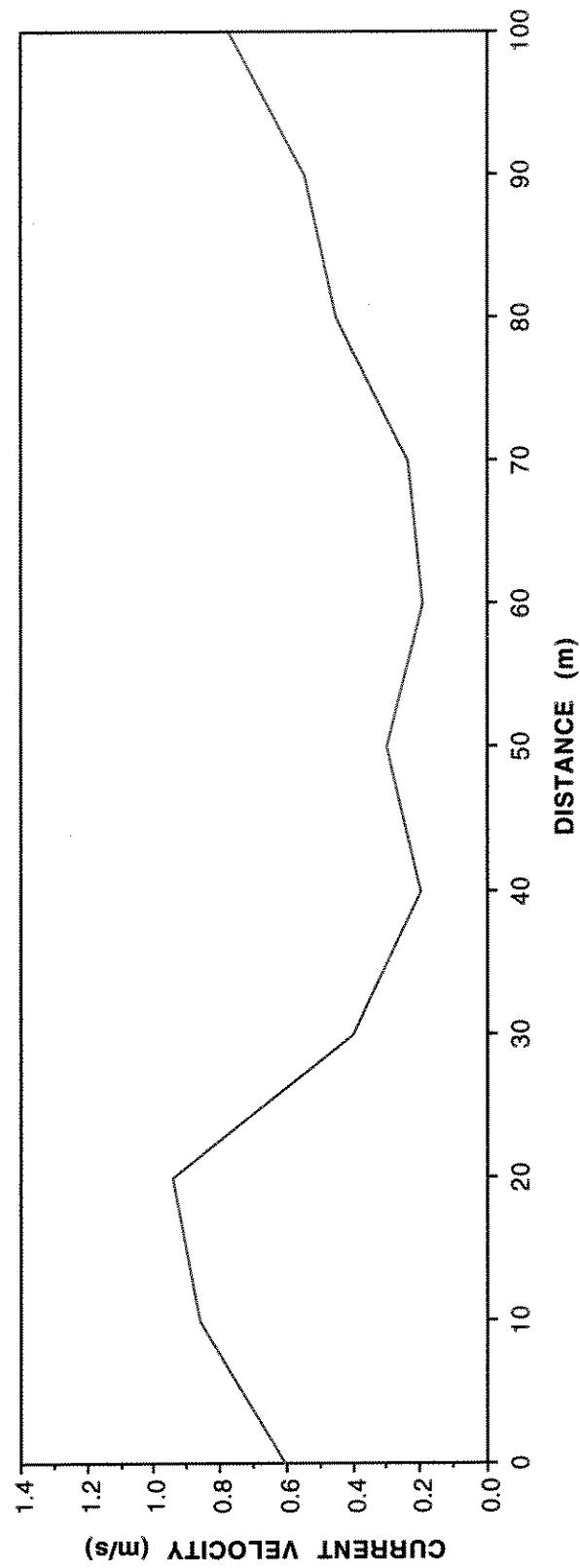
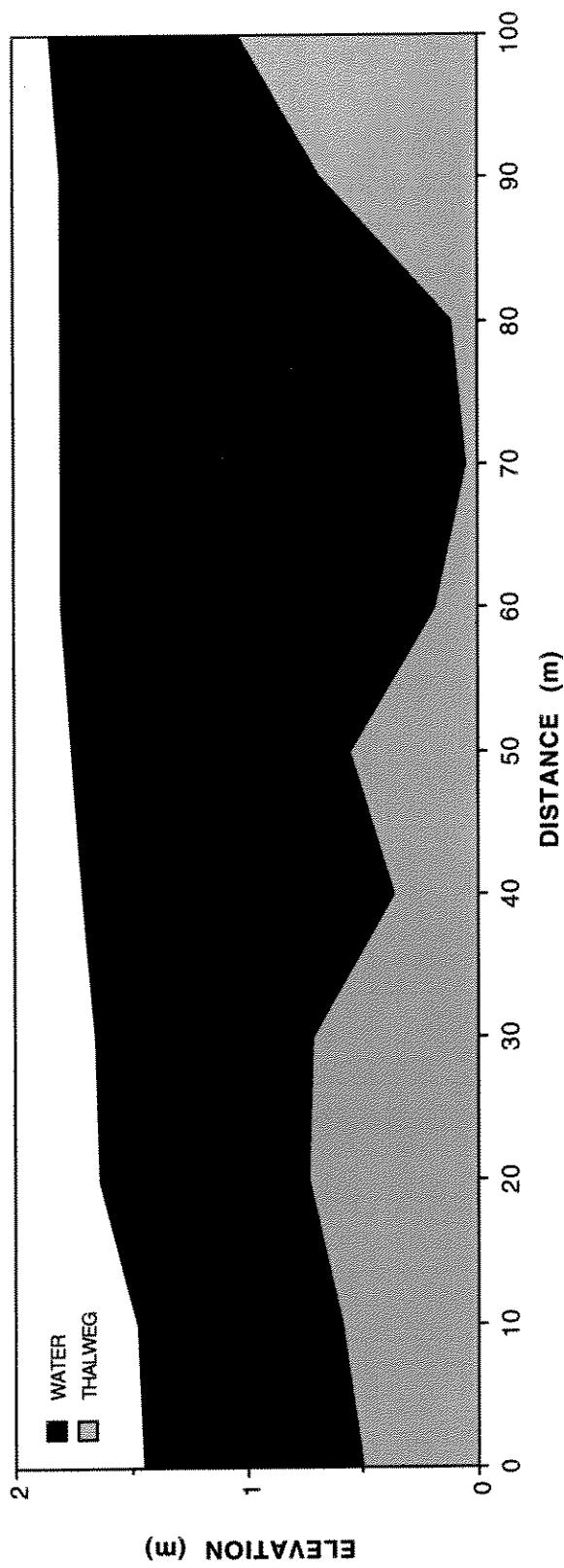


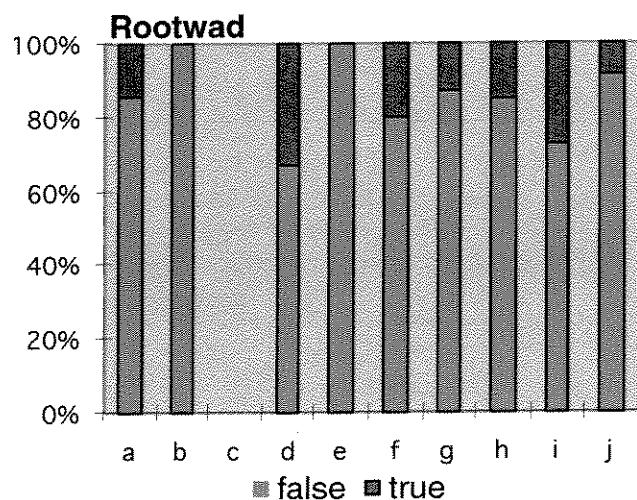
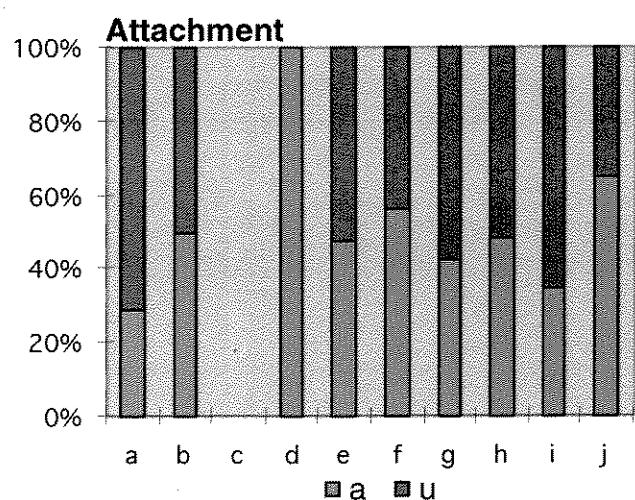
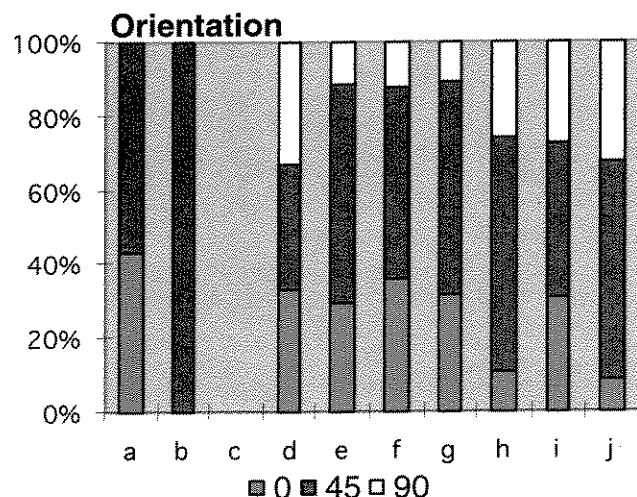
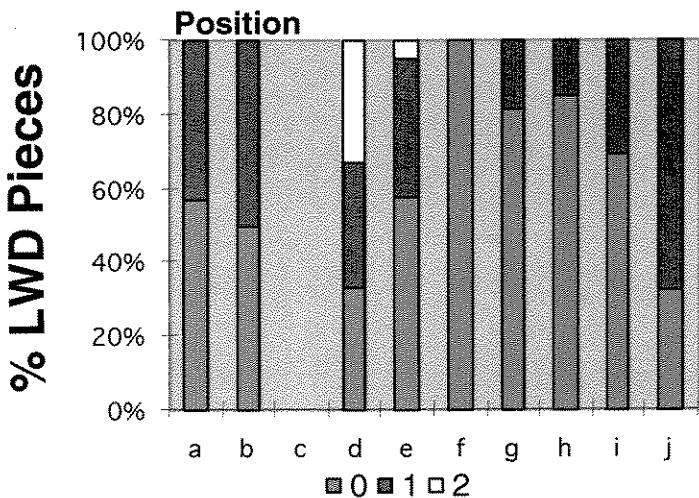
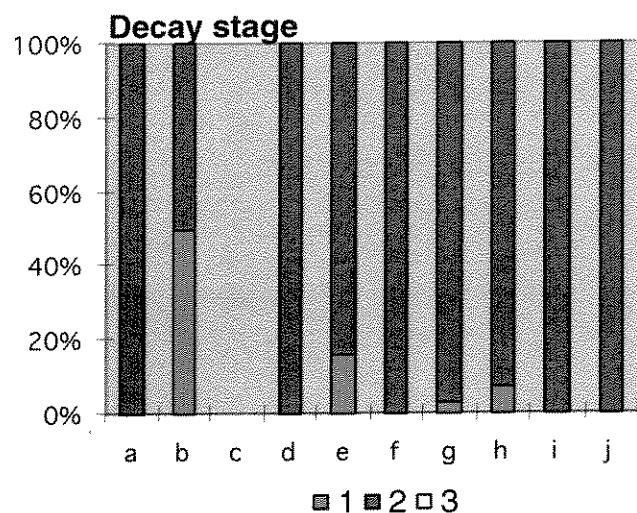
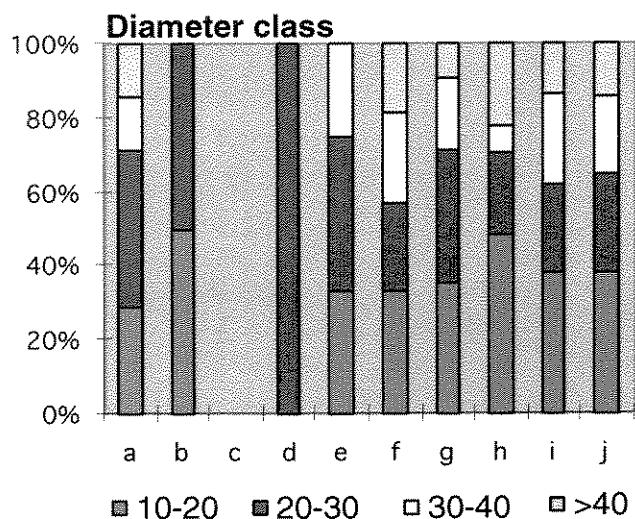
## Youngs Creek reach a

A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



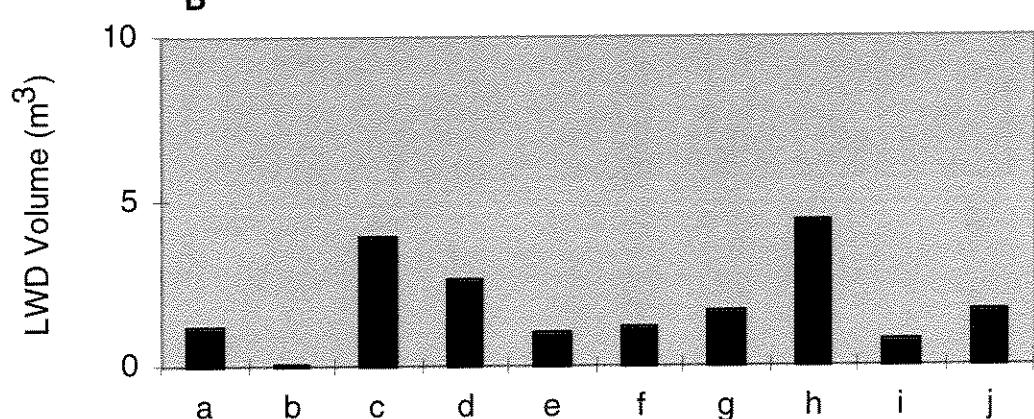
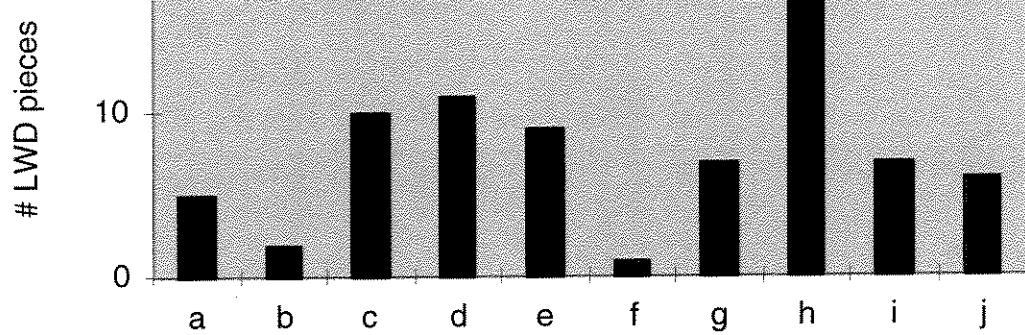
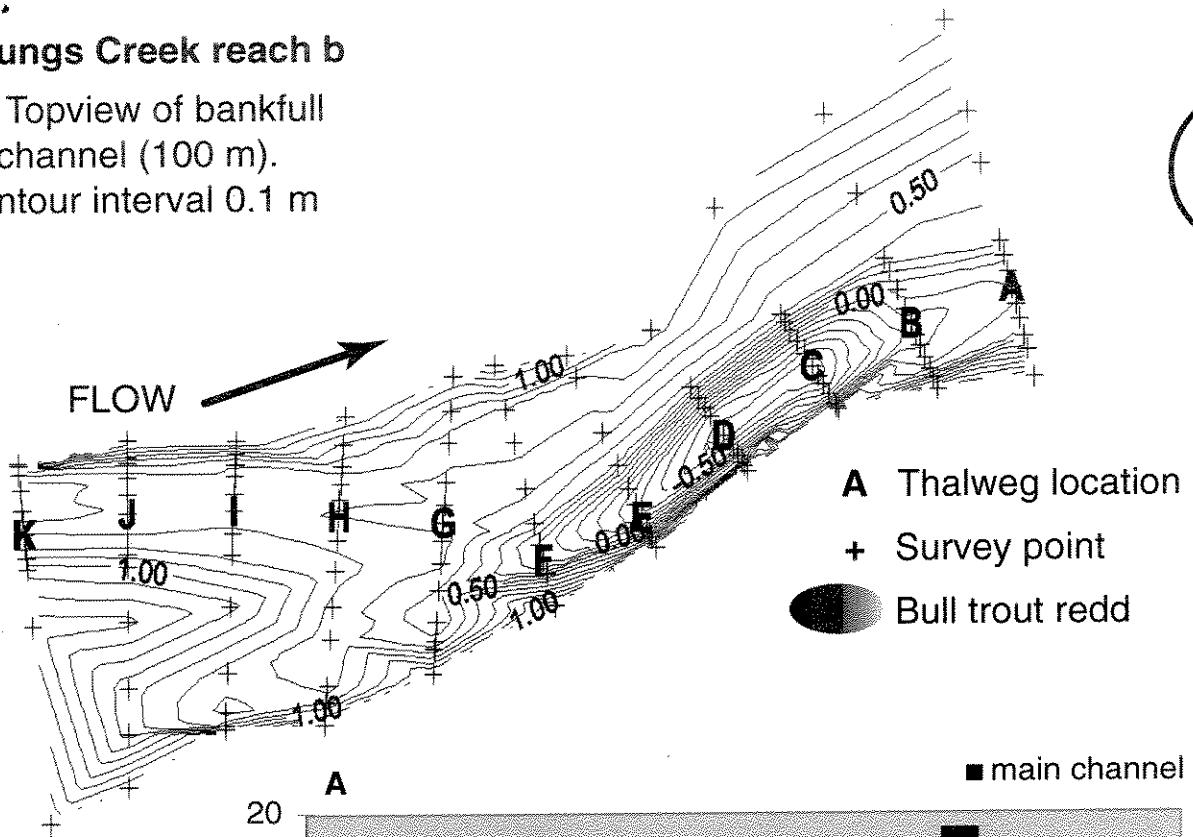
Youngs Creek Reach A



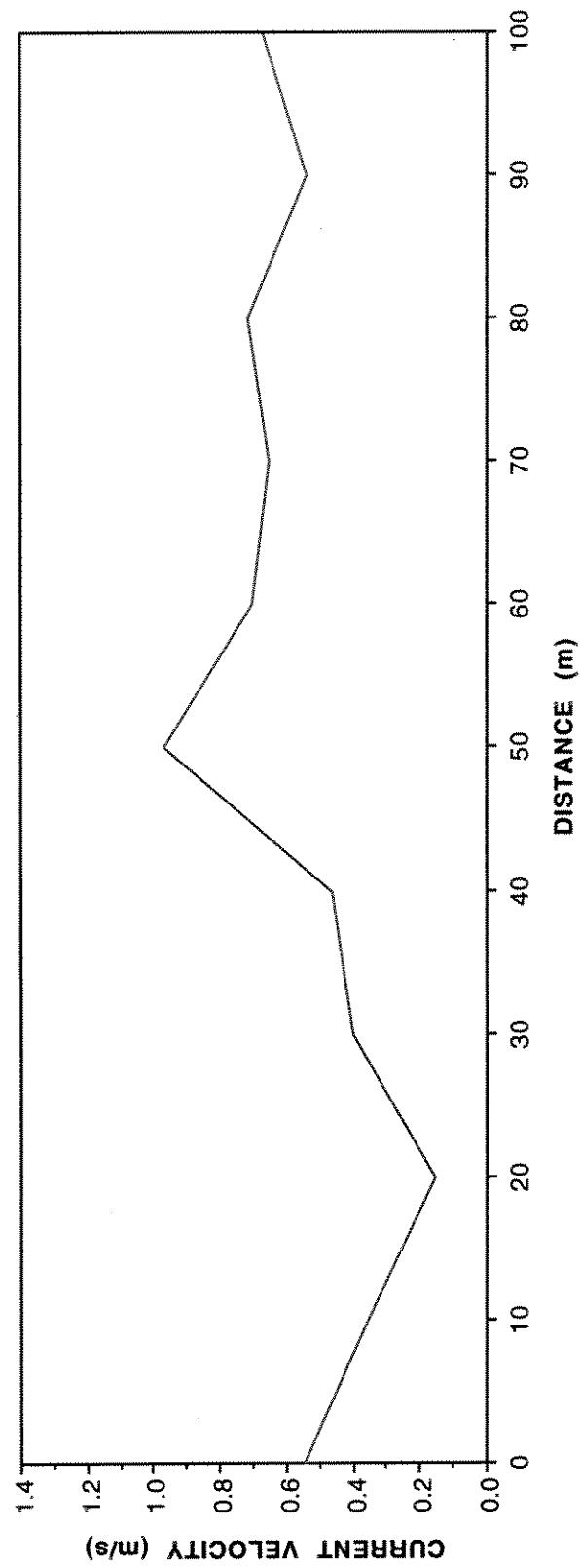
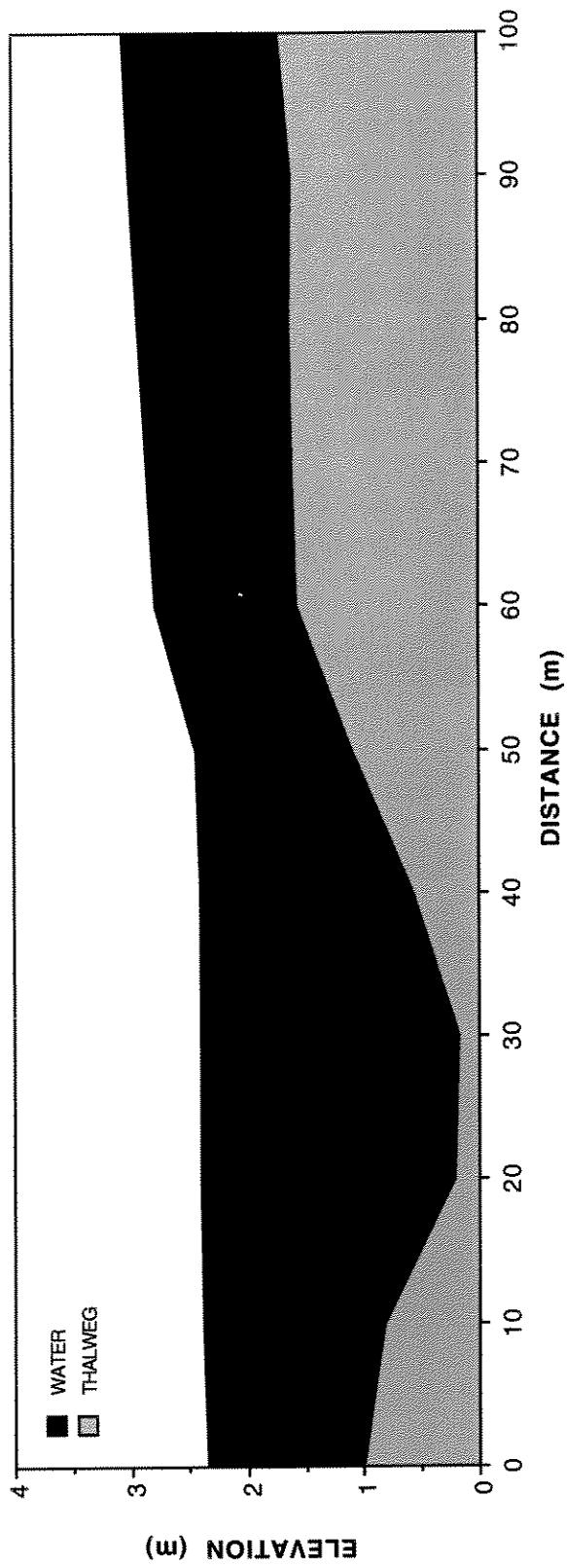


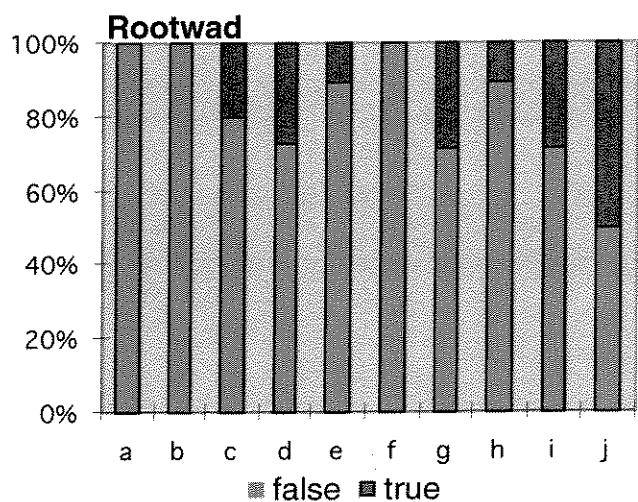
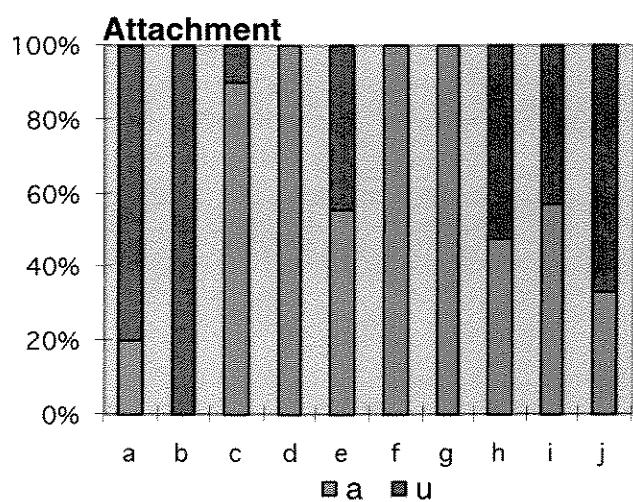
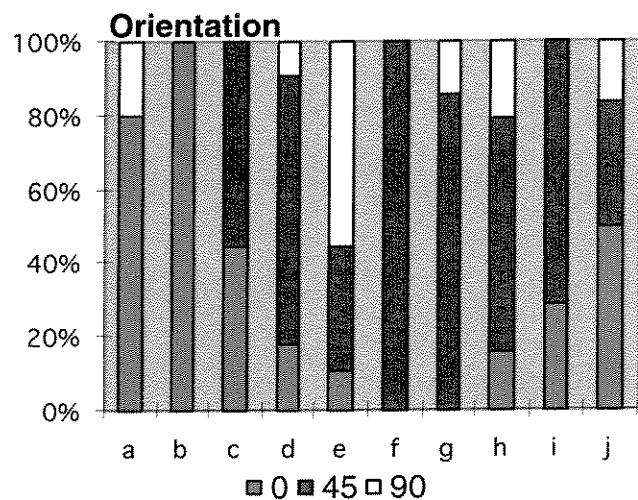
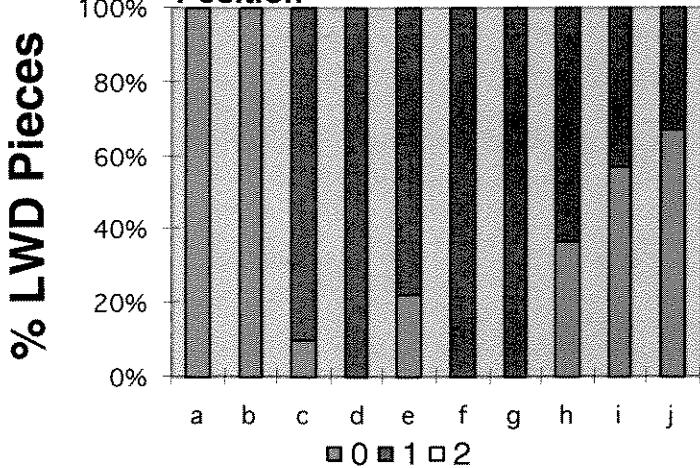
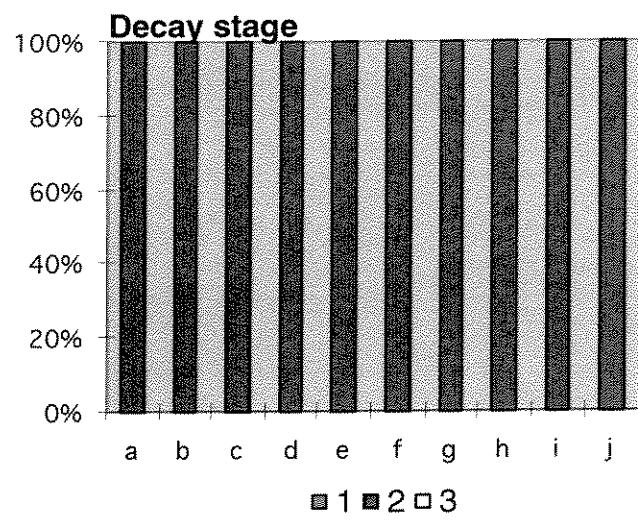
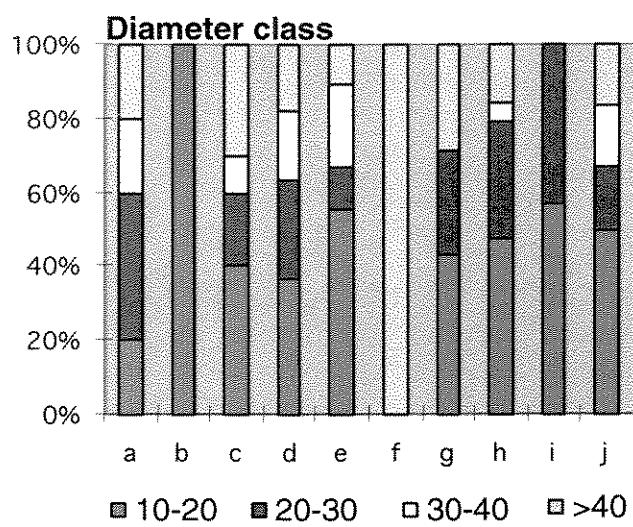
## Youngs Creek reach b

A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



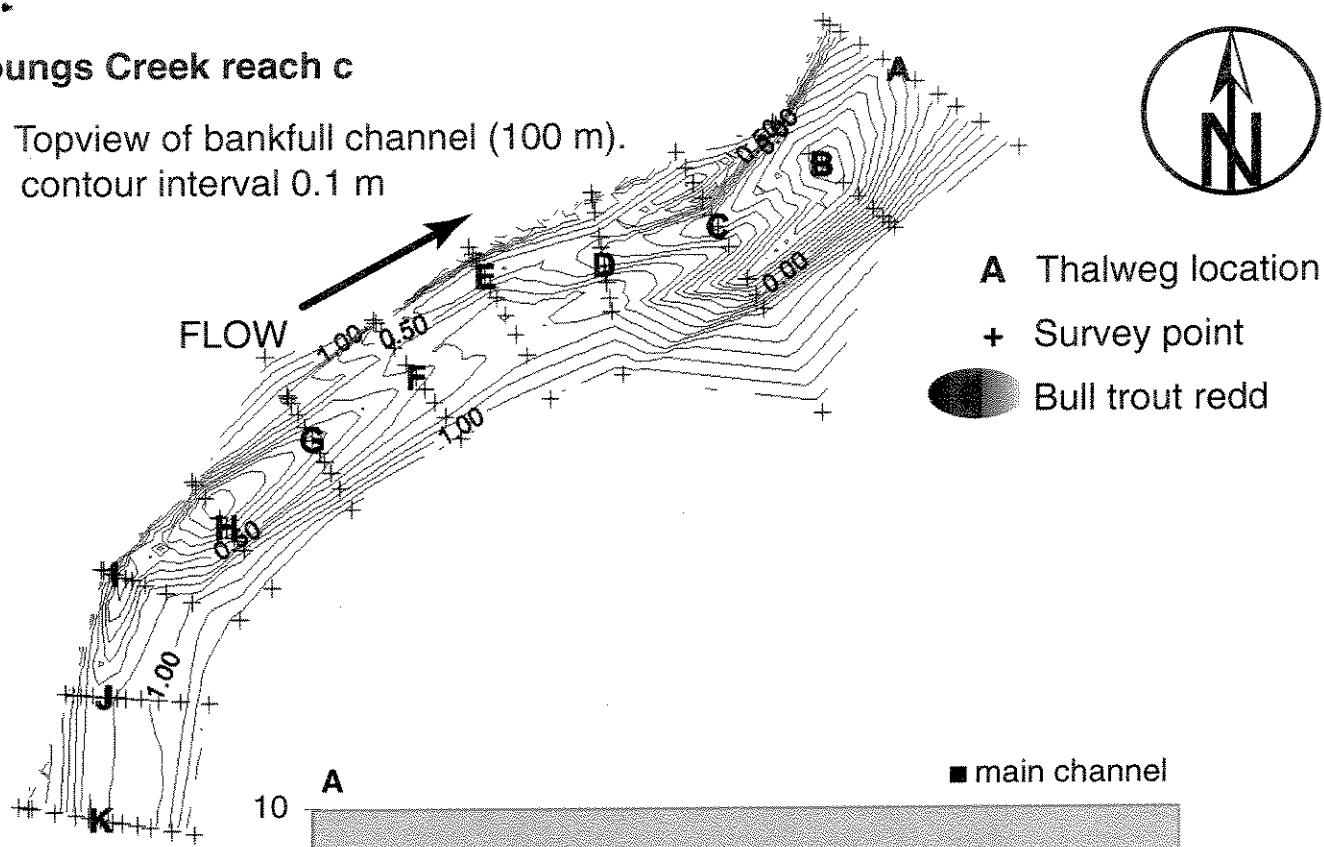
Youngs Creek Reach B





## Youngs Creek reach c

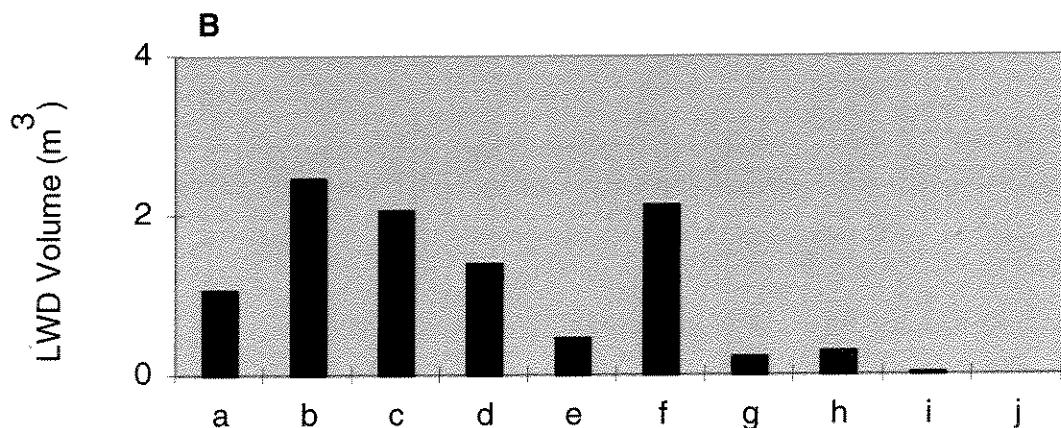
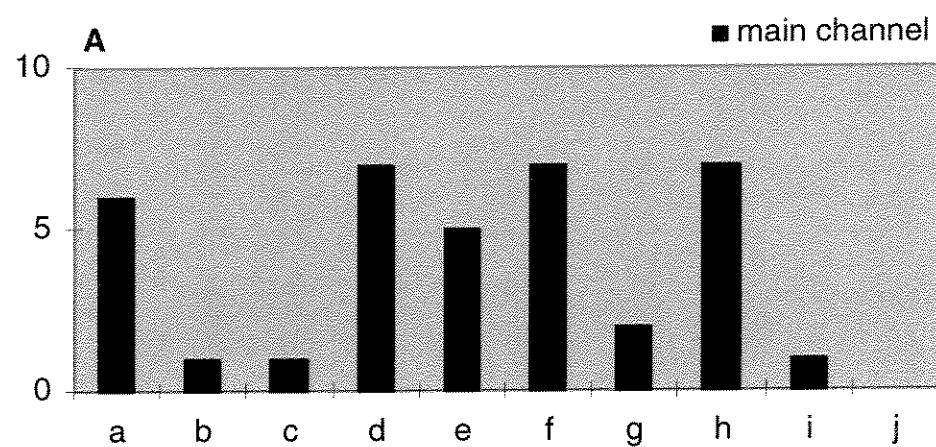
A: Topview of bankfull channel (100 m).  
contour interval 0.1 m



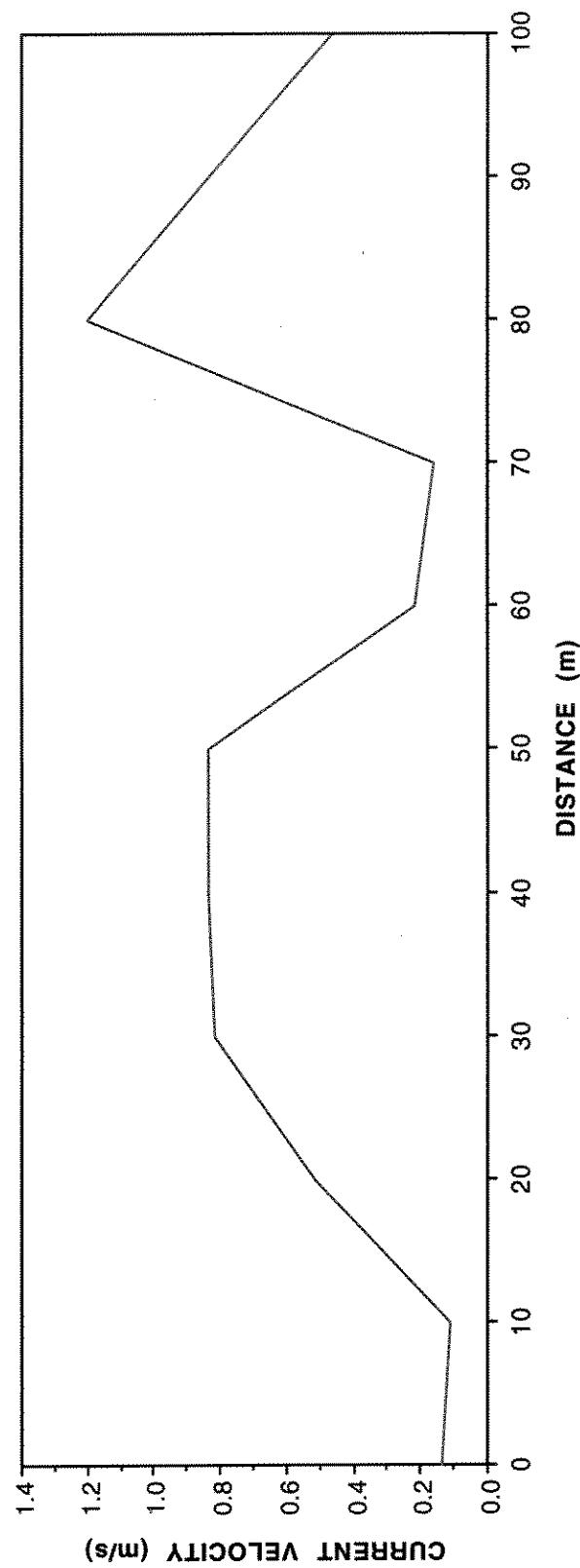
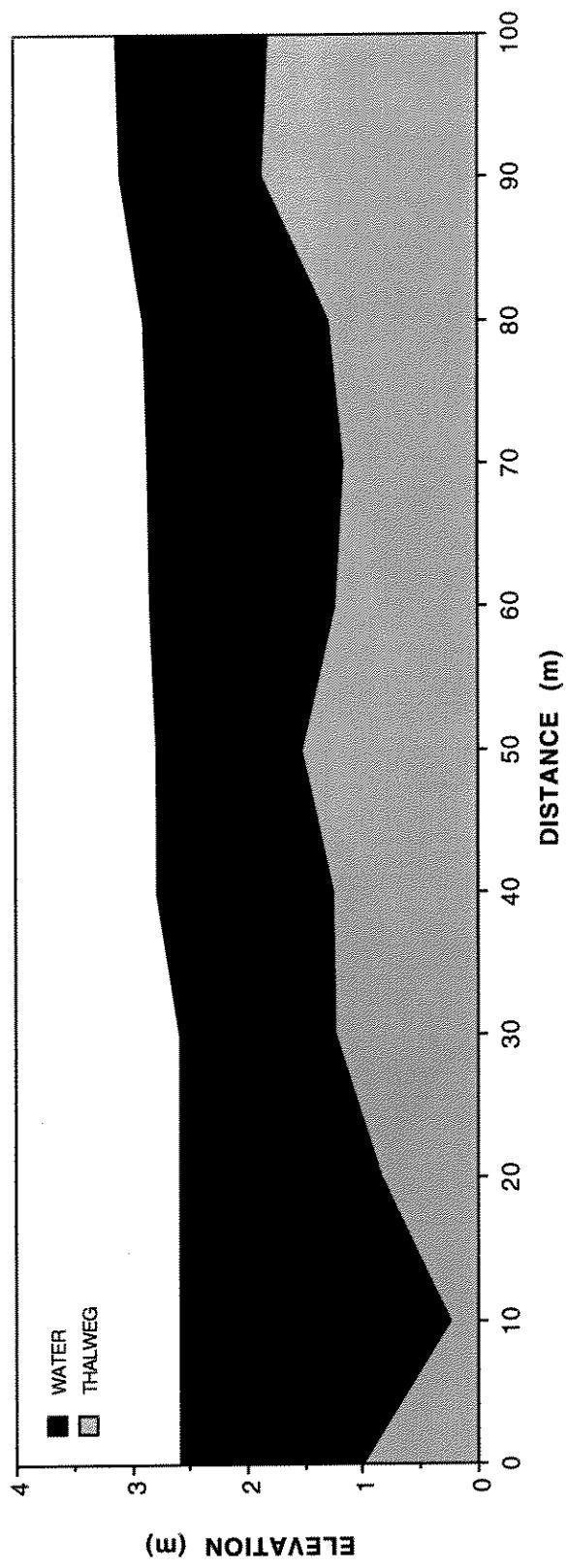
**A** Thalweg location

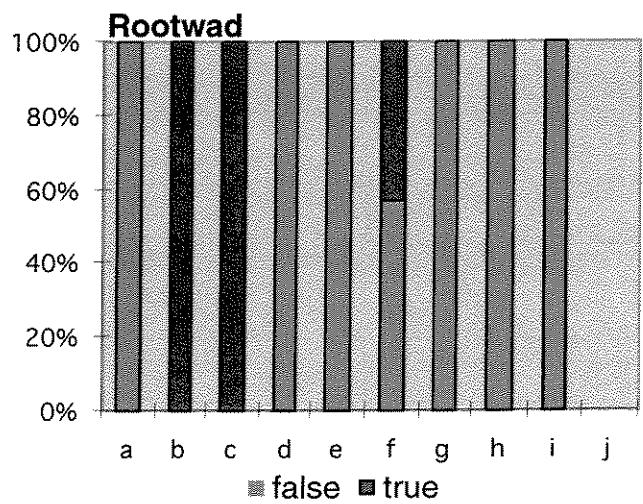
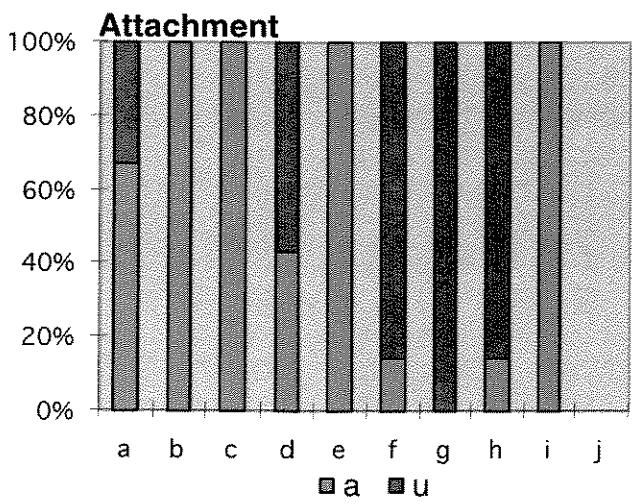
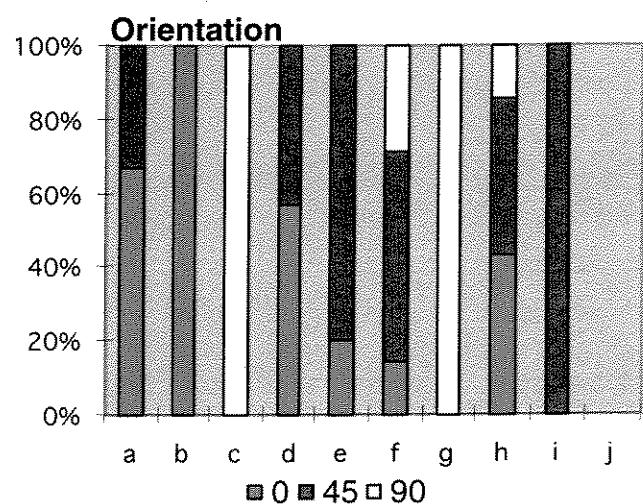
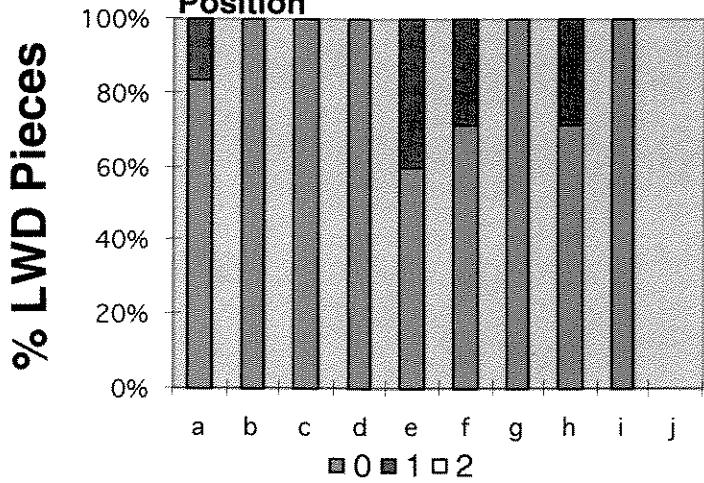
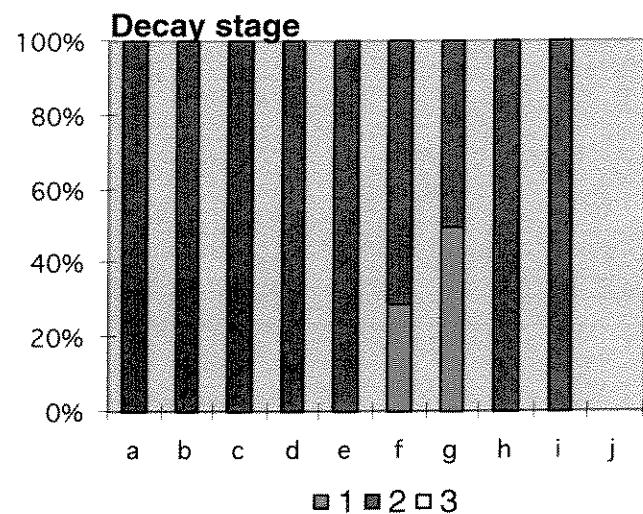
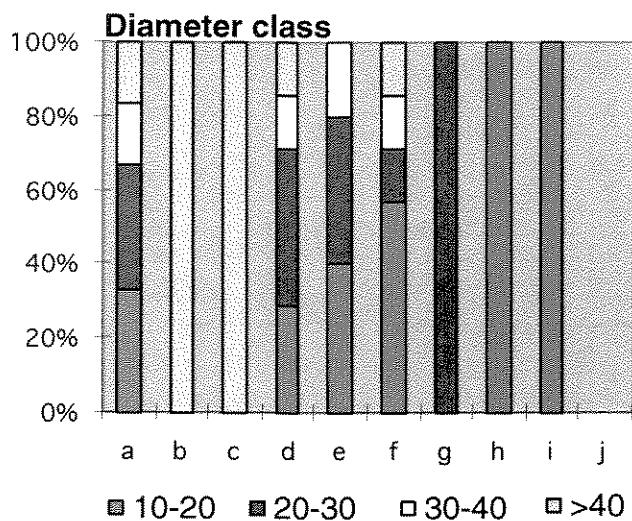
+ Survey point

● Bull trout redd



Youngs Creek Reach C





## APPENDIX B

### LARGE WOODY DEBRIS IN BULL TROUT SPAWNING STREAMS IN NORTHWEST MONTANA

F. Richard Hauer

John T. Gangemi

a n d

Colden V. Baxter

Flathead Lake Biological Station

The University of Montana

311 BioStation Lane

Polson, MT 59860

CROSS_ID	Cross_4	basin_aref	SC_ID	AGG_ID	LWD_ID	LWD_NO	LWD_D1_(m)	LWD_D2_(m)	Max_DiameterLWD	LENGTH	area_1_(m2)	area_2_(m2)	LWD_VOL_(m^3)	
co1ac	co1a	29920	0	0	3	3	0.1500	0.1800	18	5.60	0.017671	0.025447	0.1207313	
co1ac	co1a	29920	0	0	1	1	0.1100	0.1500	15	2.60	0.009503	0.017671	0.0353272	
co1ac	co1a	29920	0	0	2	2	0.2300	0.2300	23	3.40	0.041548	0.041548	0.1412616	
co1ac	co1a	29920	0	0	4	4	0.7900	0.3800	79	9.30	0.490167	0.113411	2.8066376	
co1ad	co1a	29920	0	0	5	9	0.1500	0.1400	15	3.00	0.017671	0.015394	0.0495979	
co1ad	co1a	29920	0	0	6	6	0.2800	0.2300	28	7.00	0.061575	0.041548	0.3609294	
co1ad	co1a	29920	0	0	3	7	0.2500	0.1900	25	5.50	0.049887	0.028353	0.2129605	
co1ad	co1a	29920	0	0	1	5	0.2200	0.1400	22	13.50	0.038013	0.015394	0.3604975	
co1ad	co1a	29920	0	0	4	8	0.4100	0.3100	41	3.40	0.132225	0.075477	0.3527534	
co1af	co1a	29920	0	0	1	10	0.3300	0.2750	33	3.50	0.085530	0.059396	0.2536196	
co1ag	co1a	29920	0	0	1	11	0.3000	0.0450	30	17.50	0.070686	0.001590	0.6324168	
co1ah	co1a	29920	0	0	1	12	0.0500	0.2100	21	11.40	0.001963	0.034636	0.2086173	
co1ah	co1a	29920	1	2	35	46	0.1980	0.1960	20	3.40	0.030791	0.030172	0.1036363	
co1ah	co1a	29920	1	2	40	51	0.1950	0.1830	20	3.60	0.029865	0.026302	0.1011005	
co1ah	co1a	29920	1	2	28	39	0.1810	0.1610	18	3.10	0.025730	0.020358	0.0714375	
co1ah	co1a	29920	1	2	34	45	0.1610	0.1510	16	7.20	0.002124	0.025447	0.0992541	
co1ah	co1a	29920	1	0	6	17	0.0520	0.1800	18	3.00	0.010387	0.025447	0.0537506	
co1ah	co1a	29920	1	1	13	24	0.1150	0.1800	18	3.40	0.030791	0.030172	0.1036363	
co1ah	co1a	29920	1	2	30	41	0.1520	0.1730	17	3.90	0.018146	0.023506	0.0812214	
co1ah	co1a	29920	1	2	29	40	0.1710	0.0900	17	3.30	0.022966	0.006362	0.0483904	
co1ah	co1a	29920	1	2	34	45	0.1610	0.1510	16	2.40	0.002124	0.020358	0.017908	
co1ah	co1a	29920	1	2	38	49	0.1600	0.1380	16	1.20	0.020106	0.014957	0.0210380	
co1ah	co1a	29920	1	0	2	19	0.1470	0.0700	15	5.40	0.016972	0.003848	0.0562143	
co1ah	co1a	29920	1	2	35	46	0.1400	0.1460	15	5.10	0.015394	0.016742	0.0819451	
co1ah	co1a	29920	1	2	24	35	0.1110	0.1430	14	4.50	0.009677	0.016061	0.0579093	
co1ah	co1a	29920	1	1	11	22	0.1350	0.0470	14	5.70	0.014314	0.001735	0.0457391	
co1ah	co1a	29920	1	1	12	23	0.0800	0.1290	13	2.40	0.005027	0.013070	0.0217156	
co1ah	co1a	29920	1	2	26	37	0.1260	0.1260	13	2.80	0.012469	0.012469	0.0349131	
co1ah	co1a	29920	1	2	33	44	0.1260	0.1260	10	3.30	0.008171	0.008171	0.0137155	
co1ah	co1a	29920	1	2	39	50	0.0840	0.1250	30	21.70	0.068349	0.006648	0.8137155	
co1ah	co1a	29920	1	2	27	38	0.1020	0.1020	28	14.50	0.013273	0.012272	0.0195950	
co1ah	co1a	29920	1	2	32	43	0.2950	0.0920	28	2.00	0.005542	0.012272	0.0269652	
co1ah	co1a	29920	1	1	8	19	0.0500	0.2930	29	2.5	0.057255	0.059396	0.1166512	
co1ah	co1a	29920	1	2	20	31	0.1300	0.2810	28	2.00	0.056155	0.006504	0.3206238	
co1ah	co1a	29920	1	2	31	42	0.2700	0.2750	28	2.00	0.049876	0.028353	0.1329888	
co1ah	co1a	29920	1	2	23	34	0.2660	0.0910	27	10.40	0.016513	0.0140934	0.6140934	
co1ah	co1a	29920	1	0	5	16	0.2520	0.1900	25	3.40	0.012469	0.012469	0.05458452	
co1ah	co1a	29920	1	2	21	32	0.2210	0.2500	26	6.50	0.033360	0.049087	0.2842026	
co1ah	co1a	29920	1	0	3	14	0.1600	0.2470	25	5.00	0.035633	0.032365	0.1699954	
co1ah	co1a	29920	1	2	22	33	0.2350	0.1630	24	1.80	0.020106	0.047916	0.0612202	
co1ah	co1a	29920	1	2	2	36	47	0.1280	0.2200	22	6.60	0.012568	0.038013	0.1679079
co1ah	co1a	29920	1	0	4	15	0.1450	0.2130	21	2.70	0.016513	0.035633	0.0703967	
co1ah	co1a	29920	1	2	25	36	0.2130	0.2030	21	5.50	0.013883	0.035299	0.1352775	
co1ah	co1a	29920	1	1	9	20	0.1330	0.2120	21	3.50	0.009503	0.032685	0.0738297	
co1ah	co1a	29920	1	0	17	28	0.1100	0.2040	20	4.50	0.020612	0.031731	0.1177713	
co1ah	co1a	29920	1	2	37	48	0.1620	0.2010	20	7.90	0.012868	0.031416	0.1749212	
co1ah	co1a	29920	1	1	14	25	0.1280	0.2000	20	4.50	0.017671	0.090792	0.7863596	
co1ah	co1a	29920	1	2	18	29	0.1500	0.3400	34	14.50	0.017671	0.090792	0.7863596	

co1ah	co1a	29920	1	0	7	18	0.2970	0.3300	33	6.00	0.069279	0.085530	0.4644267	FALSE
co1ah	co1a	29920	1	1	10	21	0.3300	0.2220	33	11.60	0.085530	0.038708	0.7205764	FALSE
co1ah	co1a	29920	1	1	16	27	1.0000	0.4280	100	1.20	0.785398	0.143872	0.5575619	TRUE
co1ah	co1a	29920	1	1	15	26	0.1200	0.5290	53	1.10	0.011310	0.219786	0.1271029	TRUE
co1ah	co1a	29920	1	2	19	30	0.0800	0.4520	45	13.60	0.005027	0.160460	1.1253075	FALSE
co1ai	co1a	29920	1	0	5	56	0.1900	0.1400	19	3.10	0.028553	0.015394	0.0678073	FALSE
co1ai	co1a	29920	1	0	26	77	0.1700	0.1900	19	2.50	0.022698	0.028353	0.0638135	FALSE
co1ai	co1a	29920	1	0	8	59	0.1800	0.1200	18	4.70	0.025447	0.011310	0.0863780	FALSE
co1ai	co1a	29920	1	3	11	62	0.1700	0.1450	17	2.10	0.022698	0.016513	0.0411715	FALSE
co1ai	co1a	29920	1	0	21	72	0.1700	0.1700	17	4.00	0.022698	0.022698	0.0907920	FALSE
co1ai	co1a	29920	1	0	24	75	0.1700	0.1700	17	3.80	0.022698	0.022698	0.0862524	FALSE
co1ai	co1a	29920	1	0	17	68	0.1600	0.1400	16	11.60	0.020106	0.015394	0.2058998	FALSE
co1ai	co1a	29920	1	0	15	66	0.1500	0.1200	15	9.60	0.017671	0.011310	0.1391096	FALSE
co1ai	co1a	29920	1	0	19	70	0.1500	0.1200	15	3.10	0.017671	0.011310	0.0449208	FALSE
co1ai	co1a	29920	1	0	27	78	0.1500	0.1500	15	6.50	0.017671	0.011310	0.148644	FALSE
co1ai	co1a	29920	1	3	12	63	0.1400	0.1200	14	4.90	0.015394	0.011310	0.0654236	FALSE
co1ai	co1a	29920	1	3	9	60	0.1000	0.1200	12	4.90	0.007854	0.011310	0.0469511	FALSE
co1ai	co1a	29920	1	3	13	64	0.1200	0.0800	12	4.50	0.011310	0.005027	0.0367566	FALSE
co1ai	co1a	29920	1	3	14	65	0.1000	0.1000	10	2.80	0.007854	0.0219911	0.0219911	FALSE
co1ai	co1a	29920	1	3	6	57	0.2900	0.2100	29	21.90	0.066052	0.034686	1.1025332	FALSE
co1ai	co1a	29920	1	0	22	73	0.2700	0.2000	27	2.60	0.057255	0.031416	0.1152728	FALSE
co1ai	co1a	29920	1	0	16	67	0.2000	0.2600	26	8.20	0.031416	0.053093	0.3449860	FALSE
co1ai	co1a	29920	1	0	18	69	0.2100	0.2600	26	4.90	0.034636	0.053093	0.2149358	FALSE
co1ai	co1a	29920	1	2	1	52	0.1700	0.2500	25	6.00	0.022698	0.049087	0.2152560	FALSE
co1ai	co1a	29920	1	0	20	71	0.2500	0.2400	25	6.10	0.049087	0.045239	0.2876950	FALSE
co1ai	co1a	29920	1	2	2	53	0.1800	0.2200	22	12.60	0.025447	0.038013	0.3997987	FALSE
co1ai	co1a	29920	1	0	25	76	0.2200	0.1800	22	6.10	0.038013	0.025447	0.1935534	FALSE
co1ai	co1a	29920	1	0	3	54	0.2000	0.2000	20	3.60	0.031416	0.031416	0.1099557	FALSE
co1ai	co1a	29920	1	0	4	55	0.2000	0.1800	20	2.10	0.031416	0.025447	0.0597059	FALSE
co1ai	co1a	29920	1	0	23	74	0.2900	0.3600	36	8.40	0.066052	0.1011788	0.7049257	FALSE
co1ai	co1a	29920	1	0	7	58	0.3500	0.2500	35	5.30	0.096211	0.049087	0.3850411	FALSE
co1ai	co1a	29920	1	0	10	61	0.6800	0.1900	68	0.85	0.363168	0.028353	0.1663963	TRUE
co1ai	co1a	29920	0	0	22	100	0.1900	0.1900	19	8.20	0.028353	0.028353	0.2324934	FALSE
co1ai	co1a	29920	0	0	29	107	0.1100	0.1900	19	11.40	0.00503	0.028353	0.2157801	FALSE
co1ai	co1a	29920	0	0	26	104	0.1800	0.1400	18	5.70	0.025447	0.015394	0.1163959	FALSE
co1ai	co1a	29920	0	0	27	105	0.1000	0.1500	15	9.00	0.00503	0.017671	0.1148644	FALSE
co1ai	co1a	29920	0	0	23	101	0.1400	0.1400	14	12.10	0.015394	0.015394	0.1862649	FALSE
co1ai	co1a	29920	0	0	30	108	0.1300	0.1000	13	5.00	0.013273	0.007854	0.0528180	FALSE
co1ai	co1a	29920	0	0	24	102	0.1000	0.1300	13	9.70	0.007854	0.013273	0.1024669	FALSE
co1ai	co1a	29920	0	0	32	110	0.1200	0.1200	12	3.20	0.011310	0.011310	0.0361911	FALSE
co1ai	co1a	29920	0	0	20	98	0.2400	0.2400	24	9.00	0.045239	0.045239	0.4071501	FALSE
co1ai	co1a	29920	0	0	28	106	0.2200	0.2200	22	3.50	0.038013	0.038013	0.1330463	FALSE
co1ai	co1a	29920	0	0	21	99	0.2200	0.2000	22	9.00	0.038013	0.031416	0.3124311	FALSE
co1ai	co1a	29920	0	0	25	103	0.4200	0.4200	42	6.50	0.138544	0.138544	0.9005368	FALSE
co1ai	co1a	29920	0	0	31	109	0.4100	0.4100	41	4.90	0.132025	0.132025	0.6469241	FALSE
co1ai	co1a	29920	1	0	5	83	0.1900	0.1900	19	3.60	0.028353	0.028353	0.1020703	FALSE
co1ai	co1a	29920	1	3	10	88	0.1900	0.1300	19	15.60	0.028353	0.013273	0.3246833	FALSE

co1ai	co1a	29920	1	4	34	112	0.1900	0.1500	19	15.90	0.028353	0.017671	0.3658931	FALSE
co1ai	co1a	29920	1	0	2	80	0.1800	0.1400	18	16.10	0.025447	0.015394	0.3287674	FALSE
co1ai	co1a	29920	1	0	4	82	0.1600	0.1400	16	3.10	0.020106	0.015394	0.0550249	FALSE
co1ai	co1a	29920	1	0	9	87	0.1600	0.1000	16	17.50	0.020106	0.007854	0.2446513	FALSE
co1ai	co1a	29920	1	0	18	96	0.1500	0.1500	15	12.40	0.017671	0.017671	0.2191259	FALSE
co1ai	co1a	29920	1	0	45	123	0.1000	0.1500	15	5.40	0.007854	0.017761	0.0689186	FALSE
co1ai	co1a	29920	1	0	8	86	0.1300	0.1000	13	3.80	0.013273	0.007854	0.0401417	FALSE
co1ai	co1a	29920	1	0	17	95	0.1100	0.1300	13	2.10	0.009503	0.013273	0.0239154	FALSE
co1ai	co1a	29920	1	0	3	81	0.1200	0.1000	12	5.70	0.011310	0.007854	0.0546165	FALSE
co1ai	co1a	29920	1	0	6	84	0.1200	0.1200	12	6.20	0.011310	0.011310	0.0701203	FALSE
co1ai	co1a	29920	1	0	7	85	0.1000	0.1200	12	2.90	0.007854	0.011310	0.0277874	FALSE
co1ai	co1a	29920	1	4	36	114	0.1200	0.0800	12	3.90	0.011310	0.005027	0.0318557	FALSE
co1ai	co1a	29920	1	3	12	90	0.1000	0.1100	11	10.00	0.007854	0.009503	0.0867864	FALSE
co1ai	co1a	29920	1	4	37	115	0.1100	0.0600	11	5.30	0.009503	0.002827	0.0326765	FALSE
co1ai	co1a	29920	1	0	43	121	0.1100	0.1100	11	3.10	0.009503	0.009503	0.0294603	FALSE
co1ai	co1a	29920	1	3	13	91	0.1000	0.1000	10	5.10	0.007854	0.007854	0.0400553	FALSE
co1ai	co1a	29920	1	0	39	117	0.2900	0.1900	29	3.90	0.066052	0.028353	0.18010893	FALSE
co1ai	co1a	29920	1	0	15	93	0.2700	0.2700	27	3.40	0.057255	0.057255	0.1946686	FALSE
co1ai	co1a	29920	1	0	41	119	0.2500	0.2500	25	2.30	0.049087	0.049087	0.1129009	FALSE
co1ai	co1a	29920	1	4	33	111	0.2200	0.2400	24	4.80	0.038013	0.045239	0.1998051	FALSE
co1ai	co1a	29920	1	0	16	94	0.2300	0.2300	23	6.30	0.041548	0.041548	0.2617494	FALSE
co1ai	co1a	29920	1	0	1	79	0.1600	0.2200	22	14.50	0.020106	0.038013	0.4329896	FALSE
co1ai	co1a	29920	1	0	19	97	0.2100	0.1600	21	14.60	0.034636	0.020106	0.3996181	FALSE
co1ai	co1a	29920	1	3	11	89	0.2000	0.1000	20	12.40	0.031416	0.031416	0.2434742	FALSE
co1ai	co1a	29920	1	4	35	113	0.2000	0.1400	20	7.10	0.031416	0.015394	0.1661744	FALSE
co1ai	co1a	29920	1	0	42	120	0.3400	0.3000	34	5.00	0.090792	0.070686	0.4036943	FALSE
co1ai	co1a	29920	1	0	44	122	0.1400	0.3100	31	10.20	0.015394	0.017671	0.4634395	FALSE
co1ai	co1a	29920	1	3	14	92	0.2100	0.3000	30	12.00	0.034636	0.070686	0.6319308	FALSE
co1ai	co1a	29920	1	0	40	118	0.3500	1.7500	175	2.60	0.096211	2.405280	3.2519383	TRUE
co1ai	co1a	29920	1	0	38	116	0.3800	0.4800	48	6.80	0.113411	0.180956	1.0008477	FALSE
co1ba	co1b	29920	0	a	11	0.1800	0.1500	18	3.30	0.023447	0.017671	0.0711452	FALSE	
co1ba	co1b	29920	0	a	10	10	0.1700	0.1800	18	3.10	0.022698	0.025447	0.0746245	FALSE
co1ba	co1b	29920	0	a	3	0.1450	0.1700	17	3.10	0.016513	0.022698	0.0607770	FALSE	
co1ba	co1b	29920	0	a	13	0.1600	0.1200	16	4.20	0.020106	0.011310	0.0659734	FALSE	
co1ba	co1b	29920	0	a	14	0.1100	0.1500	15	7.10	0.009503	0.017671	0.064704	FALSE	
co1ba	co1b	29920	0	a	1	0.2150	0.1800	22	3.80	0.036355	0.025447	0.1173286	FALSE	
co1ba	co1b	29920	0	a	12	12	0.2000	0.1000	20	4.50	0.031416	0.007854	0.0883572	FALSE
co1ba	co1b	29920	0	a	4	4	0.3600	0.3600	36	1.20	0.101788	0.101788	0.1221450	FALSE
co1ba	co1b	29920	0	a	2	2	0.4750	0.5100	51	8.70	0.177205	0.204282	1.6594693	FALSE
co1ba	co1b	29920	1	a	5	0.1800	0.1600	18	7.70	0.025447	0.020106	0.1753793	FALSE	
co1ba	co1b	29920	1	a	6	0.1200	0.1300	13	1.80	0.011310	0.013273	0.0221246	FALSE	
co1ba	co1b	29920	1	a	8	0.2200	0.2800	28	9.94	0.038013	0.061575	0.4949544	FALSE	
co1ba	co1b	29920	1	9	9	0.2400	0.1900	24	1.90	0.045239	0.028353	0.0699122	FALSE	
co1ba	co1b	29920	1	7	7	0.3700	0.3100	37	7.80	0.107521	0.075477	0.7136907	FALSE	
co1bb	co1b	29920	0	2	16	0.2800	0.3000	30	4.50	0.061575	0.070686	0.2975871	FALSE	
co1bb	co1b	29920	0	1	15	0.3300	0.4700	47	4.00	0.086530	0.173494	0.5180482	FALSE	
co1bc	co1b	29920	0	2	18	0.1100	0.0500	11	4.00	0.009503	0.001963	0.0229336	FALSE	

co1bc	co1b	29920	0	3	19	0.0600	0.2400	24	9.60	0.002827	0.045239	0.2307184	FALSE
co1bc	co1b	29920	0	1	17	0.0500	0.2300	23	8.70	0.001963	0.041548	0.1892729	FALSE
co1bd	co1b	29920	0	1	20	0.0700	0.1900	19	6.30	0.003848	0.028553	0.1014341	FALSE
co1be	co1b	29920	0	3	23	0.1200	0.1700	17	1.30	0.011310	0.0222998	0.0221050	FALSE
co1be	co1b	29920	0	1	21	0.2900	0.3800	38	3.30	0.066052	0.113411	0.2961145	FALSE
co1bf	co1b	29920	0	2	22	0.3100	0.3000	31	3.40	0.070886	0.2484762	0.2484762	FALSE
co1bf	co1b	29920	0	1	24	0.1800	0.1900	19	1.80	0.025447	0.028353	0.0484198	FALSE
co1bf	co1b	29920	0	2	25	0.1600	0.1800	18	3.90	0.020106	0.025447	0.0888285	FALSE
co1bf	co1b	29920	0	4	27	0.1100	0.1000	11	3.70	0.009503	0.007854	0.0321110	FALSE
co1bg	co1b	29920	0	3	26	0.1900	0.2000	20	1.80	0.028353	0.031416	0.0537919	FALSE
co1bh	co1b	29920	0	1	28	0.2600	0.1000	260	1.90	5.309287	0.785398	5.7899504	TRUE
co1bi	co1b	29920	0	1	29	0.1100	0.0800	11	3.10	0.009503	0.005027	0.0225213	FALSE
co1bj	co1b	29920	0	1	30	0.2400	0.5900	59	7.50	0.045239	0.273397	1.1948841	FALSE
co1bj	co1b	29920	0	4	34	0.1400	0.1300	14	3.40	0.015394	0.013273	0.0487339	FALSE
co1bj	co1b	29920	0	3	33	0.1400	0.0600	14	3.50	0.015394	0.002827	0.0318871	FALSE
co1bj	co1b	29920	0	6	36	0.0800	0.1400	14	4.20	0.005027	0.015394	0.0428827	FALSE
co1bj	co1b	29920	0	2	32	0.2000	0.2100	21	2.90	0.031416	0.034636	0.0957753	FALSE
co1bj	co1b	29920	0	1	31	0.5100	2.0000	200	1.80	0.204282	3.141590	3.0112847	TRUE
co1bj	co1b	29920	0	5	35	0.0600	1.0000	100	9.20	0.002827	0.785398	3.6258347	FALSE
go1aa	go1a	138337	0	1	1	0.0700	0.1100	11	5.76	0.003848	0.09503	0.0384531	FALSE
go1ab	go1a	138337	0	2	2	0.2900	0.2400	29	2.50	0.066052	0.045239	0.1391135	FALSE
go1ac	go1a	138337	0	3	3	0.1500	0.1800	18	2.56	0.017671	0.025447	0.0551915	FALSE
go1ae	go1a	138337	0	4	4	0.1500	0.1000	15	5.60	0.017671	0.007854	0.0714712	FALSE
go1af	go1a	138337	0	6	6	0.1100	0.2000	20	2.97	0.009503	0.031416	0.0607650	FALSE
go1af	go1a	138337	0	5	5	0.6400	0.6000	64	0.37	0.32699	0.282743	0.1118218	TRUE
go1ag	go1a	138337	0	7	7	0.1400	0.1200	14	1.50	0.015394	0.011310	0.0200276	FALSE
go1ag	go1a	138337	0	8	8	0.3400	0.3400	34	0.25	0.090792	0.090792	0.0226980	FALSE
go1ah	go1a	138337	0	13	13	0.1200	0.0800	12	2.00	0.011310	0.005027	0.0163363	FALSE
go1ah	go1a	138337	0	9	9	0.2400	0.1300	24	5.31	0.045239	0.013273	0.1553497	FALSE
go1ai	go1a	138337	0	11	11	0.3000	0.3800	38	5.00	0.070686	0.113411	0.4602429	FALSE
go1ai	go1a	138337	0	10	10	0.2400	0.3000	30	2.53	0.045239	0.070686	0.1466447	FALSE
go1ai	go1a	138337	0	12	12	0.4000	0.2900	40	2.96	0.125664	0.068052	0.2837390	FALSE
go1ai	go1a	138337	1	15	15	0.2400	0.1500	24	2.86	0.045239	0.017671	0.0896118	FALSE
go1ai	go1a	138337	1	14	14	3.0500	2.3000	305	1.00	7.30160	4.154753	5.7304565	TRUE
go1ai	go1a	138337	0	29	29	0.1800	0.1900	19	2.01	0.025447	0.028353	0.0564897	FALSE
go1ai	go1a	138337	0	24	24	0.1500	0.1400	15	2.01	0.017671	0.015394	0.0332306	FALSE
go1ai	go1a	138337	0	23	23	0.1100	0.1400	14	3.72	0.009503	0.015394	0.0463086	FALSE
go1ai	go1a	138337	0	32	32	0.1300	0.1000	13	2.40	0.013273	0.007854	0.0253526	FALSE
go1ai	go1a	138337	0	25	25	0.2500	0.2100	25	4.16	0.049087	0.034636	0.1741446	FALSE
go1ai	go1a	138337	0	31	31	0.1200	0.0600	12	4.03	0.011310	0.002827	0.0284864	FALSE
go1ai	go1a	138337	0	28	28	0.1000	0.1200	12	2.70	0.007854	0.011310	0.0258710	FALSE
go1ai	go1a	138337	0	33	33	0.2800	0.2800	28	2.59	0.061575	0.061575	0.1594797	FALSE
go1ai	go1a	138337	0	27	27	0.2300	0.2600	26	4.21	0.041548	0.053093	0.1992180	FALSE
go1ai	go1a	138337	0	32	32	0.1300	0.1000	13	2.40	0.013273	0.007854	0.0253526	FALSE
go1ai	go1a	138337	0	25	25	0.2500	0.2100	25	5.77	0.025447	0.045239	0.2039285	FALSE
go1ai	go1a	138337	0	30	30	0.2100	0.1800	21	3.44	0.034636	0.025447	0.1033426	FALSE
go1ai	go1a	138337	0	17	17	0.3800	0.2000	38	2.36	0.113411	0.031416	0.1708962	TRUE
go1ai	go1a	138337	0	18	18	0.2500	0.3300	33	2.06	0.049087	0.085530	0.1386556	FALSE

golai	gol1a	13837	0	21	0.2600	0.3100	31	5.48	0.053093	0.075477	0.3522806	FALSE
golai	gol1a	13837	0	20	1.3700	0.5500	137	2.57	1.474113	0.237583	2.1995285	TRUE
golai	gol1a	13837	0	16	1.0000	0.4400	100	1.60	0.785398	0.152033	0.7499604	TRUE
golai	gol1a	13837	0	19	0.5000	0.5500	55	2.34	0.196349	0.237583	0.5077006	TRUE
golai	gol1a	13837	0	22	0.3700	0.4600	46	3.48	0.107621	0.166190	0.4762572	FALSE
golai	gol1a	13837	1	36	0.1900	0.1800	19	2.61	0.028353	0.028353	0.0702086	FALSE
golai	gol1a	13837	1	35	0.1800	0.1600	18	1.80	0.025447	0.020106	0.0409977	FALSE
golai	gol1a	13837	1	39	0.1100	0.1200	12	2.35	0.009503	0.011310	0.0244553	FALSE
golai	gol1a	13837	1	40	0.2600	0.2400	26	1.10	0.053093	0.045239	0.0540825	FALSE
golai	gol1a	13837	1	41	0.2600	0.2600	26	1.97	0.053093	0.053093	0.1045930	FALSE
golai	gol1a	13837	1	42	0.2300	0.2600	26	1.65	0.041548	0.053093	0.0780783	FALSE
golai	gol1a	13837	1	34	0.2300	0.1800	23	6.90	0.041548	0.025447	0.2311307	FALSE
golai	gol1a	13837	1	37	0.2000	0.2000	20	2.91	0.031416	0.031416	0.0914203	FALSE
golai	gol1a	13837	1	38	0.3300	0.6600	66	3.63	0.085530	0.342119	0.77761828	FALSE
golai	gol1a	13837	0	59	0.1300	0.1800	18	4.98	0.013273	0.025447	0.0964130	FALSE
golai	gol1a	13837	0	50	0.1100	0.1600	16	3.51	0.009503	0.020106	0.0519646	FALSE
golai	gol1a	13837	0	52	0.1000	0.1600	16	5.51	0.007854	0.020106	0.0770302	FALSE
golai	gol1a	13837	0	56	0.1500	0.1300	15	2.79	0.017671	0.013273	0.0431678	FALSE
golai	gol1a	13837	0	55	0.1400	0.1100	14	4.16	0.015394	0.009503	0.0517860	FALSE
golai	gol1a	13837	0	57	0.0900	0.1100	11	3.26	0.006362	0.009503	0.0258800	FALSE
golai	gol1a	13837	0	53	0.2500	0.2300	25	1.90	0.049087	0.041548	0.0861031	FALSE
golai	gol1a	13837	0	43	0.2500	0.2200	25	3.94	0.049087	0.038013	0.1715881	FALSE
golai	gol1a	13837	0	45	0.2300	0.2000	23	3.09	0.041548	0.031416	0.1127285	FALSE
golai	gol1a	13837	0	46	0.2200	0.2200	22	5.21	0.038013	0.038013	0.1980490	FALSE
golai	gol1a	13837	0	60	0.2100	0.2200	22	3.56	0.034636	0.038013	0.1293157	FALSE
golai	gol1a	13837	0	47	0.2000	0.2200	22	1.30	0.031416	0.038013	0.0451289	FALSE
golai	gol1a	13837	0	49	0.2100	0.2100	21	2.46	0.034636	0.034636	0.0852046	FALSE
golai	gol1a	13837	0	48	0.1300	0.2100	21	5.04	0.013273	0.034636	0.1207313	FALSE
golai	gol1a	13837	0	51	0.2700	0.3000	30	4.38	0.05255	0.070686	0.2801913	FALSE
golai	gol1a	13837	0	54	0.6800	0.3800	68	2.46	0.363168	0.113411	0.5861924	TRUE
golai	gol1a	13837	0	58	0.2300	0.4500	45	7.10	0.041548	0.159043	0.7120964	TRUE
golai	gol1a	13837	0	44	0.2700	0.4000	40	6.74	0.05255	0.125664	0.6164373	FALSE
golai	gol1a	13837	1	61	0.1500	0.1300	15	7.68	0.017671	0.013273	0.1188275	FALSE
go1ba	go1b	13837	0	5	0.1500	0.1200	15	1.40	0.017671	0.01310	0.0202868	FALSE
go1ba	go1b	13837	0	6	0.1100	0.1300	13	1.30	0.009533	0.013273	0.0148047	FALSE
go1ba	go1b	13837	0	2	0.2900	0.2300	29	2.70	0.066932	0.041548	0.1452593	FALSE
go1ba	go1b	13837	0	4	0.2800	0.2900	29	2.90	0.061575	0.066052	0.1850593	FALSE
go1ba	go1b	13837	0	1	0.2300	0.1600	23	3.88	0.041548	0.020106	0.1196082	FALSE
go1ba	go1b	13837	0	3	0.4000	0.7900	79	2.58	0.125664	0.490167	0.7944209	FALSE
go1bb	go1b	13837	0	16	0.1400	0.1900	19	3.29	0.015394	0.028353	0.0719632	FALSE
go1bb	go1b	13837	0	30	0.1800	0.1500	18	2.15	0.025447	0.017671	0.0463522	FALSE
go1bb	go1b	13837	0	14	0.1800	0.1200	18	8.44	0.025447	0.01310	0.1551129	FALSE
go1bb	go1b	13837	0	9	0.1400	0.1500	15	2.10	0.015394	0.017671	0.0347185	FALSE
go1bb	go1b	13837	0	18	0.1100	0.1500	15	6.06	0.009503	0.017671	0.0687521	FALSE
go1bb	go1b	13837	0	7	0.1400	0.1400	14	1.73	0.015394	0.015394	0.0266313	FALSE
go1bb	go1b	13837	0	19	0.1100	0.1400	14	2.21	0.009503	0.015394	0.0275113	FALSE
go1bb	go1b	13837	0	17	0.1000	0.1400	14	3.83	0.007854	0.015394	0.0445195	FALSE

g01bb	g01b	13837	0	a	28	28	0.0700	0.1400	14	4.81	0.003848	0.015394	0.0462776	FALSE
g01bb	g01b	13837	0	a	29	29	0.1200	0.1300	13	3.73	0.011310	0.013273	0.0458472	FALSE
g01bb	g01b	13837	0	a	13	13	0.0900	0.1200	12	4.41	0.006362	0.011310	0.0389655	FALSE
g01bb	g01b	13837	0	a	3	3	0.0900	0.1100	11	4.54	0.006362	0.009503	0.0360136	FALSE
g01bb	g01b	13837	0	a	2	2	0.1000	0.0700	10	3.88	0.007854	0.003848	0.0227027	FALSE
g01bb	g01b	13837	0	a	24	24	0.2700	0.2600	27	3.76	0.057255	0.053093	0.2074549	FALSE
g01bb	g01b	13837	0	a	27	27	0.2300	0.2700	27	3.79	0.041548	0.057255	0.1872317	FALSE
g01bb	g01b	13837	0	a	15	15	0.2400	0.2600	26	2.75	0.045239	0.053093	0.1106232	FALSE
g01bb	g01b	13837	0	a	10	10	0.2000	0.2600	26	4.90	0.031416	0.053093	0.2070465	FALSE
g01bb	g01b	13837	0	a	32	32	0.2500	0.2500	25	1.75	0.049087	0.049087	0.0859029	FALSE
g01bb	g01b	13837	0	a	6	6	0.2300	0.2500	25	2.70	0.041548	0.049087	0.1223571	FALSE
g01bb	g01b	13837	0	a	11	11	0.1600	0.2400	24	3.24	0.020106	0.045239	0.1058590	FALSE
g01bb	g01b	13837	0	a	12	12	0.2200	0.2200	22	2.97	0.038013	0.038013	0.1128993	FALSE
g01bb	g01b	13837	0	a	1	1	0.1800	0.3800	38	4.47	0.025447	0.113411	0.3103483	FALSE
g01bb	g01b	13837	0	a	4	4	0.3100	0.3100	31	4.15	0.075477	0.075477	0.3132283	FALSE
g01bb	g01b	13837	0	a	26	26	1.6000	0.4500	160	2.14	2.010618	0.159043	2.3215368	TRUE
g01bb	g01b	13837	0	a	8	8	1.5000	0.9000	150	2.99	1.767144	0.636172	3.5929579	TRUE
g01bb	g01b	13837	0	a	25	25	0.4300	0.7500	75	1.00	0.145220	0.441786	0.23505030	TRUE
g01bb	g01b	13837	0	a	23	23	0.7000	0.2900	70	1.60	0.384845	0.066052	0.3607174	TRUE
g01bb	g01b	13837	0	a	20	20	0.6000	0.3100	60	1.00	0.282743	0.075477	0.1791099	TRUE
g01bb	g01b	13837	0	a	21	21	0.5900	0.3000	59	10.34	0.273397	0.076866	1.7789073	FALSE
g01bb	g01b	13837	0	a	5	5	0.4700	0.3000	47	8.92	0.173494	0.076866	1.0890432	FALSE
g01bb	g01b	13837	0	a	22	22	0.4000	0.1500	40	15.00	0.125664	0.017671	1.070128	FALSE
g01bb	g01b	13837	0	a	31	31	0.1700	0.4000	40	1.80	0.022698	0.125664	0.1333254	FALSE
g01bb	g01b	13837	1	a	34	34	0.1700	0.1900	19	2.60	0.022698	0.028353	0.0663661	FALSE
g01bb	g01b	13837	1	a	33	33	0.1200	0.1100	12	2.81	0.011310	0.009503	0.0282423	FALSE
g01bc	g01b	13837	0	a	5	5	0.1800	0.1800	18	6.14	0.025447	0.025447	0.1562438	FALSE
g01bc	g01b	13837	0	a	3	3	0.1300	0.1800	18	2.61	0.013273	0.025447	0.0505297	FALSE
g01bc	g01b	13837	0	a	2	2	0.1600	0.1600	16	3.67	0.020106	0.020106	0.0737897	FALSE
g01bc	g01b	13837	0	a	4	4	0.1500	0.1400	15	5.25	0.017671	0.015394	0.0867962	FALSE
g01bc	g01b	13837	0	a	7	7	0.2900	0.2800	29	1.80	0.066052	0.061575	0.1148644	FALSE
g01bc	g01b	13837	0	a	6	6	0.2900	0.2700	29	0.90	0.066052	0.057255	0.0554883	FALSE
g01bc	g01b	13837	0	a	1	1	0.3500	0.2900	35	4.30	0.096211	0.066052	0.3488657	FALSE
g01bd	g01b	13837	0	a	1	1	0.1300	0.1000	13	3.15	0.013273	0.007854	0.033253	FALSE
g01bd	g01b	13837	0	a	2	2	0.4000	0.4300	43	2.0	0.125664	0.145220	0.2708336	TRUE
g01be	g01b	13837	0	a	1	1	0.5500	0.3100	19	4.93	0.011310	0.028353	0.0977682	FALSE
g01bf	g01b	13837	0	a	1	1	0.2500	0.3000	30	7.03	0.049087	0.070686	0.4210025	FALSE
g01bh	g01b	13837	0	a	1	1	0.0900	0.1700	17	6.71	0.006362	0.022698	0.0974953	FALSE
g01bh	g01b	13837	0	a	2	2	0.0900	0.1600	16	6.79	0.006362	0.020106	0.0898385	FALSE
g01bh	g01b	13837	0	a	7	7	0.1700	0.2900	29	2.40	0.022698	0.066052	0.1064999	FALSE
g01bh	g01b	13837	0	a	6	6	0.1600	0.2000	20	1.60	0.020106	0.031416	0.0412177	FALSE
g01bh	g01b	13837	2	a	5	5	0.1700	0.1400	17	2.76	0.022698	0.015394	0.0525667	FALSE
g01bh	g01b	13837	2	a	4	4	0.2300	0.1600	23	1.85	0.041548	0.020106	0.0570297	FALSE
g01bh	g01b	13837	2	a	3	3	0.3000	0.1900	30	4.58	0.070686	0.028353	0.2267985	FALSE
g01bi	g01b	13837	0	a	3	3	0.1200	0.1600	16	2.20	0.011310	0.020106	0.0345575	FALSE
g01bi	g01b	13837	0	a	2	2	0.1500	0.1500	15	3.03	0.017671	0.017671	0.0535445	FALSE

g01b	g01b	13837	0	1	0.2200	0.1200	22	5.76	0.038013	0.011310	0.1420501	FALSE
g01b	g01b	13837	0	4	0.3600	0.5000	50	7.86	0.101788	0.196349	1.1716780	FALSE
g01b	g01b	13837	2	5	0.1200	0.1000	12	4.15	0.011310	0.011310	0.0397647	FALSE
g01b	g01b	13837	2	6	0.2300	0.2500	25	2.69	0.041548	0.049087	0.1219039	FALSE
g01b	g01b	13837	0	1	0.2700	0.2800	28	2.40	0.057255	0.061575	0.1425968	FALSE
g01b	g01b	13837	2	3	0.1900	0.1600	19	2.49	0.028353	0.020106	0.0603315	FALSE
g01b	g01b	13837	4	4	0.1400	0.1800	18	1.53	0.015394	0.025447	0.0312431	FALSE
g01b	g01b	13837	2	5	0.2400	0.2700	27	5.33	0.045239	0.057255	0.2731475	FALSE
g01b	g01b	13837	2	2	0.2200	0.2100	22	1.78	0.038013	0.034636	0.0646578	FALSE
g01ca	g01c	13837	0	1	0.1350	0.1100	14	1.00	0.014314	0.009503	0.0119086	FALSE
g01ca	g01c	13837	0	2	0.1200	0.0800	12	3.20	0.011310	0.005027	0.0261380	FALSE
g01cb	g01c	13837	0	6	0.0600	0.1800	18	6.90	0.002827	0.025447	0.0975464	FALSE
g01cb	g01c	13837	0	13	0.1400	0.1000	14	2.75	0.015394	0.007854	0.0319657	FALSE
g01cb	g01c	13837	0	7	0.2400	0.2400	24	2.50	0.045239	0.045239	0.1130972	FALSE
g01cb	g01c	13837	0	4	0.3700	0.2800	37	5.30	0.107521	0.061575	0.4481046	TRUE
g01cb	g01c	13837	3	3	0.3200	0.3500	35	3.60	0.080425	0.096211	0.3179446	FALSE
g01cb	g01c	13837	0	8	0.3200	0.3200	32	2.50	0.080425	0.080425	0.2010618	FALSE
g01cb	g01c	13837	0	5	0.4600	0.2100	46	9.50	0.166190	0.034636	0.95339242	FALSE
g01cc	g01c	13837	0	11	0.1150	0.1400	14	3.35	0.010387	0.015394	0.0431826	FALSE
g01cc	g01c	13837	0	12	0.1000	0.1130	11	2.90	0.007854	0.010029	0.0259299	FALSE
g01cc	g01c	13837	0	14	0.2000	0.1300	20	4.50	0.031416	0.013273	0.1005505	TRUE
g01cc	g01c	13837	0	10	1.8000	3.2000	320	1.00	0.254688	0.042470	5.2935792	TRUE
g01cc	g01c	13837	0	17	3.0700	1.7200	307	1.00	7.402293	2.323520	4.8629064	TRUE
g01cc	g01c	13837	0	9	0.5100	0.6000	60	3.20	0.204282	0.282743	0.7792400	TRUE
g01cc	g01c	13837	0	16	0.5400	0.5900	59	1.75	0.228022	0.273397	0.4396164	FALSE
g01cc	g01c	13837	0	15	0.4600	0.3700	46	1.90	0.166190	0.107521	0.2600255	FALSE
g01cc	g01c	13837	1	32	0.1600	0.1200	16	2.80	0.020106	0.011310	0.0439823	FALSE
g01cc	g01c	13837	2	35	0.1800	0.1300	18	4.50	0.025447	0.013273	0.0871202	FALSE
g01cc	g01c	13837	2	37	0.0900	0.1300	13	2.00	0.003362	0.013273	0.0196349	FALSE
g01cc	g01c	13837	2	34	0.2700	0.2200	27	2.89	0.057255	0.038013	0.1376633	FALSE
g01cc	g01c	13837	2	33	0.2500	0.2200	25	2.85	0.049087	0.038013	0.12411183	FALSE
g01cc	g01c	13837	2	38	0.1250	0.2200	22	5.95	0.012222	0.038013	0.1495981	FALSE
g01cc	g01c	13837	2	36	1.2000	1.2000	120	1.20	1.130972	1.130972	1.3571669	TRUE
g01cd	g01c	13837	0	22	0.1300	0.2400	24	4.25	0.013213	0.045239	0.1243382	FALSE
g01cd	g01c	13837	0	19	0.3300	0.3100	33	3.90	0.085630	0.075477	0.3139627	FALSE
g01cd	g01c	13837	0	18	0.2200	0.3000	30	4.10	0.038013	0.070686	0.2228330	FALSE
g01cd	g01c	13837	0	20	0.3500	0.4600	46	11.20	0.096211	0.166190	1.4694473	FALSE
g01cd	g01c	13837	1	30	0.1800	0.1000	18	5.50	0.026447	0.007854	0.0915773	FALSE
g01cd	g01c	13837	1	31	0.3500	0.0700	35	6.80	0.096211	0.003848	0.3402028	FALSE
g01cd	g01c	13837	2	27	0.1600	0.1000	16	2.75	0.020106	0.007854	0.0384452	FALSE
g01cd	g01c	13837	2	28	0.1300	0.1100	13	3.00	0.013273	0.009503	0.0341648	FALSE
g01cd	g01c	13837	2	29	0.1800	0.2100	21	2.75	0.025447	0.034636	0.0826140	FALSE
g01cd	g01c	13837	2	23	0.1400	0.2000	20	2.90	0.015394	0.031416	0.0678741	FALSE
g01cd	g01c	13837	2	24	0.6000	0.2600	60	7.30	0.282743	0.0563093	1.2258013	TRUE
g01cd	g01c	13837	2	25	0.4800	0.3900	48	20.50	0.180956	0.1119459	3.0792491	FALSE
g01cd	g01c	13837	2	21	0.2400	0.4300	43	1.70	0.045239	0.145220	0.1618901	FALSE

g01bi	g01b	13837	0	1	1	0.2200	0.1200	22	5.76	0.038013	0.011310	0.1420501	FALSE	
g01bi	g01b	13837	0	4	4	0.3600	0.5000	50	7.86	0.101788	0.196349	1.1716780	FALSE	
g01bi	g01b	13837	2	5	5	0.1200	0.1000	12	4.15	0.011310	0.007854	0.0397647	FALSE	
g01bi	g01b	13837	2	6	6	0.2300	0.2500	25	2.69	0.041548	0.049087	0.1219039	FALSE	
g01bi	g01b	13837	0	1	1	0.2100	0.2800	28	2.40	0.057255	0.061575	0.1425968	FALSE	
g01bi	g01b	13837	2	3	3	0.1900	0.1600	19	2.49	0.028353	0.020106	0.0603315	FALSE	
g01bi	g01b	13837	2	4	4	0.1400	0.1800	18	1.53	0.015394	0.025447	0.0312431	FALSE	
g01bi	g01b	13837	2	5	5	0.2400	0.2700	27	5.33	0.045239	0.057255	0.273145	FALSE	
g01bi	g01b	13837	2	2	2	0.2200	0.2100	22	1.78	0.038013	0.034636	0.0646578	FALSE	
g01cb	g01c	13837	0	1	1	0.1350	0.1100	14	1.00	0.014314	0.009503	0.0119086	FALSE	
g01ca	g01c	13837	0	2	2	0.1200	0.0800	12	3.20	0.011310	0.005027	0.0261380	FALSE	
g01cb	g01c	13837	0	6	6	0.0600	0.1800	18	6.90	0.002827	0.025447	0.0975464	FALSE	
g01cb	g01c	13837	2	13	13	0.1400	0.1000	14	2.75	0.015394	0.007854	0.0319657	FALSE	
g01cb	g01c	13837	2	7	7	0.2400	0.2400	24	2.50	0.045239	0.045239	0.1130972	FALSE	
g01cb	g01c	13837	0	4	4	0.3700	0.2800	37	5.30	0.107521	0.061575	0.4481046	TRUE	
g01cb	g01c	13837	0	3	3	0.3200	0.3500	35	3.60	0.080425	0.096211	0.3179446	FALSE	
g01cb	g01c	13837	0	8	8	0.3200	0.3200	32	2.50	0.080425	0.080425	0.2010618	FALSE	
g01cb	g01c	13837	0	5	5	0.4600	0.2100	46	9.50	0.166190	0.0539242	0.9539242	FALSE	
g01cc	g01c	13837	0	11	11	0.1150	0.1400	14	3.95	0.015394	0.0431826	0.0431826	FALSE	
g01cc	g01c	13837	0	12	12	0.1000	0.1130	11	2.90	0.007854	0.010029	0.0259299	FALSE	
g01cc	g01c	13837	0	14	14	0.2000	0.1300	20	4.50	0.031416	0.013273	0.1005505	TRUE	
g01cc	g01c	13837	0	10	10	1.8000	3.2000	320	1.00	2.544688	0.8042470	5.2935792	TRUE	
g01cc	g01c	13837	0	17	17	3.0700	1.7200	307	1.00	7.402293	2.323520	4.8629064	TRUE	
g01cc	g01c	13837	0	9	9	0.5100	0.6000	60	3.20	0.204282	0.282743	0.7792400	TRUE	
g01cc	g01c	13837	0	16	16	0.5400	0.5900	59	1.75	0.229022	0.273397	0.4396164	FALSE	
g01cc	g01c	13837	0	15	15	0.4600	0.3700	46	1.90	0.166190	0.107521	0.2600255	FALSE	
g01cc	g01c	13837	1	a	32	0.1600	0.1200	16	2.80	0.020106	0.011310	0.0439823	FALSE	
g01cc	g01c	13837	2		35	0.1800	0.1300	18	4.50	0.025447	0.013273	0.0871202	FALSE	
g01cc	g01c	13837	2		37	0.0900	0.1300	13	2.00	0.006362	0.013273	0.0196349	FALSE	
g01cc	g01c	13837	2		34	0.2700	0.2200	27	2.89	0.057255	0.038013	0.1376633	FALSE	
g01cc	g01c	13837	2		33	0.2500	0.2200	25	2.85	0.049087	0.038013	0.1241183	FALSE	
g01cc	g01c	13837	2		38	0.1250	0.2200	22	5.95	0.012272	0.038013	0.1495981	FALSE	
g01cc	g01c	13837	2		36	1.2000	1.2000	120	1.20	1.130972	1.130972	1.3571669	TRUE	
g01cd	g01c	13837	0	a	22	0.1300	0.2400	24	4.25	0.013273	0.045239	0.1243382	FALSE	
g01cd	g01c	13837	0		19	1.9	0.3300	0.3100	33	3.90	0.085630	0.075477	0.3139627	FALSE
g01cd	g01c	13837	0		18	0.2200	0.3000	30	4.10	0.038013	0.070686	0.2228330	FALSE	
g01cd	g01c	13837	0		20	0.3500	0.4600	46	11.20	0.096211	0.166190	1.4694473	FALSE	
g01cd	g01c	13837	1	a	30	0.1800	0.1000	18	5.50	0.025447	0.007854	0.0915773	FALSE	
g01cd	g01c	13837	1	a	31	0.3500	0.0700	35	6.80	0.096211	0.003848	0.302028	FALSE	
g01cd	g01c	13837	2	a	27	0.1600	0.1000	16	2.75	0.020106	0.007854	0.084452	FALSE	
g01cd	g01c	13837	2	a	28	0.1300	0.1100	13	3.00	0.013273	0.009503	0.0341648	FALSE	
g01cd	g01c	13837	2	a	29	0.1800	0.2100	21	2.75	0.025447	0.034636	0.0826140	FALSE	
g01cd	g01c	13837	2	a	23	0.1400	0.2000	20	2.90	0.015394	0.031416	0.0678741	FALSE	
g01cd	g01c	13837	2	a	26	0.8600	0.5300	86	0.88	0.580880	0.220618	0.326592	TRUE	
g01cd	g01c	13837	2	a	24	0.6000	0.2600	60	7.30	0.282743	0.053093	1.2258013	TRUE	
g01cd	g01c	13837	2	a	25	0.4800	0.3900	48	20.50	0.180956	0.119459	3.0794491	FALSE	
g01cd	g01c	13837	2	a	21	0.2400	0.4300	43	1.70	0.045239	0.1452220	0.1618901	FALSE	

go1ce	13837	0	40	0.2800	0.1000	28	9.00	0.061575	0.007854	0.3124311	FALSE
go1ce	13837	0	41	0.1400	0.3000	30	2.20	0.015394	0.070886	0.0946875	FALSE
go1ce	13837	0	39	0.6000	0.1600	60	8.85	0.282743	0.020106	1.3401080	TRUE
go1cf	13837	0	43	0.1800	0.0900	18	7.40	0.025447	0.006362	0.1176918	FALSE
go1cf	13837	0	45	0.1200	0.2000	20	7.22	0.011310	0.031416	0.1542395	FALSE
go1cf	13837	0	46	0.3100	0.3900	39	6.39	0.075477	0.119459	0.6228194	FALSE
go1cf	13837	0	44	0.4900	0.8400	84	1.20	0.188574	0.554176	0.4456502	TRUE
go1cf	13837	0	42	0.5700	0.4100	57	5.70	0.255176	0.132025	1.1035228	FALSE
go1cg	13837	0	47	1.7000	0.2900	170	2.40	2.269799	0.066052	2.8030208	TRUE
go1ch	13837	0	49	0.1600	0.0900	16	3.30	0.020106	0.006362	0.0436720	FALSE
go1ch	13837	0	52	1.7500	0.3800	175	1.45	2.405280	0.113411	1.8266512	TRUE
go1ch	13837	0	48	1.7500	0.3200	175	4.60	2.405280	0.080425	5.7171205	TRUE
go1ch	13837	0	51	1.4500	0.4300	145	1.15	1.6511298	0.145220	1.0329980	TRUE
go1ch	13837	0	50	1.2000	0.5100	120	2.20	1.1301972	0.204282	1.4687797	TRUE
go1ch	13837	0	54	0.5900	0.1700	59	2.82	0.273397	0.022698	0.4174937	FALSE
go1ci	13837	0	55	0.5000	0.5000	50	6.30	0.196349	0.196349	1.2370011	FALSE
go1ci	13837	0	53	0.4000	0.4700	47	3.70	0.125664	0.173494	0.56334421	FALSE
go1ci	13837	0	58	0.5700	1.8500	185	1.60	0.255176	2.688023	2.3545569	TRUE
go1ci	13837	0	56	0.9500	0.3000	95	6.90	0.708821	0.070686	2.6892992	TRUE
go1ci	13837	0	57	0.5000	0.3800	50	8.00	0.196349	0.113411	1.2390431	TRUE
go1cj	13837	0	63	0.1900	0.0650	19	3.00	0.028353	0.03318	0.0475067	FALSE
go1cj	13837	0	61	0.1600	0.1000	16	3.30	0.020106	0.07854	0.0461342	FALSE
go1cj	13837	0	59	0.2900	0.2200	29	5.60	0.066052	0.038013	0.2913825	FALSE
go1cj	13837	0	60	0.1700	0.2600	26	6.70	0.022698	0.053093	0.2538994	FALSE
go1cj	13837	0	72	2.4000	1.5000	240	1.15	4.522890	1.767144	3.6173445	FALSE
go1cj	13837	0	62	0.3800	0.4200	42	10.20	0.113411	0.138544	1.2849731	FALSE
go1cj	13837	3	69	0.1800	0.1000	18	3.57	0.025447	0.07854	0.0594420	FALSE
go1cj	13837	3	64	0.1500	0.1700	17	2.90	0.011671	0.022698	0.0585357	FALSE
go1cj	13837	3	74	0.1600	0.1300	16	4.70	0.020106	0.013273	0.0784416	FALSE
go1cj	13837	3	73	0.2300	0.2000	0.2000	4.70	0.017671	0.017671	0.0505403	FALSE
go1cj	13837	3	75	0.2000	0.0700	20	3.00	0.061575	0.028353	0.4181653	TRUE
go1cj	13837	3	65	0.2200	0.2800	28	3.40	0.038013	0.061575	0.1693003	FALSE
go1cj	13837	3	66	0.2600	0.2600	26	3.60	0.053093	0.053093	0.1911343	FALSE
go1cj	13837	3	73	0.2300	0.2000	23	3.00	0.041548	0.031416	0.1094451	FALSE
go1cj	13837	3	71	0.2800	0.1900	28	9.30	0.096211	0.045239	0.6577429	TRUE
go1cj	13837	3	67	0.3100	0.2800	31	3.00	0.075477	0.061575	0.2055778	FALSE
j1aa	9151	0	9	0.1300	0.1200	13	3.00	0.013273	0.011310	0.0368744	FALSE
j1aa	9151	0	4	0.2900	0.2000	29	4.80	0.066052	0.031416	0.2339228	FALSE
j1aa	9151	0	3	0.2200	0.2900	29	2.10	0.038013	0.066052	0.1092684	FALSE
j1aa	9151	0	2	0.1100	0.1900	19	2.86	0.009503	0.028353	0.0541343	FALSE
j1aa	9151	0	7	0.1000	0.1500	15	8.00	0.007854	0.017671	0.1021017	FALSE
j1aa	9151	0	9	0.1900	0.1800	19	6.50	0.028353	0.025447	0.1748491	FALSE
j1aa	9151	0	1	0.1100	0.1900	19	7.75	0.009503	0.028353	0.1466926	FALSE
j1aa	9151	0	2	0.1100	0.1900	19	2.86	0.009503	0.028353	0.0541343	FALSE
j1aa	9151	0	a	0.1000	0.1500	15	8.00	0.007854	0.017671	0.1021017	FALSE
j1aa	9151	0	a	0.1900	0.1800	19	6.50	0.028353	0.025447	0.1748491	FALSE
j1aa	9151	0	8	0.4600	0.4600	46	3.00	0.166190	0.166190	0.4985703	FALSE
j1ab	9151	0	10	0.1400	0.0700	14	4.80	0.015394	0.003848	0.0461814	FALSE

j1ac	j1a	9151	0		13	2.6000	2.6000	260	1.50	5.309287	5.309287	7.9639307	TRUE
j1ac	j1a	9151	0	b	11	0.3800	0.6300	63	8.00	0.113411	0.311724	1.7005427	TRUE
j1ad	j1a	9151	0	b	17	0.1700	0.1200	17	3.60	0.022698	0.011310	0.0612139	FALSE
j1ad	j1a	9151	0	b	16	0.1100	0.1500	15	3.50	0.009503	0.017671	0.0475558	FALSE
j1ad	j1a	9151	0	b	14	0.1000	0.1400	14	7.80	0.007864	0.015394	0.0906663	FALSE
j1ad	j1a	9151	0	b	19	0.1200	0.1300	13	2.00	0.011310	0.013273	0.0245829	FALSE
j1ad	j1a	9151	0	b	20	0.0800	0.1300	13	5.00	0.005027	0.013273	0.0457494	FALSE
j1ad	j1a	9151	0	b	21	0.2400	0.2900	29	4.20	0.045239	0.066052	0.2337107	FALSE
j1ad	j1a	9151	0	b	23	0.1700	0.2900	29	3.80	0.022698	0.066052	0.1686248	FALSE
j1ad	j1a	9151	0	b	25	0.2800	0.2400	28	5.00	0.061575	0.045339	0.2670352	FALSE
j1ad	j1a	9151	0	b	12	0.2800	0.0100	28	17.50	0.061575	0.000079	0.5394699	FALSE
j1ad	j1a	9151	0	b	26	0.2000	0.2600	26	2.10	0.031416	0.053093	0.0887342	FALSE
j1ad	j1a	9151	0	b	18	0.2500	0.2300	25	7.50	0.049087	0.041548	0.3398808	FALSE
j1ad	j1a	9151	0	b	22	0.2400	0.2400	24	1.86	0.045239	0.0841443	0.045239	FALSE
j1ad	j1a	9151	0	b	28	0.2000	0.2400	24	2.40	0.031416	0.045239	0.0919858	FALSE
j1ad	j1a	9151	0	b	27	0.1500	0.2100	21	7.50	0.017671	0.034636	0.961530	FALSE
j1ad	j1a	9151	0	b	24	0.2200	0.3400	34	5.20	0.038013	0.090792	0.3348935	FALSE
j1ad	j1a	9151	0	b	15	0.2000	0.3200	32	12.00	0.031416	0.080425	0.6710436	FALSE
j1ae	j1a	9151	0	c	30	0.2600	0.2900	29	2.90	0.053093	0.066052	0.1727600	FALSE
j1ae	j1a	9151	0	c	31	0.2300	0.2400	24	2.90	0.045239	0.12558403	0.12558403	FALSE
j1ae	j1a	9151	0	c	32	0.7500	0.3600	75	1.10	0.441786	0.101788	0.2999655	TRUE
j1ae	j1a	9151	0	c	33	0.4700	0.6100	61	1.60	0.173494	0.292246	0.3722926	TRUE
j1ae	j1a	9151	0	c	29	0.2000	0.4300	43	30.80	0.031416	0.145220	2.7201928	FALSE
j1af	j1a	9151	0	c	41	0.1600	0.1500	16	3.30	0.020106	0.017671	0.0624331	FALSE
j1af	j1a	9151	0	c	44	0.1500	0.1400	15	2.00	0.017671	0.015394	0.0330652	FALSE
j1af	j1a	9151	0	c	49	0.0900	0.1500	15	3.70	0.006362	0.017671	0.0446114	FALSE
j1af	j1a	9151	0	c	34	0.2400	0.2900	29	10.25	0.045239	0.066052	0.5703655	FALSE
j1af	j1a	9151	0	c	47	0.2600	0.1900	26	9.00	0.053093	0.028353	0.3665057	FALSE
j1af	j1a	9151	0	c	48	0.2500	0.2500	25	3.30	0.049087	0.049087	0.1619882	FALSE
j1af	j1a	9151	0	c	40	0.1400	0.2400	24	4.00	0.015394	0.045239	0.1212684	FALSE
j1af	j1a	9151	0	c	45	0.2100	0.2100	21	1.50	0.034636	0.034636	0.0519540	FALSE
j1af	j1a	9151	0	c	43	0.1400	0.2100	21	8.30	0.015394	0.034636	0.2076338	FALSE
j1af	j1a	9151	0	c	39	0.1800	0.2000	20	2.30	0.025447	0.031416	0.0653922	FALSE
j1af	j1a	9151	0	c	36	0.1300	0.3900	39	15.50	0.013273	0.119459	0.128674	TRUE
j1af	j1a	9151	0	c	46	0.2400	0.3600	36	12.00	0.045239	0.101788	0.8821585	FALSE
j1af	j1a	9151	0	c	38	0.20000	0.12000	200	1.50	0.145190	0.1130972	3.2044218	TRUE
j1af	j1a	9151	0	c	35	0.5900	0.3200	59	5.80	0.273397	0.080425	1.0260826	TRUE
j1af	j1a	9151	0	c	42	0.4800	0.4800	48	11.80	0.180956	0.180956	2.1352259	TRUE
j1af	j1a	9151	0	c	37	0.4600	0.3300	46	13.00	0.166190	0.085530	1.6361793	FALSE
j1ag	j1a	9151	0	c	85	0.0800	0.1400	14	3.30	0.005027	0.015394	0.0336936	FALSE
j1ag	j1a	9151	0	c	78	0.1200	0.1100	12	2.00	0.011310	0.009503	0.0208130	FALSE
j1ag	j1a	9151	0	c	55	0.1000	0.0700	10	3.60	0.00854	0.003848	0.0210644	FALSE
j1ag	j1a	9151	0	c	86	0.2900	0.2100	29	3.60	0.066052	0.034636	0.1812383	TRUE
j1ag	j1a	9151	0	c	52	0.2100	0.2800	28	10.46	0.034636	0.061575	0.5031845	FALSE
j1ag	j1a	9151	0	c	87	0.1500	0.2800	28	2.90	0.017671	0.061575	0.1149076	FALSE
j1ag	j1a	9151	0	c	88	0.2700	0.2700	27	2.50	0.057255	0.057255	0.1431387	FALSE
j1ag	j1a	9151	0	c	72	0.2700	0.0900	27	3.70	0.057255	0.066362	0.1176918	FALSE

j1aq	j1a	9151	0	c	71	0.1700	0.2700	27	2.20	0.022698	0.057255	0.0879488	FALSE
j1ag	j1a	9151	0	c	84	0.2500	0.1700	25	2.00	0.049087	0.022698	0.0717853	FALSE
j1ag	j1a	9151	0	c	81	0.1600	0.2400	24	2.20	0.020106	0.045239	0.0718796	FALSE
j1ag	j1a	9151	0	c	89	0.1700	0.2000	20	4.00	0.022298	0.031416	0.1082278	FALSE
j1ag	j1a	9151	0	c	82	0.3300	0.3800	38	3.30	0.085330	0.113411	0.3282530	FALSE
j1ag	j1a	9151	0	c	50	0.3100	0.3500	35	7.00	0.075477	0.096211	0.6009076	TRUE
j1ag	j1a	9151	0	c	80	0.3100	0.2700	31	4.00	0.075477	0.057255	0.2654644	FALSE
j1ag	j1a	9151	0	c	51	0.3000	0.10000	330	1.50	8.552979	0.785398	7.037822	TRUE
j1ag	j1a	9151	0	c	53	0.2900	0.4800	48	9.00	0.066052	0.180956	1.1115338	TRUE
j1ag	j1a	9151	0	c	77	0.4700	0.4700	47	3.00	0.173494	0.173494	0.5204829	FALSE
j1ag	j1a	9151	0	c	79	0.4700	0.4700	47	4.80	0.173494	0.173494	0.8327727	FALSE
j1ah	j1a	9151	0	c	73	0.3100	0.4400	44	7.60	0.075477	0.152053	0.8646127	FALSE
j1ag	j1a	9151	0	c	83	0.4300	0.4200	43	5.00	0.145220	0.138544	0.7094103	FALSE
j1ag	j1a	9151	0	c	54	0.4200	0.4200	42	2.00	0.138544	0.138544	0.2770882	FALSE
j1ah	j1a	9151	0	c	60	0.1900	0.1400	19	3.70	0.028353	0.013394	0.0809313	TRUE
j1ah	j1a	9151	0	c	65	0.1900	0.1900	19	3.60	0.028353	0.028353	0.1020703	FALSE
j1ah	j1a	9151	0	c	56	0.1000	0.1300	13	4.10	0.007854	0.013273	0.0433107	FALSE
j1ah	j1a	9151	0	c	67	0.2500	0.2800	28	5.20	0.049087	0.061575	0.2877225	FALSE
j1ah	j1a	9151	0	c	70	0.2500	0.2200	25	6.30	0.049087	0.038013	0.2743668	FALSE
j1ah	j1a	9151	0	c	62	0.2100	0.2300	23	4.10	0.034636	0.041548	0.5617763	FALSE
j1ah	j1a	9151	0	c	68	0.2100	0.2100	21	3.00	0.034636	0.034636	0.1039081	FALSE
j1ah	j1a	9151	0	c	61	0.1700	0.2100	21	3.50	0.022698	0.034636	0.1003345	FALSE
j1ah	j1a	9151	0	c	57	0.1100	0.2000	20	4.10	0.009503	0.031416	0.0838844	FALSE
j1ah	j1a	9151	0	c	64	0.3400	0.3600	36	5.30	0.090792	0.101788	0.5103356	FALSE
j1ah	j1a	9151	0	c	75	0.3400	0.2200	34	5.00	0.090792	0.038013	0.3220130	FALSE
j1ah	j1a	9151	0	c	74	0.3000	0.2700	30	4.40	0.070686	0.057255	0.2814708	FALSE
j1ah	j1a	9151	0	c	63	0.3000	0.2600	30	3.85	0.070686	0.053093	0.2382739	FALSE
j1ah	j1a	9151	0	c	76	0.3000	0.1600	30	4.20	0.070686	0.020106	0.19096631	FALSE
j1ah	j1a	9151	0	c	66	0.2900	0.3000	30	3.80	0.066052	0.070686	0.25998016	FALSE
j1ah	j1a	9151	0	c	58	0.2500	0.3000	300	1.00	4.908734	7.068578	5.9886559	TRUE
j1ah	j1a	9151	0	c	69	0.2000	0.2000	200	1.20	3.141590	3.141590	3.7699080	TRUE
j1ah	j1a	9151	0	c	59	1.5000	2.0000	200	0.60	1.767144	3.141590	1.4726223	TRUE
j1ai	j1a	9151	0	c	93	0.1200	0.0800	12	5.30	0.011310	0.005027	0.0432911	FALSE
j1ai	j1a	9151	0	c	92	0.1600	0.2100	21	5.30	0.020106	0.034636	0.1450668	FALSE
j1ai	j1a	9151	0	c	90	0.1900	0.3600	36	8.00	0.028353	0.101788	0.5205615	TRUE
j1ai	j1a	9151	0	c	91	0.3000	0.3300	33	7.90	0.070686	0.085530	0.6170515	FALSE
j1ai	j1a	9151	0	c	96	0.1200	0.1900	19	9.20	0.011310	0.096211	0.2742019	FALSE
j1ai	j1a	9151	0	c	103	0.1800	0.0700	18	6.50	0.02447	0.003848	0.0952098	FALSE
j1ai	j1a	9151	0	c	97	0.1300	0.0600	13	4.60	0.01273	0.002827	0.0370315	FALSE
j1ai	j1a	9151	0	c	94	0.1700	0.2600	26	11.50	0.022698	0.053093	0.4357974	FALSE
j1ai	j1a	9151	0	c	102	0.1700	0.2200	22	3.70	0.022698	0.038013	0.1123158	FALSE
j1ai	j1a	9151	0	c	99	0.3500	0.3500	35	2.85	0.096211	0.096211	0.2742019	FALSE
j1ai	j1a	9151	0	c	101	0.3400	0.3400	34	11.00	0.090792	0.090792	0.9987115	FALSE
j1ai	j1a	9151	0	c	98	0.3200	0.3200	32	5.60	0.080425	0.080425	0.4503783	FALSE
j1ai	j1a	9151	0	c	100	0.3100	0.3100	31	3.00	0.075477	0.075477	0.2264301	FALSE
j1ai	j1a	9151	0	c	95	1.5000	1.0000	150	0.50	1.76744	0.785398	0.6381355	TRUE
j1ai	j1a	9151	0	c	114	0.1800	0.1300	18	4.30	0.025447	0.013273	0.0832482	FALSE

ii1a	j1a	9151	0	106	106	0.1600	0.1800	18	5.80	0.020106	0.025447	0.1321039	FALSE
ii1a	j1a	9151	0	112	112	0.1300	0.1800	18	4.50	0.013273	0.0871202	0.053447	FALSE
ii1a	j1a	9151	0	110	110	0.1700	0.1700	17	2.00	0.022698	0.022698	0.053960	FALSE
ii1a	j1a	9151	0	108	108	0.0700	0.1700	17	9.30	0.003848	0.022668	0.1234409	FALSE
ii1a	j1a	9151	0	111	111	0.1600	0.1600	16	3.00	0.020106	0.020106	0.0603185	FALSE
ii1a	j1a	9151	0	104	104	0.1400	0.1400	16	5.50	0.020106	0.015394	0.0976249	FALSE
ii1a	j1a	9151	0	107	107	0.1300	0.1500	15	6.00	0.013273	0.017671	0.0928340	FALSE
ii1a	j1a	9151	0	116	116	0.1400	0.1300	14	3.00	0.015394	0.013273	0.0400005	FALSE
ii1a	j1a	9151	0	109	109	0.1200	0.1400	14	9.00	0.011310	0.015394	0.1201658	FALSE
ii1a	j1a	9151	0	115	115	0.1100	0.1100	11	3.40	0.009503	0.009503	0.0323113	FALSE
ii1a	j1a	9151	0	117	117	0.2200	0.2700	27	2.50	0.038013	0.057255	0.1190859	FALSE
ii1a	j1a	9151	0	113	113	0.1900	0.2400	24	5.00	0.028353	0.045239	0.1839794	FALSE
ii1a	j1a	9151	0	105	105	0.2000	0.2300	23	5.70	0.031416	0.041548	0.2079458	FALSE
ii1ba	j1b	9151	0	2	2	0.1800	0.1500	18	7.00	0.025447	0.017671	0.1509411	FALSE
ii1ba	j1b	9151	0	7	7	0.1800	0.1500	18	6.30	0.025447	0.017671	0.1358227	FALSE
ii1ba	j1b	9151	0	6	6	0.1500	0.1300	15	2.40	0.017671	0.013273	0.0371336	FALSE
ii1ba	j1b	9151	0	5	5	0.1400	0.1000	14	3.30	0.015394	0.007854	0.0383568	FALSE
ii1ba	j1b	9151	0	8	8	0.0800	0.1300	13	5.40	0.005027	0.013273	0.0494094	FALSE
ii1ba	j1b	9151	0	3	3	0.1200	0.1000	12	5.50	0.011310	0.007854	0.0527002	FALSE
ii1ba	j1b	9151	0	4	4	0.1100	0.1100	11	2.80	0.006503	0.009503	0.0266093	FALSE
ii1ba	j1b	9151	0	1	1	0.3000	0.2100	30	9.10	0.07686	0.034636	0.4792142	FALSE
ii1bb	j1b	9151	0	9	9	0.1700	0.1700	17	1.20	0.022698	0.0272376	0.022698	FALSE
ii1bb	j1b	9151	0	10	10	0.1400	0.1400	14	2.10	0.015394	0.015394	0.0323270	FALSE
ii1bc	j1b	9151	0	15	15	0.1000	0.1000	10	2.70	0.007854	0.007854	0.0212057	FALSE
ii1bc	j1b	9151	0	14	14	0.2500	0.2500	25	2.20	0.049087	0.049087	0.1079922	FALSE
ii1bc	j1b	9151	0	12	12	0.3900	0.2500	39	8.50	0.119459	0.049087	0.7163218	FALSE
ii1bc	j1b	9151	0	13	13	0.3300	0.2600	33	7.30	0.085530	0.053093	0.5059727	FALSE
ii1bc	j1b	9151	0	11	11	1.2000	1.2000	120	0.60	1.130972	1.130972	0.6778534	TRUE
ii1bc	j1b	9151	0	18	18	0.1100	0.1200	12	5.10	0.009503	0.011310	0.0530732	FALSE
ii1be	j1b	9151	0	17	17	0.2200	0.2500	25	4.70	0.038013	0.049087	0.2046864	FALSE
ii1be	j1b	9151	0	16	16	0.2200	0.1200	22	6.00	0.038013	0.011310	0.1479689	FALSE
ii1bf	j1b	9151	0	23	23	0.1100	0.1900	19	4.90	0.009503	0.028353	0.0927476	FALSE
ii1bf	j1b	9151	0	21	21	0.2300	0.1800	23	2.70	0.041548	0.025447	0.0904424	FALSE
ii1bf	j1b	9151	0	20	20	0.2000	0.2300	23	6.00	0.031416	0.041548	0.0948525	FALSE
ii1bg	j1b	9151	0	24	24	0.2600	0.3600	36	5.10	0.053093	0.101788	0.3949450	FALSE
ii1bg	j1b	9151	0	25	25	0.5000	1.6000	160	2.50	0.196349	0.010618	2.7587087	FALSE
ii1bg	j1b	9151	0	22	22	0.5400	0.4300	54	5.70	0.229022	0.145220	1.0665894	FALSE
ii1bg	j1b	9151	0	19	19	0.4100	0.3400	41	2.20	0.132025	0.090792	0.2450990	FALSE
ii1bg	j1b	9151	0	31	31	0.0400	0.0000	4	13.40	0.001257	0.000000	0.0084195	FALSE
ii1bg	j1b	9151	0	28	28	0.1700	0.1200	17	4.00	0.022698	0.011310	0.0680154	FALSE
ii1bg	j1b	9151	0	27	27	0.1400	0.1600	16	2.60	0.015394	0.020106	0.0461500	FALSE
ii1bg	j1b	9151	0	26	26	0.1200	0.1600	16	3.60	0.011310	0.020106	0.0565486	FALSE
ii1bg	j1b	9151	0	30	30	0.1500	0.2500	25	4.90	0.017671	0.049087	0.1635590	FALSE
ii1bg	j1b	9151	0	29	29	0.1700	0.2000	20	4.90	0.022698	0.031416	0.1325790	FALSE
ii1bg	j1b	9151	0	32	32	0.1700	0.2000	20	4.80	0.022698	0.031416	0.1298733	FALSE
ii1bg	j1b	9151	0	33	33	1.2000	0.5000	120	1.50	1.130972	0.196349	0.9954913	TRUE
ii1bh	j1b	9151	0	37	37	0.1800	0.1800	18	2.80	0.025447	0.025447	0.0712513	FALSE

ii1bh	ii1b	9151	0	39	39	0.1600	0.1600	0.1600	0.1600	0.1600	0.1600	16	2.60	0.020106	0.020106	0.0522761	0.0522761
ii1bh	ii1b	9151	0	34	34	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	16	2.90	0.007854	0.020106	0.0405422	0.0405422
ii1bh	ii1b	9151	0	36	36	0.1400	0.1400	0.1400	0.1400	0.1400	0.1400	14	3.80	0.015394	0.002827	0.0346203	0.0346203
ii1bh	ii1b	9151	0	38	38	0.0900	0.0900	0.0900	0.0900	0.0900	0.0900	12	5.10	0.006362	0.011310	0.0450622	0.0450622
ii1bh	ii1b	9151	0	35	35	0.4400	0.4400	0.4400	0.4400	0.4400	0.4400	51	2.20	0.152053	0.204282	0.3919683	0.3919683
ii1bh	ii1b	9151	0	41	41	0.1100	0.1100	0.1100	0.1100	0.1100	0.1100	17	4.70	0.009503	0.022698	0.076730	0.076730
ii1bh	ii1b	9151	0	42	42	0.1100	0.1100	0.1100	0.1100	0.1100	0.1100	11	7.40	0.009503	0.01257	0.0398118	0.0398118
ii1bh	ii1b	9151	0	40	40	0.0400	0.0400	0.0400	0.0400	0.0400	0.0400	10	10.00	0.001257	0.007854	0.0455531	0.0455531
ii1bh	ii1b	9151	0	46	46	0.1100	0.1100	0.1100	0.1100	0.1100	0.1100	16	2.70	0.009503	0.020106	0.0399728	0.0399728
ii1bh	ii1b	9151	0	43	43	0.1100	0.1100	0.1100	0.1100	0.1100	0.1100	11	3.60	0.009503	0.006362	0.0285571	0.0285571
ii1bh	ii1b	9151	0	45	45	0.2500	0.2500	0.2500	0.2500	0.2500	0.2500	25	2.30	0.049087	0.038013	0.1001657	0.1001657
ii1bh	ii1b	9151	0	44	44	0.2300	0.2300	0.2300	0.2300	0.2300	0.2300	23	4.30	0.041548	0.034636	0.1637946	0.1637946
ny1aa	ny1a	54353	0	2.	2.	0.0900	0.0900	0.0900	0.0900	0.0900	0.0900	9	2.50	0.006362	0.003848	0.0127627	0.0127627
ny1aa	ny1a	54353	0	1.	1.	0.0700	0.0700	0.0700	0.0700	0.0700	0.0700	15	5.40	0.003848	0.017671	0.0581037	0.0581037
ny1ab	ny1a	54353	0	3.	3.	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	13	3.00	0.007854	0.013273	0.0316908	0.0316908
ny1ac	ny1a	54353	0	5.	5.	0.0900	0.0900	0.0900	0.0900	0.0900	0.0900	13	2.70	0.006362	0.013273	0.0265012	0.0265012
ny1ac	ny1a	54353	0	4.	4.	0.2800	0.2800	0.2800	0.2800	0.2800	0.2800	28	2.20	0.061575	0.020106	0.0898495	0.0898495
ny1ai	ny1a	54353	0	6.	6.	0.1500	0.1500	0.1500	0.1500	0.1500	0.1500	15	8.10	0.017671	0.00707	0.0744321	0.0744321
ny1ai	ny1a	54353	0	7.	7.	0.1500	0.1500	0.1500	0.1500	0.1500	0.1500	15	10.70	0.017671	0.01257	0.1012632	0.1012632
ny1ba	ny1b	54353	0	1.	1.	0.0700	0.0700	0.0700	0.0700	0.0700	0.0700	37	12.80	0.003848	0.017521	0.71277639	0.71277639
ny1bb	ny1b	54353	0	2.	2.	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	10	2.60	0.007854	0.005027	0.0167447	0.0167447
ny1bb	ny1b	54353	0	5.	5.	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	150	1.60	0.785398	1.767144	2.0420335	2.0420335
ny1bd	ny1b	54353	0	3.	3.	0.2400	0.2400	0.2400	0.2400	0.2400	0.2400	24	6.00	0.04239	0.020106	0.1960352	0.1960352
ny1bf	ny1b	54353	0	4.	4.	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	13	2.40	0.013273	0.006362	0.0235619	0.0235619
ol1ab	ol1a	25429	0	1.	1.	0.1800	0.1800	0.1800	0.1800	0.1800	0.1800	18	2.00	0.025447	0.020106	0.0455531	0.0455531
ol1ab	ol1a	25429	0	4.	4.	0.0800	0.0800	0.0800	0.0800	0.0800	0.0800	11	2.20	0.005027	0.009503	0.0159828	0.0159828
ol1ab	ol1a	25429	0	3.	3.	0.2400	0.2400	0.2400	0.2400	0.2400	0.2400	24	9.80	0.043239	0.015394	0.2971002	0.2971002
ol1ab	ol1a	25429	0	2.	2.	0.1000	0.1000	0.1000	0.1000	0.1000	0.1000	34	4.10	0.007854	0.090792	0.2022241	0.2022241
ol1ad	ol1a	25429	0	5.	5.	0.2700	0.2700	0.2700	0.2700	0.2700	0.2700	27	2.70	0.057255	0.017671	0.1011513	0.1011513
ol1ae	ol1a	25429	0	7.	7.	0.0900	0.0900	0.0900	0.0900	0.0900	0.0900	18	2.40	0.006362	0.025447	0.0381703	0.0381703
ol1ae	ol1a	25429	0	6.	6.	0.2300	0.2300	0.2300	0.2300	0.2300	0.2300	23	3.40	0.041548	0.017671	0.1006723	0.1006723
ol1ah	ol1a	25429	0	10.	10.	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	17	2.00	0.013273	0.022698	0.0359712	0.0359712
ol1ah	ol1a	25429	0	13.	13.	0.3700	0.3700	0.3700	0.3700	0.3700	0.3700	37	13.00	0.107521	0.006362	0.7402371	0.7402371
ol1ah	ol1a	25429	0	11.	11.	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	200	2.60	0.196349	3.141590	4.3393212	4.3393212
ol1ah	ol1a	25429	0	9.	9.	0.3700	0.3700	0.3700	0.3700	0.3700	0.3700	55	2.00	0.107521	0.235783	0.3451037	0.3451037
ol1ah	ol1a	25429	0	8.	8.	0.0700	0.0700	0.0700	0.0700	0.0700	0.0700	43	24.50	0.003848	0.145220	1.8260885	1.8260885
ol1ai	ol1a	25429	0	12.	12.	0.6700	0.6700	0.6700	0.6700	0.6700	0.6700	67	2.10	0.352565	0.352565	0.7403864	0.7403864
ol1ba	ol1b	25429	0	2.	2.	0.0800	0.0800	0.0800	0.0800	0.0800	0.0800	18	2.60	0.005027	0.025447	0.0396154	0.0396154
ol1ba	ol1b	25429	0	3.	3.	0.7200	0.7200	0.7200	0.7200	0.7200	0.7200	72	3.00	0.015394	0.0407150	0.0204203	0.0204203
ol1ba	ol1b	25429	0	5.	5.	0.4700	0.4700	0.4700	0.4700	0.4700	0.4700	47	0.40	0.173494	0.070686	0.6532544	0.6532544
ol1ba	ol1b	25429	0	a.	a.	0.4700	0.4700	0.4700	0.4700	0.4700	0.4700	41	6.40	0.125664	0.132025	0.8246045	0.8246045
ol1bc	ol1b	25429	0	12.	12.	0.1400	0.1400	0.1400	0.1400	0.1400	0.1400	14	6.50	0.015394	0.003848	0.0625373	0.0625373
ol1bc	ol1b	25429	0	10.	10.	0.1400	0.1400	0.1400	0.1400	0.1400	0.1400	14	9.60	0.015394	0.000079	0.0742672	0.0742672

o11bc	25429	0	14	0.0700	0.1300	13	4.00	0.003848	0.013273	0.034233	FALSE
o11bc	25429	0	13	0.1100	0.0900	11	4.80	0.009503	0.006362	0.0380761	FALSE
o11bc	25429	0	11	0.1100	0.0300	11	6.10	0.009503	0.000707	0.0311410	FALSE
o11bc	25429	0	9	0.2100	0.0100	21	15.70	0.034636	0.000079	0.2725094	FALSE
o11be	25429	0	16	0.1400	0.1100	14	2.90	0.015394	0.009503	0.0361008	FALSE
o11be	25429	0	15	0.1900	0.2000	20	2.00	0.028353	0.031416	0.05597687	FALSE
o11bf	25429	0	18	0.0700	0.1900	19	8.60	0.003848	0.028353	0.1384656	FALSE
o11bf	25429	0	24	0.1800	0.1500	18	2.30	0.025447	0.017671	0.0495861	FALSE
o11bf	25429	0	26	0.1800	0.0400	18	5.10	0.025447	0.001257	0.0680340	FALSE
o11bf	25429	0	21	0.2100	0.0600	21	11.00	0.034636	0.002827	0.2060490	FALSE
o11bf	25429	0	22	0.1100	0.2100	21	6.50	0.009503	0.034636	0.1434529	FALSE
o11bf	25429	0	23	0.2000	0.3100	31	7.10	0.031416	0.075477	0.3794687	FALSE
o11bf	25429	0	20	0.1400	0.3100	31	4.10	0.015394	0.075477	0.1862845	FALSE
o11bf	25429	0	19	1.0000	0.6000	100	2.40	0.785398	1.2817887	TRUE	
o11bf	25429	0	17	0.1400	0.4700	47	10.80	0.015394	0.173494	0.199957	TRUE
o11bf	25429	0	25	0.4700	0.3300	47	6.40	0.173494	0.085530	0.8288771	FALSE
o11g	25429	0	27	0.2800	0.0200	28	14.20	0.061575	0.000314	0.4394142	FALSE
o11i	25429	0	28	0.0700	0.1100	11	3.70	0.003848	0.009503	0.0247008	FALSE
o11j	25429	0	29	0.2000	0.1500	20	2.60	0.031416	0.017671	0.0638135	FALSE
o11ca	25429	0	3	0.0800	0.1500	15	4.00	0.005027	0.017671	0.0453960	FALSE
o11ca	25429	0	6	0.1300	0.0600	13	2.70	0.013273	0.02827	0.0217359	FALSE
o11ca	25429	0	5	0.2500	0.1800	25	3.00	0.040087	0.025447	0.1118013	FALSE
o11ca	25429	0	2	0.3400	0.3800	38	3.70	0.090792	0.113411	0.3777762	FALSE
o11ca	25429	0	4	2.0000	1.0000	200	2.30	3.14590	0.785398	4.5160356	TRUE
o11ca	25429	0	1	0.7300	0.4500	73	11.30	0.415838	0.159043	3.2633345	TRUE
o11cb	25429	0	7	0.0900	0.1100	11	5.00	0.006352	0.009503	0.0396626	FALSE
o11cb	25429	0	12	0.2200	0.2300	23	2.50	0.038013	0.041548	0.0994510	FALSE
o11cb	25429	0	13	0.1200	0.2100	21	2.90	0.011310	0.034636	0.0666213	FALSE
o11cb	25429	0	8	0.1100	0.2100	21	2.60	0.009533	0.034636	0.0573811	FALSE
o11cb	25429	0	11	0.3400	0.2200	34	3.90	0.090792	0.038013	0.2511701	FALSE
o11cb	25429	0	10	0.6500	2.0000	200	2.00	0.331830	3.141590	3.4734204	TRUE
o11cb	25429	0	9	0.4000	0.2400	40	7.60	0.125664	0.045239	0.6494295	TRUE
o11cc	25429	0	15	0.1000	0.1800	18	2.30	0.007854	0.025447	0.0382960	FALSE
o11cc	25429	0	14	0.2300	0.2400	24	4.00	0.041548	0.045239	0.1735728	FALSE
o11cc	25429	0	16	0.0700	0.2300	23	5.70	0.003848	0.015458	0.1293785	FALSE
o11cd	25429	0	18	0.2800	0.1100	28	3.10	0.061575	0.009503	0.1101716	FALSE
o11cf	25429	0	17	0.2400	0.2000	24	2.10	0.045239	0.031416	0.0804875	FALSE
o11cf	25429	0	20	0.2000	0.9000	200	3.40	3.141590	0.636172	6.4221954	TRUE
o11cg	25429	0	19	0.5800	0.7900	79	6.00	0.264208	0.490167	2.2631229	TRUE
o11ci	25429	0	21	0.2200	0.2500	25	6.00	0.038013	0.049087	0.2613017	FALSE
o11ci	25429	0	29	0.1400	0.1700	17	2.60	0.015394	0.022698	0.0495193	FALSE
o11ci	25429	0	27	0.1400	0.0400	14	6.60	0.015394	0.001257	0.0549464	FALSE
o11ci	25429	0	30	0.1100	0.0300	11	4.80	0.009503	0.000707	0.0245044	FALSE
o11ci	25429	0	22	0.2500	0.1900	25	4.50	0.049087	0.028353	0.1742404	FALSE
o11ci	25429	0	28	0.2000	0.0400	20	10.30	0.031416	0.001257	0.1682636	FALSE
o11ci	25429	0	23	0.3200	0.3200	32	2.30	0.080425	0.080425	0.1849768	FALSE
o11ci	25429	0	26	0.2900	0.4700	47	7.70	0.066052	0.173494	0.9222530	FALSE

o1c	o1c	25429	0	33	33	0.1100	0.0900	11	3.60	0.009503	0.006362	0.0285571	FALSE
o1c	o1c	25429	0	31	31	0.3900	0.1300	39	8.60	0.119459	0.013273	0.5707484	FALSE
o1c	o1c	25429	0	24	24	2.0000	0.0090	200	3.20	3.141590	0.000064	5.0266458	TRUE
o1c	o1c	25429	0	32	32	0.4200	0.1000	42	15.20	0.138544	0.007854	1.126255	FALSE
re1aa	re1a	3982	0	a	4	0.1800	0.1600	18	2.68	0.025447	0.020106	0.010411	FALSE
re1aa	re1a	3982	0	a	7	0.1500	0.1500	15	0.017671	0.01671	0.0353429	FALSE	
re1aa	re1a	3982	0	a	3	0.2200	0.1700	22	4.07	0.038013	0.022698	0.1235473	FALSE
re1aa	re1a	3982	0	a	9	0.2000	0.0100	20	1.80	0.031416	0.000079	0.0283450	TRUE
re1aa	re1a	3982	0	a	6	0.2000	0.2000	20	2.00	0.031416	0.0628318	0.031416	FALSE
re1aa	re1a	3982	0	a	1	0.3500	0.2900	35	7.50	0.096211	0.066052	0.6084867	FALSE
re1aa	re1a	3982	0	a	2	0.3200	0.3500	35	3.97	0.080425	0.096211	0.3566223	FALSE
re1aa	re1a	3982	0	a	5	0.3400	0.3400	34	2.09	0.090792	0.090792	0.1897552	FALSE
re1aa	re1a	3982	0	a	8	0.5900	0.3700	59	3.10	0.273397	0.107521	0.5904226	FALSE
re1aa	re1a	3982	0	a	11	0.4300	0.0120	43	2.00	0.145220	0.000113	0.1453331	TRUE
re1aa	re1a	3982	0	a	10	0.4000	0.2300	40	6.40	0.125664	0.041548	0.5350756	FALSE
re1ab	re1a	3982	0	a	14	1.0000	2.0000	200	2.70	0.785398	3.141590	5.3014331	TRUE
re1ab	re1a	3982	0	a	13	0.1600	0.1600	16	2.00	0.020106	0.020106	0.0402124	FALSE
re1ab	re1a	3982	0	a	12	0.3300	0.3200	33	2.90	0.085530	0.080425	0.2405340	FALSE
re1ac	re1a	3982	0	a	17	0.6000	0.5000	60	1.10	0.282743	0.196349	0.2635609	TRUE
re1ac	re1a	3982	0	a	15	0.2000	0.2200	22	5.90	0.031416	0.038013	0.2048160	FALSE
re1ac	re1a	3982	0	a	18	0.2000	0.2000	20	3.30	0.031416	0.031416	0.1036725	FALSE
re1ac	re1a	3982	0	a	19	0.2000	0.2000	20	3.30	0.031416	0.031416	0.1036725	FALSE
re1ac	re1a	3982	0	a	16	0.4000	0.4000	40	1.90	0.125664	0.125664	0.2387008	FALSE
re1ad	re1a	3982	0	a	30	0.1900	0.1800	19	3.30	0.028353	0.025447	0.0887696	FALSE
re1ad	re1a	3982	0	a	22	0.1800	0.1800	18	2.30	0.025447	0.025447	0.0585278	FALSE
re1ad	re1a	3982	0	a	29	0.1400	0.1000	14	2.50	0.015394	0.007854	0.0290597	FALSE
re1ad	re1a	3982	0	a	23	0.1700	0.2900	29	9.80	0.022698	0.066052	0.4348746	FALSE
re1ad	re1a	3982	0	a	27	0.2600	0.2400	26	3.50	0.053093	0.045239	0.1720806	FALSE
re1ad	re1a	3982	0	a	21	0.2500	0.2500	25	2.30	0.049087	0.049087	0.1129009	FALSE
re1ad	re1a	3982	0	a	28	0.2300	0.2100	23	3.80	0.041548	0.034636	0.1447488	FALSE
re1ad	re1a	3982	0	a	25	0.1800	0.2000	20	3.50	0.022447	0.031416	0.0995099	FALSE
re1ad	re1a	3982	0	a	24	0.3000	0.3000	30	5.40	0.07686	0.070686	0.3817032	FALSE
re1ad	re1a	3982	0	a	20	0.6000	0.5800	60	6.80	0.282743	0.284208	1.8596328	FALSE
re1ad	re1a	3982	0	a	26	0.4500	0.4000	45	4.30	0.15043	0.125664	0.6121192	FALSE
re1ae	re1a	3982	0	a	35	0.2500	0.2500	25	2.20	0.049087	0.049087	0.1079922	FALSE
re1ae	re1a	3982	0	a	32	0.1800	0.2200	22	2.00	0.025447	0.038013	0.0634601	FALSE
re1ae	re1a	3982	0	a	31	0.3500	0.3000	35	7.90	0.096211	0.070686	0.6592430	FALSE
re1ae	re1a	3982	0	a	36	0.9000	1.2000	120	1.80	0.636172	1.130972	1.5904299	TRUE
re1ae	re1a	3982	0	a	34	0.9000	1.1500	115	2.00	0.636172	1.038688	1.6748602	TRUE
re1ae	re1a	3982	0	a	33	0.4400	0.3600	44	4.90	0.152053	0.101788	0.6219092	FALSE
re1af	re1a	3982	0	a	37	0.2200	0.3400	34	14.70	0.038013	0.090792	0.9467181	FALSE
re1af	re1a	3982	0	a	38	0.8500	1.8000	180	1.80	0.567450	2.544688	2.8009238	TRUE
re1af	re1a	3982	0	a	39	0.8500	1.8000	180	1.80	0.567450	2.544688	2.8009238	FALSE
re1ag	re1a	3982	0	a	42	0.1700	0.1700	17	2.50	0.022698	0.022698	0.0567450	FALSE
re1ag	re1a	3982	0	a	43	0.1400	0.1600	16	3.90	0.015394	0.020106	0.0692249	FALSE
re1ag	re1a	3982	0	a	40	1.5000	2.0000	200	3.50	1.767144	3.141590	8.5902852	TRUE
re1ag	re1a	3982	0	a	41	0.9200	0.7000	92	1.40	0.664760	0.384845	0.7347237	FALSE

re1ah	re1a	3982	0	44	0.2400	0.3400	34	6.60	0.045239	0.090792	0.4489018	FALSE	
re1ah	re1a	3982	0	45	0.2800	0.3000	30	1.90	0.061675	0.070886	0.1256479	FALSE	
re1ai	re1a	3982	0	48	0.9000	0.6000	90	1.90	0.636172	0.2822473	0.8129693	TRUE	
re1ai	re1a	3982	0	47	0.1600	0.2000	20	2.00	0.020106	0.031416	0.0515221	FALSE	
re1aj	re1a	3982	0	51	0.2800	0.3200	32	1.90	0.061575	0.080425	0.1348999	FALSE	
re1aj	re1a	3982	0	51	0.2600	0.2600	26	2.00	0.053093	0.053093	0.1061857	FALSE	
re1aj	re1a	3982	0	50	0.2400	0.2400	24	2.00	0.045239	0.045239	0.0904778	FALSE	
re1aj	re1a	3982	0	49	0.1700	0.2300	23	2.90	0.022698	0.041548	0.0931560	FALSE	
re1ba	re1b	3982	0	2	0.2300	0.1700	23	1.50	0.041548	0.022698	0.0481841	FALSE	
re1ba	re1b	3982	0	5	0.2000	0.1400	20	4.10	0.031416	0.015394	0.0955999	FALSE	
re1ba	re1b	3982	0	3	0.2000	0.1100	20	1.80	0.031416	0.009503	0.0368873	FALSE	
re1bb	re1b	3982	0	4	0.1600	0.2000	20	2.20	0.020106	0.031416	0.0566743	FALSE	
re1bb	re1b	3982	0	6	0.3600	0.3300	36	4.30	0.101788	0.085530	0.4027322	FALSE	
re1bb	re1b	3982	0	1	0.3100	0.3200	32	5.00	0.075477	0.080425	0.3897535	FALSE	
re1bb	re1b	3982	0	7	0.3100	0.2400	31	3.80	0.075477	0.045239	0.2293596	FALSE	
re1bb	re1b	3982	0	14	0.1700	0.1200	17	2.40	0.022698	0.011310	0.040893	FALSE	
re1bb	re1b	3982	0	12	0.2300	0.1900	23	1.80	0.041548	0.028353	0.0629103	FALSE	
re1bb	re1b	3982	0	8	0.2000	0.2100	21	5.40	0.031416	0.034636	0.1783402	FALSE	
re1bb	re1b	3982	0	9	0.1600	0.2100	21	4.50	0.020106	0.034636	0.1231700	FALSE	
re1bb	re1b	3982	0	11	0.2000	0.2000	20	1.80	0.031416	0.0565486	0.0565486	FALSE	
re1bb	re1b	3982	0	10	0.3500	0.2400	35	1.90	0.096211	0.045239	0.1343776	FALSE	
re1bb	re1b	3982	0	13	0.9000	0.7000	90	1.80	0.636172	0.384845	0.9189151	TRUE	
re1bc	re1b	3982	0	18	0.1800	0.1800	18	2.00	0.025447	0.025447	0.0508938	FALSE	
re1bc	re1b	3982	0	16	0.2300	0.2600	26	2.40	0.041548	0.053093	0.1135685	FALSE	
re1bc	re1b	3982	0	17	1.6000	2.0000	200	3.50	0.201618	3.141590	9.0163683	TRUE	
re1bc	re1b	3982	0	15	0.4800	0.4000	48	2.80	0.18956	0.125664	0.4292669	FALSE	
re1bd	re1b	3982	0	21	0.1800	0.1500	18	4.20	0.025447	0.017671	0.0905485	FALSE	
re1bd	re1b	3982	0	37	0.1300	0.1700	17	4.10	0.013273	0.022698	0.0737410	FALSE	
re1bd	re1b	3982	0	35	0.1400	0.1400	14	2.00	0.013394	0.015394	0.0307876	FALSE	
re1bd	re1b	3982	0	41	0.1400	0.1400	14	6.90	0.015394	0.1062172	0.1062172	FALSE	
re1bd	re1b	3982	0	b	69	0.2900	29	4.20	0.066052	0.066052	0.2774181	FALSE	
re1bd	re1b	3982	0	19	0.2800	0.2800	28	3.60	0.061575	0.061575	0.2216706	FALSE	
re1bd	re1b	3982	0	20	0.2800	0.2800	28	2.50	0.061575	0.1539379	0.1539379	FALSE	
re1bd	re1b	3982	0	43	0.2700	0.2700	27	4.10	0.057255	0.057255	0.2347475	FALSE	
re1bd	re1b	3982	0	74	0.2500	0.2500	25	3.20	0.049087	0.049087	0.1570795	FALSE	
re1bd	re1b	3982	0	39	0.2400	0.2400	24	3.10	0.045239	0.045239	0.1492406	FALSE	
re1bd	re1b	3982	0	45	0.2400	0.2300	24	3.00	0.045239	0.041548	0.1301796	FALSE	
re1bd	re1b	3982	0	a	31	0.2400	0.2000	24	3.80	0.045239	0.031416	0.1456441	FALSE
re1bd	re1b	3982	0	a	29	0.2200	0.2200	22	5.50	0.038013	0.038013	0.2090728	FALSE
re1bd	re1b	3982	0	24	0.2100	0.2100	21	3.10	0.034636	0.034636	0.1073717	FALSE	
re1bd	re1b	3982	0	a	34	0.2000	0.2000	20	2.00	0.031416	0.031416	0.0628318	FALSE
re1bd	re1b	3982	0	b	67	0.2000	0.2000	20	2.00	0.031416	0.031416	0.0628318	FALSE
re1bd	re1b	3982	0	a	30	0.3500	0.3500	35	2.50	0.096211	0.096211	0.2405280	FALSE
re1bd	re1b	3982	0	b	26	0.3300	0.2800	33	2.00	0.085530	0.081575	0.1471050	FALSE
re1bd	re1b	3982	0	b	71	0.3000	0.3000	30	6.50	0.070686	0.070686	0.4594575	FALSE
re1bd	re1b	3982	0	b	73	0.2000	0.9000	220	2.00	3.801324	0.636172	4.4374959	TRUE
re1bd	re1b	3982	0	38	0.6300	0.6300	63	5.00	0.311724	0.311724	1.5586213	FALSE	

re1bd	re1b	3982	0	b	70	70	0.6000	0.6000	60	6.70	0.282743	0.282743	1.8943788	FALSE
re1bd	re1b	3982	0	a	42	42	0.5100	0.5100	51	2.80	0.204282	0.204282	0.5719893	FALSE
re1bd	re1b	3982	0	a	25	25	0.5000	0.4000	50	3.30	0.196349	0.125664	0.5313214	FALSE
re1bd	re1b	3982	0	a	36	36	0.4000	0.5000	50	5.40	0.125664	0.196349	0.8694350	FALSE
re1bd	re1b	3982	0	b	66	66	0.4800	0.4800	48	4.80	0.180956	0.180956	0.8685868	FALSE
re1bd	re1b	3982	0	a	22	22	0.4400	0.4400	48	2.20	0.152053	0.180956	0.3663094	FALSE
re1bd	re1b	3982	0	a	28	28	0.4500	0.4700	47	7.10	0.159043	0.173494	1.1805074	FALSE
re1bd	re1b	3982	0	a	44	44	0.4500	0.4400	45	5.90	0.159043	0.162053	0.9177331	FALSE
re1bd	re1b	3982	0	b	68	68	0.4400	0.4400	44	4.50	0.152053	0.162053	0.6842383	FALSE
re1bd	re1b	3982	0	a	40	40	0.4200	0.4000	42	4.20	0.138544	0.125664	0.5548362	FALSE
re1bd	re1b	3982	0	a	27	27	0.3700	0.4200	42	9.40	0.107521	0.138544	1.565057	FALSE
re1bd	re1b	3982	0	a	23	23	0.3600	0.4200	42	7.00	0.101788	0.138544	0.8411607	FALSE
re1bd	re1b	3982	0	a	32	32	0.4000	0.4000	40	3.30	0.125664	0.125664	0.4146899	FALSE
re1bd	re1b	3982	0	a	33	33	0.4000	0.4000	40	3.80	0.125664	0.125664	0.4775217	FALSE
re1bd	re1b	3982	0	b	72	72	0.3800	0.4000	40	4.60	0.113411	0.125664	0.5498725	FALSE
re1be	re1b	3982	0	b	53	53	0.1800	0.1500	18	2.00	0.025447	0.017671	0.0431183	FALSE
re1be	re1b	3982	0	b	77	77	0.1300	0.0800	13	3.50	0.013273	0.005027	0.030246	FALSE
re1be	re1b	3982	0	a	76	76	0.1000	0.1000	10	3.20	0.007854	0.007854	0.0251327	FALSE
re1be	re1b	3982	0	b	49	49	0.2900	0.2900	29	2.40	0.086052	0.066052	0.1535246	FALSE
re1be	re1b	3982	0	b	50	50	0.2900	0.2900	29	3.30	0.066052	0.066052	0.2179714	FALSE
re1be	re1b	3982	0	b	56	56	0.2800	0.2600	28	2.80	0.061575	0.053093	0.160352	FALSE
re1be	re1b	3982	0	b	78	78	0.2200	0.1700	22	3.40	0.038013	0.022698	0.1032091	FALSE
re1be	re1b	3982	0	b	62	62	0.2000	0.2000	20	4.00	0.031416	0.031416	0.1256636	FALSE
re1be	re1b	3982	0	b	55	55	0.3800	0.3500	38	3.30	0.113411	0.096211	0.3458773	FALSE
re1be	re1b	3982	0	b	57	57	0.3600	0.3600	36	5.40	0.101788	0.101788	0.5496626	FALSE
re1be	re1b	3982	0	b	65	65	0.3200	0.3200	32	2.70	0.080425	0.080425	0.2171467	FALSE
re1be	re1b	3982	0	b	46	46	0.3100	0.2800	31	12.20	0.075477	0.061575	0.8360164	FALSE
re1be	re1b	3982	0	b	58	58	0.3000	0.3000	30	3.50	0.070686	0.070686	0.2474402	FALSE
re1be	re1b	3982	0	b	59	59	0.3000	0.3000	30	1.90	0.070686	0.070686	0.1343030	FALSE
re1be	re1b	3982	0	b	63	63	0.3000	0.3000	30	2.60	0.070686	0.070686	0.1837830	FALSE
re1be	re1b	3982	0	b	64	64	0.3000	0.3000	30	3.70	0.070686	0.070686	0.2615374	FALSE
re1be	re1b	3982	0	b	75	75	1.9000	1.8000	190	2.50	0.283585	0.2544688	6.7249661	TRUE
re1be	re1b	3982	0	b	54	54	0.5500	0.5500	55	9.50	0.237583	0.237583	2.2570361	FALSE
re1be	re1b	3982	0	b	48	48	0.5200	0.5200	52	5.50	0.212371	0.212371	0.5309287	FALSE
re1be	re1b	3982	0	b	60	60	0.5200	0.5200	52	6.90	0.212371	0.212371	1.4653632	FALSE
re1be	re1b	3982	0	b	47	47	0.5000	0.5000	50	6.30	0.196349	0.196349	1.2370011	FALSE
re1bf	re1b	3982	0	b	51	51	0.4800	0.4800	48	6.00	0.180956	0.180956	1.0857335	FALSE
re1bf	re1b	3982	0	b	61	61	0.4000	0.4000	40	7.10	0.125664	0.125664	0.8922116	FALSE
re1bf	re1b	3982	0	b	52	52	0.4000	0.3000	40	3.00	0.125664	0.070686	0.2945241	FALSE
re1bf	re1b	3982	0	b	86	86	0.1100	0.1100	11	1.90	0.009503	0.009503	0.0180563	FALSE
re1bf	re1b	3982	0	b	82	82	0.2500	0.2300	25	1.80	0.049087	0.041548	0.0815714	FALSE
re1bf	re1b	3982	0	b	84	84	0.3500	0.3500	35	2.00	0.096211	0.096211	1.1924224	FALSE
re1bf	re1b	3982	0	b	80	80	0.3300	0.3000	33	3.10	0.085530	0.070686	0.2421341	FALSE
re1bf	re1b	3982	0	b	85	85	0.3100	0.3100	31	2.00	0.075477	0.075477	0.1509534	FALSE
re1bf	re1b	3982	0	b	81	81	0.3100	0.2100	31	2.00	0.075477	0.034636	0.1101127	FALSE
re1bf	re1b	3982	0	b	83	83	1.0000	0.8000	100	1.50	0.785398	0.502654	0.9660389	TRUE
re1bf	re1b	3982	0	b	79	79	0.8000	0.4200	80	6.60	0.502654	0.38544	2.1159551	FALSE

re1bg	re1b	3982	0	c	93	93	0.1700	0.1800	18	2.80	0.022698	0.025447	0.0674028	FALSE
re1bg	re1b	3982	0	c	95	95	0.1500	0.1800	18	2.30	0.017671	0.025447	0.0459861	FALSE
re1bg	re1b	3982	0	c	99	99	0.1100	0.1200	12	2.10	0.009503	0.011310	0.0218537	FALSE
re1bg	re1b	3982	0	c	89	89	0.2500	0.2500	25	3.30	0.049087	0.049087	0.1619882	FALSE
re1bg	re1b	3982	0	c	102	102	0.2400	0.1700	24	3.10	0.045239	0.022698	0.1053022	FALSE
re1bg	re1b	3982	0	c	94	94	0.2100	0.2300	23	4.40	0.034636	0.041548	0.1676038	FALSE
re1bg	re1b	3982	0	c	97	97	0.2200	0.1900	22	3.60	0.038013	0.028353	0.1194590	FALSE
re1bg	re1b	3982	0	c	92	92	0.2000	0.2000	20	2.60	0.031416	0.031416	0.0816813	FALSE
re1bg	re1b	3982	0	c	100	100	1.1000	0.7000	110	1.00	0.950331	0.384845	0.6675879	TRUE
re1bg	re1b	3982	0	c	96	96	0.7000	1.0000	100	1.50	0.384845	0.785398	0.8776817	TRUE
re1bg	re1b	3982	0	c	90	90	0.6000	0.6200	62	3.50	0.282743	0.301907	1.0231373	FALSE
re1bg	re1b	3982	0	c	88	88	0.5300	0.3700	53	3.00	0.220618	0.107521	0.4922086	FALSE
re1bg	re1b	3982	0	c	87	87	0.3800	0.4700	47	3.90	0.113411	0.173494	0.5594661	FALSE
re1bg	re1b	3982	0	c	91	91	0.4400	0.4500	45	3.80	0.152053	0.159043	0.5910823	FALSE
re1bg	re1b	3982	0	c	101	101	0.3300	0.4200	42	8.20	0.085530	0.138544	0.9187030	FALSE
re1bg	re1b	3982	0	c	98	98	0.3800	0.4000	40	2.20	0.113411	0.125664	0.2629825	FALSE
re1bh	re1b	3982	0	c	107	107	0.2800	0.2800	28	3.30	0.061575	0.061575	0.2031980	FALSE
re1bh	re1b	3982	0	c	106	106	0.1700	0.2400	24	4.30	0.02698	0.045239	0.1460643	FALSE
re1bh	re1b	3982	0	c	103	103	0.1800	0.2200	22	2.30	0.025447	0.038013	0.0729791	FALSE
re1bh	re1b	3982	0	c	105	105	0.2900	0.3000	30	2.10	0.066052	0.070686	0.1435746	FALSE
re1bh	re1b	3982	0	c	104	104	0.4200	0.3900	42	3.20	0.138544	0.119459	0.4128049	FALSE
re1bi	re1b	3982	0	c	111	111	0.1000	0.1000	10	2.20	0.007854	0.007854	0.0172787	FALSE
re1bi	re1b	3982	0	c	115	115	0.2300	0.2800	28	7.50	0.041548	0.061575	0.3867101	FALSE
re1bi	re1b	3982	0	c	110	110	0.2700	0.2000	27	2.90	0.057255	0.031416	0.1285735	FALSE
re1bi	re1b	3982	0	c	119	119	0.2400	0.2300	24	4.90	0.045239	0.041548	0.2126267	FALSE
re1bi	re1b	3982	0	c	113	113	0.2400	0.2200	24	4.90	0.045239	0.038013	0.2039677	FALSE
re1bi	re1b	3982	0	c	109	109	0.2300	0.2300	23	2.40	0.041548	0.041548	0.0997141	FALSE
re1bi	re1b	3982	0	c	120	120	0.3600	0.3600	36	2.10	0.101788	0.101788	0.2137538	FALSE
re1bi	re1b	3982	0	c	121	121	0.3500	0.3600	36	2.00	0.096211	0.101788	0.1979987	FALSE
re1bi	re1b	3982	0	c	118	118	0.2500	0.3000	30	2.00	0.049087	0.070686	0.1197731	FALSE
re1bi	re1b	3982	0	c	108	108	1.5000	1.7000	170	2.60	1.767144	2.265799	5.2480261	TRUE
re1bi	re1b	3982	0	c	114	114	0.4000	0.5200	52	7.50	0.125664	0.212371	1.2676316	FALSE
re1bi	re1b	3982	0	c	116	116	0.4500	0.4900	49	6.70	0.159043	0.188574	1.1645167	FALSE
re1bi	re1b	3982	0	c	117	117	0.4000	0.4000	40	3.90	0.125664	0.125664	0.4900880	FALSE
re1bi	re1b	3982	0	c	112	112	0.4000	0.3500	40	8.90	0.125664	0.098211	0.9873428	FALSE
re1bi	re1b	3982	0	c	122	122	0.1400	0.1400	14	2.00	0.015394	0.015394	0.0307876	FALSE
re1bj	re1b	3982	0	c	123	123	0.1300	0.1100	13	2.10	0.013273	0.009503	0.0239154	FALSE
wh1aa	wh1a	24296	0	c	4	4	0.0500	0.2300	23	14.80	0.001963	0.041548	0.3219816	FALSE
wh1aa	wh1a	24296	0	c	6	6	0.2100	0.0400	21	12.90	0.034636	0.001257	0.2315077	FALSE
wh1aa	wh1a	24296	0	c	7	7	0.1800	0.0200	18	14.00	0.025447	0.002827	0.1979202	FALSE
wh1aa	wh1a	24296	0	c	5	5	0.1500	0.1600	16	2.00	0.0117671	0.020106	0.0377776	FALSE
wh1aa	wh1a	24296	0	c	1	1	0.1100	0.1500	15	4.90	0.009503	0.017671	0.0665781	FALSE
wh1aa	wh1a	24296	0	c	4	4	0.0500	0.2300	23	14.80	0.001963	0.041548	0.3219816	FALSE
wh1aa	wh1a	24296	0	c	3	3	0.1800	0.0200	18	9.80	0.025447	0.001257	0.2315077	FALSE
wh1aa	wh1a	24296	0	c	5	5	0.1500	0.1600	16	2.00	0.0117671	0.020106	0.0377776	FALSE
wh1ab	wh1a	24296	0	c	9	9	0.1400	0.1400	14	1.90	0.015394	0.015394	0.0292482	FALSE
wh1ab	wh1a	24296	0	c	8	8	0.2200	0.1600	22	11.60	0.038013	0.020106	0.3370926	FALSE
wh1ac	wh1a	24296	0	c	12	12	0.1600	0.1100	16	2.00	0.020106	0.009503	0.0296095	FALSE

wh1ac	wh1a	24296	0	11	0.1500	0.0800	15	5.70	0.017671	0.005027	0.0646893	FALSE	
wh1ac	wh1a	24296	0	14	0.0600	0.1200	12	5.00	0.002827	0.01310	0.0353429	FALSE	
wh1ac	wh1a	24296	0	13	0.1800	0.2400	24	6.70	0.025447	0.045239	0.2367973	FALSE	
wh1ad	wh1a	24296	0	10	0.2200	0.0900	22	4.80	0.038013	0.006362	0.164999	FALSE	
wh1ad	wh1a	24296	0	15	0.1600	0.1600	16	6.80	0.020106	0.020106	0.1367220	FALSE	
wh1ad	wh1a	24296	0	16	0.1600	0.1600	16	4.20	0.020106	0.020106	0.0844459	FALSE	
wh1ad	wh1a	24296	0	20	0.1200	0.1400	14	2.00	0.011310	0.015394	0.0267035	FALSE	
wh1ad	wh1a	24296	0	30	0.0700	0.1300	13	5.30	0.003848	0.013273	0.0453724	FALSE	
wh1ad	wh1a	24296	0	18	0.0700	0.2400	24	3.50	0.003848	0.045249	0.0859029	FALSE	
wh1ad	wh1a	24296	0	19	0.19	0.2300	23	8.70	0.041548	0.038013	0.3460893	FALSE	
wh1ad	wh1a	24296	0	17	0.17	0.2000	23	3.10	0.031416	0.041548	0.1130933	FALSE	
wh1ad	wh1a	24296	0	29	0.29	0.3400	34	2.00	0.090792	0.090792	0.1815839	FALSE	
wh1ae	wh1a	24296	0	31	0.1800	0.1900	19	2.60	0.025447	0.028353	0.0699396	FALSE	
wh1ae	wh1a	24296	0	25	0.1800	0.0300	18	13.40	0.025447	0.000707	0.172300	FALSE	
wh1ae	wh1a	24296	0	24	0.0900	0.1100	11	4.20	0.006362	0.009503	0.0333166	FALSE	
wh1ae	wh1a	24296	0	34	0.0600	0.1000	10	4.00	0.002827	0.007864	0.0213628	FALSE	
wh1ae	wh1a	24296	0	35	0.2900	0.2000	29	3.00	0.066052	0.031416	0.142017	FALSE	
wh1ae	wh1a	24296	0	26	0.2300	0.1700	23	8.00	0.041548	0.022698	0.2569821	FALSE	
wh1ae	wh1a	24296	0	22	0.2200	0.1800	22	2.40	0.038013	0.025447	0.0761521	FALSE	
wh1ae	wh1a	24296	0	27	0.27	0.2000	1900	3.50	0.031416	0.028353	0.1049553	FALSE	
wh1ae	wh1a	24296	0	23	0.2000	0.1800	20	2.40	0.031416	0.025447	0.0682953	FALSE	
wh1ae	wh1a	24296	0	21	0.2300	0.3400	34	3.80	0.041548	0.090792	0.2514450	FALSE	
wh1ae	wh1a	24296	0	28	0.3100	0.0700	31	16.40	0.075477	0.003848	0.6504662	FALSE	
wh1ae	wh1a	24296	0	32	0.32	0.3500	56	4.80	0.096211	0.246301	0.8220284	TRUE	
wh1af	wh1a	24296	0	36	0.36	0.1400	17	7.70	0.015394	0.022698	0.1466653	FALSE	
wh1af	wh1a	24296	0	40	0.40	0.0500	13	8.20	0.001963	0.013273	0.0624705	FALSE	
wh1af	wh1a	24296	0	37	0.37	0.1100	12	3.10	0.009503	0.011310	0.0322662	FALSE	
wh1af	wh1a	24296	0	38	0.38	0.1800	23	3.00	0.025447	0.041548	0.1004916	FALSE	
wh1af	wh1a	24296	0	39	0.39	0.2100	1900	21	2.90	0.034636	0.028353	0.0913339	FALSE
wh1ag	wh1a	24296	0	42	0.42	0.0400	1200	12	7.10	0.001257	0.011310	0.0446106	FALSE
wh1ag	wh1a	24296	0	41	0.41	0.1000	3600	36	16.70	0.001854	0.101788	0.9155064	FALSE
wh1ah	wh1a	24296	0	47	0.47	0.1300	1700	17	2.40	0.013273	0.022698	0.0431654	FALSE
wh1ah	wh1a	24296	0	45	0.45	0.2900	1700	29	12.20	0.086652	0.022698	0.5413745	FALSE
wh1ah	wh1a	24296	0	44	0.44	0.2700	1500	27	9.30	0.05255	0.017671	0.3484102	FALSE
wh1ai	wh1a	24296	0	46	0.46	0.1300	3400	34	17.00	0.013273	0.090792	0.8846539	FALSE
wh1ai	wh1a	24296	0	33	0.33	0.0600	5400	54	27.80	0.002827	0.229022	0.2227059	FALSE
wh1ai	wh1a	24296	0	48	0.48	0.4000	4500	45	5.60	0.125664	0.159043	0.7971785	FALSE
wh1ai	wh1a	24296	0	49	0.49	0.1900	6000	19	13.90	0.028333	0.002827	0.2167030	FALSE
wh1ai	wh1a	24296	0	51	0.51	0.1700	1700	17	4.50	0.022698	0.01310	0.1021409	FALSE
wh1ai	wh1a	24296	0	56	0.56	0.1300	1200	13	2.00	0.013273	0.011310	0.02455829	FALSE
wh1ai	wh1a	24296	0	50	0.50	0.1100	6000	11	5.90	0.009503	0.002827	0.0363757	FALSE
wh1ai	wh1a	24296	0	43	0.43	0.0100	2200	22	20.00	0.000079	0.038013	0.3809178	FALSE
wh1ai	wh1a	24296	0	55	0.55	0.0700	2000	20	12.30	0.003848	0.031416	0.2168757	FALSE
wh1ai	wh1a	24296	0	54	0.54	0.0900	1200	12	3.70	0.006362	0.011310	0.0326922	FALSE
wh1ai	wh1a	24296	0	53	0.53	0.2000	2200	22	4.80	0.031416	0.038013	0.1666299	FALSE
wh1ai	wh1a	24296	0	52	0.52	0.1800	2200	22	7.00	0.025447	0.038013	0.2221104	FALSE
wh1ai	wh1b	24296	0	18	0.18	0.1500	1900	19	7.20	0.0117671	0.028353	0.1656875	FALSE

wh1ba	wh1b	24296	0	2	0.0500	0.1700	17	9.00	0.001983	0.022698	0.11109767	FALSE
wh1ba	wh1b	24296	0	15	0.1600	0.1100	16	2.80	0.020106	0.009503	0.0414533	FALSE
wh1ba	wh1b	24296	0	9	0.1500	0.1500	15	7.90	0.017671	0.017671	0.1396044	FALSE
wh1ba	wh1b	24296	0	7	0.1300	0.1500	15	2.00	0.013223	0.017671	0.0309447	FALSE
wh1ba	wh1b	24296	0	6	0.1100	0.1400	14	2.40	0.009503	0.015394	0.0298765	FALSE
wh1ba	wh1b	24296	0	16	0.0900	0.1400	14	8.10	0.006362	0.015394	0.0881098	FALSE
wh1ba	wh1b	24296	0	11	0.0400	0.1300	13	6.20	0.001267	0.013273	0.0450425	FALSE
wh1ba	wh1b	24296	0	8	0.2500	0.2000	25	4.30	0.049087	0.031416	0.1730820	FALSE
wh1ba	wh1b	24296	0	19	0.1900	0.2400	24	4.20	0.028353	0.045239	0.1545427	FALSE
wh1ba	wh1b	24296	0	10	0.2200	0.1000	22	9.50	0.038013	0.007854	0.2178693	FALSE
wh1ba	wh1b	24296	0	13	0.2100	0.2100	21	2.70	0.034636	0.034636	0.0935173	FALSE
wh1ba	wh1b	24296	0	12	0.2000	0.1500	20	6.50	0.031416	0.017671	0.1595339	FALSE
wh1ba	wh1b	24296	0	14	0.3500	0.3500	35	2.00	0.096211	0.096211	0.1924224	FALSE
wh1ba	wh1b	24296	0	3	0.2700	0.3500	35	7.50	0.057255	0.096211	0.57555000	FALSE
wh1ba	wh1b	24296	0	1	0.1700	0.3100	31	5.00	0.022698	0.075477	0.2454367	FALSE
wh1ba	wh1b	24296	0	4	0.3000	0.1700	30	7.50	0.070686	0.022698	0.3501891	FALSE
wh1ba	wh1b	24296	0	5	0.2700	0.3000	30	8.50	0.057255	0.070686	0.5437503	FALSE
wh1ba	wh1b	24296	0	17	0.5800	0.5800	58	3.20	0.264208	0.264208	0.845647	FALSE
wh1bb	wh1b	24296	0	23	0.1200	0.0900	12	2.50	0.011310	0.006362	0.02220893	FALSE
wh1bb	wh1b	24296	0	29	0.2800	0.2800	28	6.00	0.031416	0.01575	0.27789732	FALSE
wh1bb	wh1b	24296	0	20	0.2500	0.1800	25	6.00	0.049087	0.025447	0.2238627	FALSE
wh1bb	wh1b	24296	0	21	0.2100	0.0900	21	9.50	0.034636	0.006362	0.1947393	FALSE
wh1bb	wh1b	24296	0	24	0.2100	0.0800	21	9.00	0.034636	0.005027	0.17784816	FALSE
wh1bb	wh1b	24296	0	22	0.0600	0.2000	20	16.90	0.002827	0.031416	0.2893561	FALSE
wh1bc	wh1b	24296	0	34	0.1200	0.1500	15	6.30	0.011310	0.017671	0.0912907	FALSE
wh1bc	wh1b	24296	0	27	0.1400	0.1400	14	5.60	0.015394	0.015394	0.0862052	FALSE
wh1bc	wh1b	24296	0	28	0.1300	0.1400	14	3.80	0.013273	0.015394	0.0544673	FALSE
wh1bc	wh1b	24296	0	35	0.1000	0.1300	13	2.50	0.007854	0.013273	0.0264090	FALSE
wh1bc	wh1b	24296	0	25	0.2600	0.0600	26	13.40	0.05093	0.002827	0.37466660	FALSE
wh1bc	wh1b	24296	0	31	0.1400	0.2400	24	11.00	0.015394	0.045239	0.3334798	FALSE
wh1bc	wh1b	24296	0	26	0.2100	0.2300	23	7.60	0.034636	0.041548	0.2894975	FALSE
wh1bc	wh1b	24296	0	32	0.0700	0.2200	22	8.20	0.003848	0.038013	0.1716329	FALSE
wh1bc	wh1b	24296	0	33	0.0800	0.2100	21	9.20	0.005027	0.034636	0.1824478	FALSE
wh1bc	wh1b	24296	0	30	0.3800	0.2800	38	3.50	0.113411	0.061575	0.3062265	FALSE
wh1bd	wh1b	24296	0	36	0.1400	0.1900	19	8.70	0.015394	0.028353	0.1902979	FALSE
wh1bd	wh1b	24296	0	42	0.1500	0.1800	18	2.00	0.017671	0.025447	0.04311183	FALSE
wh1bd	wh1b	24296	0	37	0.0600	0.1800	18	10.60	0.002827	0.025447	0.1498638	FALSE
wh1bd	wh1b	24296	0	39	0.1100	0.1600	16	4.90	0.009503	0.020106	0.0725432	FALSE
wh1bd	wh1b	24296	0	40	0.1100	0.1100	11	2.60	0.009503	0.009503	0.0247086	FALSE
wh1bd	wh1b	24296	0	38	0.2900	0.1800	29	8.90	0.060502	0.025447	0.4071697	FALSE
wh1bd	wh1b	24296	0	41	0.1700	0.2200	22	2.50	0.022698	0.038013	0.0758890	FALSE
wh1bd	wh1b	24296	0	45	0.1900	0.2000	20	2.30	0.028353	0.031416	0.0687341	FALSE
wh1bd	wh1b	24296	0	43	0.3100	0.3100	31	4.00	0.075477	0.075477	0.3019068	FALSE
wh1be	wh1b	24296	0	48	0.1700	0.1300	17	6.00	0.022698	0.013273	0.1079136	FALSE
wh1be	wh1b	24296	0	47	0.1600	0.0900	16	11.90	0.020106	0.006362	0.1574840	FALSE
wh1be	wh1b	24296	0	50	0.1500	0.1100	15	4.70	0.017671	0.009503	0.0638607	FALSE
wh1be	wh1b	24296	0	56	0.0900	0.1300	13	5.60	0.006362	0.013273	0.0549778	FALSE

wh1be	wh1b	24296	0	46	46	0.2300	0.1400	23	15.70	0.041548	0.015394	0.4469894	FALSE
wh1be	wh1b	24296	0	49	49	0.2100	0.2200	22	2.00	0.034636	0.038013	0.0726493	FALSE
wh1be	wh1b	24296	0	44	44	0.0800	0.5100	51	26.00	0.005027	0.204282	2.721096	FALSE
wh1bf	wh1b	24296	0	57	57	0.0700	0.1500	15	6.20	0.003848	0.017671	0.0667117	FALSE
wh1bf	wh1b	24296	0	54	54	0.0700	0.1200	12	6.20	0.003848	0.011310	0.0469903	FALSE
wh1bf	wh1b	24296	0	53	53	0.0900	0.2600	26	13.30	0.006362	0.053093	0.3955730	FALSE
wh1bf	wh1b	24296	0	51	51	0.0900	0.2300	23	11.20	0.006362	0.041548	0.2629118	FALSE
wh1bf	wh1b	24296	0	52	52	0.2000	0.3800	38	15.00	0.031416	0.113411	1.0882047	FALSE
wh1bf	wh1b	24296	0	55	55	0.1700	0.3000	30	13.80	0.022698	0.070686	0.6443480	FALSE
wh1bg	wh1b	24296	0	61	61	0.0500	0.1900	19	8.20	0.001963	0.028353	0.1242970	FALSE
wh1bg	wh1b	24296	0	60	60	0.1300	0.1800	18	8.20	0.013273	0.025447	0.1587524	FALSE
wh1bh	wh1b	24296	0	62	62	0.1500	0.1700	17	5.00	0.017671	0.022698	0.1009236	FALSE
wh1bh	wh1b	24296	0	63	63	0.0300	0.1600	16	10.50	0.000707	0.020106	0.1092284	FALSE
wh1bh	wh1b	24296	0	58	58	0.2600	0.3300	33	6.50	0.053093	0.085530	0.4505236	FALSE
wh1bh	wh1b	24296	0	59	59	0.3100	0.3100	31	2.00	0.075477	0.075477	0.1509334	FALSE
wh1bh	wh1b	24296	0	64	64	0.2200	0.1700	22	5.00	0.038013	0.022698	0.1517781	FALSE
wh1bh	wh1b	24296	0	65	65	0.2200	0.1600	22	5.00	0.038013	0.020106	0.1452995	FALSE
wh1bh	wh1b	24296	0	66	66	0.1400	0.2200	22	6.80	0.015394	0.038013	0.1815839	FALSE
wh1bh	wh1b	24296	0	67	67	0.3000	0.2700	30	5.00	0.07686	0.057255	0.3198531	FALSE
wh1bh	wh1b	24296	0	68	68	0.4100	0.3400	41	4.00	0.132025	0.009008	0.2658665	FALSE
wh1bi	wh1b	24296	0	70	70	0.1000	0.1700	17	10.00	0.007854	0.022698	0.1527598	FALSE
wh1bi	wh1b	24296	0	72	72	0.1200	0.1400	14	6.90	0.011310	0.015394	0.0921271	FALSE
wh1bi	wh1b	24296	0	69	69	0.0800	0.1200	12	5.40	0.000527	0.011310	0.0441079	FALSE
wh1bi	wh1b	24296	0	87	87	0.1100	0.0400	11	1.00	0.005053	0.001257	0.0053800	FALSE
wh1bi	wh1b	24296	0	73	73	0.0800	0.1100	11	5.20	0.005027	0.009503	0.0377778	FALSE
wh1bi	wh1b	24296	0	71	71	0.3800	0.3700	38	3.00	0.113411	0.107521	0.3313985	FALSE
wh1bj	wh1b	24296	0	79	79	0.1800	0.1300	18	3.50	0.025447	0.013273	0.0677602	FALSE
wh1bj	wh1b	24296	0	82	82	0.1600	0.1100	16	5.60	0.020106	0.009503	0.0829066	FALSE
wh1bj	wh1b	24296	0	78	78	0.1600	0.0600	16	6.50	0.020106	0.002827	0.0745342	FALSE
wh1bj	wh1b	24296	0	81	81	0.1300	0.0900	13	3.60	0.013223	0.0063362	0.0353429	FALSE
wh1bj	wh1b	24296	0	83	83	0.0800	0.1200	12	3.60	0.005027	0.011310	0.0294053	FALSE
wh1bj	wh1b	24296	0	84	84	0.1000	0.0700	10	2.20	0.007854	0.003848	0.0128727	FALSE
wh1bj	wh1b	24296	0	80	80	0.2700	0.2800	28	2.60	0.057255	0.061575	0.1544798	FALSE
wh1bj	wh1b	24296	0	75	75	0.2600	0.1500	26	6.10	0.053093	0.017671	0.2158312	FALSE
wh1bj	wh1b	24296	0	85	85	0.1600	0.2200	22	3.20	0.020106	0.038013	0.0929911	FALSE
wh1bj	wh1b	24296	0	86	86	0.2100	0.1500	21	3.40	0.034636	0.017671	0.0889227	FALSE
wh1bj	wh1b	24296	0	76	76	0.0800	0.2000	20	9.20	0.005027	0.031416	0.1676352	FALSE
wh1bj	wh1b	24296	0	77	77	0.2600	0.3500	35	5.10	0.053093	0.096211	0.3807254	FALSE
wh1bj	wh1b	24296	0	74	74	0.4500	0.3500	45	3.00	0.159043	0.096211	0.3828813	FALSE
wh1ca	wh1c	24296	0	14	14	0.1800	0.1900	19	2.60	0.025447	0.028353	0.0699396	FALSE
wh1ca	wh1c	24296	0	18	18	0.1200	0.0300	12	4.70	0.011310	0.000707	0.0282390	FALSE
wh1ca	wh1c	24296	0	11	11	0.1700	0.2000	20	3.30	0.022698	0.031416	0.0892879	TRUE
wh1ca	wh1c	24296	0	1	1	0.0500	0.2000	20	8.00	0.001963	0.031416	0.1335176	FALSE
wh1ca	wh1c	24296	0	12	12	0.3500	0.3100	35	3.30	0.096211	0.073477	0.2832850	TRUE
wh1ca	wh1c	24296	0	16	16	0.3300	0.2600	33	4.80	0.085530	0.053093	0.3326944	FALSE
wh1ca	wh1c	24296	0	17	17	0.3100	0.3100	31	3.30	0.075477	0.075477	0.2490731	FALSE
wh1ca	wh1c	24296	0	13	13	2.0000	1.2000	200	0.60	3.141590	1.130972	1.2817687	TRUE

wh1ca	wh1c	24296	0	15	0.3700	0.4000	40	5.80	0.107521	0.125664	0.6762351	FALSE	
wh1cb	wh1c	24296	0	b	27	0.1100	0.1700	40	6.30	0.080425	0.125664	0.6491782	FALSE
wh1cb	wh1c	24296	0	b	21	0.1500	0.1300	17	3.10	0.009503	0.022698	0.0499120	FALSE
wh1cb	wh1c	24296	0	b	28	0.0900	0.1500	15	5.00	0.017671	0.013273	0.0773617	FALSE
wh1cb	wh1c	24296	0	a	7	0.0800	0.1400	15	4.20	0.006362	0.017671	0.0504696	FALSE
wh1cb	wh1c	24296	0	b	24	0.1300	0.1300	14	5.90	0.005027	0.015394	0.0602400	FALSE
wh1cb	wh1c	24296	0	a	34	0.1700	0.2800	28	2.30	0.013273	0.013273	0.0305284	FALSE
wh1cb	wh1c	24296	0	a	5	0.1900	0.2700	27	6.90	0.022698	0.061575	0.2907424	FALSE
wh1cb	wh1c	24296	0	b	6	0.2600	0.2200	26	3.10	0.053093	0.038013	0.1412145	FALSE
wh1cb	wh1c	24296	0	a	9	0.2500	0.1100	25	11.70	0.049087	0.009503	0.3427553	FALSE
wh1cb	wh1c	24296	0	b	20	0.2000	0.2500	25	5.70	0.031416	0.049087	0.2294342	FALSE
wh1cb	wh1c	24296	0	b	23	0.2400	0.2400	24	4.00	0.045239	0.045239	0.1809556	FALSE
wh1cb	wh1c	24296	0	a	4	0.2300	0.2300	23	2.50	0.041548	0.041548	0.1038688	FALSE
wh1cb	wh1c	24296	0	b	26	0.2300	0.2300	23	5.10	0.041548	0.041548	0.2118924	FALSE
wh1cb	wh1c	24296	0	b	29	0.2000	0.2000	20	2.60	0.031416	0.031416	0.0816813	FALSE
wh1cb	wh1c	24296	0	b	25	0.1300	0.2000	20	3.50	0.01273	0.01273	0.0782060	FALSE
wh1cb	wh1c	24296	0	a	2	0.3800	0.3500	38	3.70	0.113411	0.096211	0.3878018	TRUE
wh1cb	wh1c	24296	0	a	8	0.0400	0.2200	34	12.60	0.090792	0.038013	0.8114727	FALSE
wh1cb	wh1c	24296	0	b	22	0.4200	0.5400	54	3.90	0.138544	0.229022	0.7167338	FALSE
wh1cb	wh1c	24296	0	a	10	0.2300	0.4700	47	14.90	0.041548	0.173494	1.6020617	TRUE
wh1cc	wh1c	24296	0	a	43	0.1700	0.1900	19	6.00	0.022698	0.028353	0.1531525	FALSE
wh1cc	wh1c	24296	0	a	33	0.1600	0.1800	18	5.10	0.020106	0.025447	0.1161603	FALSE
wh1cc	wh1c	24296	0	a	45	0.0900	0.1400	14	3.80	0.006362	0.015394	0.0413355	FALSE
wh1cc	wh1c	24296	0	a	46	0.0700	0.1200	12	3.90	0.003848	0.011310	0.0295584	FALSE
wh1cc	wh1c	24296	0	a	42	0.0900	0.1100	11	3.60	0.006362	0.009503	0.0285571	FALSE
wh1cc	wh1c	24296	0	a	38	0.2700	0.2200	27	4.30	0.057255	0.038013	0.2048277	FALSE
wh1cc	wh1c	24296	0	a	47	0.1300	0.2600	26	3.10	0.013273	0.053093	0.1028674	FALSE
wh1cc	wh1c	24296	0	a	41	0.2500	0.2400	25	2.60	0.04087	0.045239	0.1179078	FALSE
wh1cc	wh1c	24296	0	a	37	0.2400	0.2300	24	5.70	0.045239	0.041548	0.2473413	FALSE
wh1cc	wh1c	24296	0	a	40	0.2300	0.2300	23	2.90	0.041548	0.1204878	0.1204878	FALSE
wh1cc	wh1c	24296	0	a	39	0.2000	0.2300	23	2.60	0.031416	0.041548	0.0948525	FALSE
wh1cc	wh1c	24296	0	a	36	0.1500	0.2300	23	6.00	0.017871	0.041548	0.1776569	FALSE
wh1cc	wh1c	24296	0	b	31	0.1700	0.2100	21	3.90	0.022698	0.034636	0.1118013	FALSE
wh1cc	wh1c	24296	0	b	30	0.1200	0.2100	21	4.20	0.011310	0.034636	0.0964861	FALSE
wh1cc	wh1c	24296	0	a	48	0.2000	0.1700	20	2.90	0.031416	0.022698	0.0784651	FALSE
wh1cc	wh1c	24296	0	a	35	0.3500	0.2500	35	2.00	0.096211	0.049087	0.1452985	FALSE
wh1cc	wh1c	24296	0	a	44	0.3000	0.2000	300	1.00	0.708578	3.141590	5.1050838	TRUE
wh1cc	wh1c	24296	0	a	49	0.21000	0.8000	210	2.10	3.463603	0.562654	4.1645702	TRUE
wh1cc	wh1c	24296	0	a	53	0.1700	0.1400	17	6.40	0.145220	0.246301	1.2528661	FALSE
wh1cc	wh1c	24296	0	a	50	0.2100	0.2600	26	4.20	0.034636	0.053093	0.1842307	FALSE
wh1cc	wh1c	24296	0	a	51	0.2200	0.1800	22	2.40	0.038013	0.025447	0.0761521	FALSE
wh1cc	wh1c	24296	0	a	52	0.2400	0.3000	30	7.20	0.045239	0.070686	0.4173288	FALSE
wh1cc	wh1c	24296	0	a	53	0.1700	0.1400	17	6.00	0.022698	0.015394	0.1142753	FALSE
wh1cf	wh1c	24296	0	a	54	0.1400	0.1300	14	3.00	0.015394	0.03273	0.0430005	FALSE
wh1cg	wh1c	24296	0	a	72	0.0800	0.1400	14	5.70	0.005027	0.05394	0.0581980	FALSE
wh1cq	wh1c	24296	0	a	71	0.1200	0.1200	12	3.60	0.011310	0.011310	0.0407150	FALSE

wh1cg	wh1c	24296	0	74	74	0.1200	0.1200	12	5.00	0.011310	0.011310	0.0565486	FALSE	
wh1cg	wh1c	24296	0	70	70	0.1200	0.0900	12	3.60	0.011310	0.006362	0.0318086	FALSE	
wh1cg	wh1c	24296	0	69	69	0.1200	0.0400	12	5.00	0.011310	0.001257	0.0314159	FALSE	
wh1cg	wh1c	24296	0	75	75	0.2700	0.1600	27	7.60	0.057255	0.020106	0.2939743	FALSE	
wh1cg	wh1c	24296	0	58	58	0.2400	0.2600	26	3.50	0.045239	0.053093	0.1720806	FALSE	
wh1cg	wh1c	24296	0	56	56	0.1900	0.2000	20	4.20	0.028553	0.031416	0.1255144	FALSE	
wh1cg	wh1c	24296	0	55	55	0.2000	0.3500	35	9.40	0.031416	0.096211	0.5998473	TRUE	
wh1cg	wh1c	24296	0	73	73	0.2200	0.3200	32	7.00	0.038013	0.080425	0.4145328	TRUE	
wh1cg	wh1c	24296	0	57	57	2.2000	1.0000	220	3.30	3.80124	7.568398	7.568398	TRUE	
which	wh1c	24296	0	62	62	0.1700	0.1300	17	3.40	0.022688	0.013273	0.0611510	FALSE	
which	wh1c	24296	0	59	59	0.2200	0.2800	26	2.80	0.038013	0.053093	0.1275486	FALSE	
which	wh1c	24296	0	76	76	0.2400	0.1000	24	12.10	0.045239	0.007854	0.3212119	FALSE	
which	wh1c	24296	0	77	77	0.2300	0.3800	38	11.70	0.041548	0.113411	0.9065097	TRUE	
which	wh1c	24296	0	60	60	0.3200	0.3600	36	3.90	0.080425	0.101788	0.3553138	FALSE	
which	wh1c	24296	0	61	61	0.3400	0.2800	34	4.40	0.090792	0.061575	0.3352077	FALSE	
which	wh1c	24296	0	93	93	0.2500	0.3000	30	3.30	0.049087	0.010686	0.1976256	FALSE	
which	wh1c	24296	0	92	92	0.2200	0.3000	30	5.50	0.038013	0.070686	0.2989223	FALSE	
which	wh1c	24296	0	78	78	2.0000	0.6000	200	3.00	3.141590	0.282743	5.1364997	TRUE	
wh1ci	wh1c	24296	0	79	79	0.1900	0.1900	19	2.30	0.028353	0.022353	0.0652116	FALSE	
wh1ci	wh1c	24296	0	63	63	0.1700	0.0500	17	12.20	0.022698	0.001963	0.1504350	TRUE	
wh1ci	wh1c	24296	0	67	67	0.1600	0.1600	16	3.10	0.020106	0.020106	0.0623291	FALSE	
wh1ci	wh1c	24296	0	66	66	0.1300	0.1300	13	2.90	0.013273	0.013273	0.0384923	FALSE	
wh1ci	wh1c	24296	0	c	82	82	0.1200	0.1200	12	2.90	0.011310	0.011310	0.0327982	FALSE
wh1ci	wh1c	24296	0	c	85	85	0.1100	0.1100	11	2.50	0.009503	0.009503	0.0237583	FALSE
wh1ci	wh1c	24296	0	64	64	0.0100	0.1000	10	9.50	0.000797	0.007854	0.0336794	FALSE	
wh1ci	wh1c	24296	0	c	80	80	0.2600	0.2000	26	6.70	0.053093	0.031416	0.2831044	FALSE
wh1ci	wh1c	24296	0	c	68	68	0.2000	0.2000	20	2.10	0.031416	0.031416	0.0859734	FALSE
wh1ci	wh1c	24296	0	c	81	81	0.2200	0.3100	31	9.60	0.038013	0.075477	0.5447517	TRUE
wh1ci	wh1c	24296	0	c	91	91	0.1500	0.1700	17	3.40	0.017671	0.022698	0.0686280	FALSE
wh1ci	wh1c	24296	0	c	88	88	0.1100	0.1500	15	4.90	0.009503	0.0117671	0.06655781	FALSE
wh1ci	wh1c	24296	0	c	83	83	0.2700	0.0900	27	12.70	0.057255	0.066362	0.4033692	TRUE
wh1ci	wh1c	24296	0	c	87	87	0.2600	0.2600	26	2.20	0.053093	0.053093	0.1168043	FALSE
wh1ci	wh1c	24296	0	c	90	90	0.2200	0.1700	22	2.10	0.038013	0.022698	0.0637468	FALSE
wh1ci	wh1c	24296	0	c	84	84	0.3400	0.1700	34	10.90	0.090792	0.022698	0.6183202	TRUE
wh1ci	wh1c	24296	0	c	86	86	0.2600	0.3400	34	5.60	0.053093	0.090792	0.4023775	FALSE
wh1ci	wh1c	24296	0	c	89	89	0.0000	1.5000	300	3.60	7.068578	1.767144	15.9042954	TRUE
y01aa	y01a	57523	0	a	3	0.1600	0.1400	16	2.10	0.020106	0.015394	0.0372150	FALSE	
y01aa	y01a	57523	0	a	4	0.1300	0.1200	13	3.90	0.013273	0.011310	0.0479467	FALSE	
y01aa	y01a	57523	0	a	2	2	0.2200	0.2500	25	4.50	0.038013	0.049087	0.1159763	FALSE
y01aa	y01a	57523	0	a	5	0.1300	0.2500	25	2.80	0.013273	0.049087	0.0873048	FALSE	
y01aa	y01a	57523	0	a	6	0.1900	0.2200	22	2.20	0.02853	0.038013	0.0730027	FALSE	
y01aa	y01a	57523	0	a	7	0.3600	0.3500	35	2.50	0.096211	0.2405280	0.2405280	FALSE	
y01ab	y01a	57523	0	c	1	1	0.3500	1.0000	100	4.10	0.196349	0.785398	2.0125811	TRUE
y01ab	y01a	57523	0	c	8	8	0.1200	0.0600	12	7.30	0.011310	0.002827	0.0516006	FALSE
y01ab	y01a	57523	0	c	9	9	0.2200	0.2300	23	2.50	0.038013	0.057255	0.0994510	FALSE
y01ad	y01a	57523	0	c	10	10	0.1700	0.2700	27	4.50	0.022698	0.096211	0.1798953	FALSE
y01ad	y01a	57523	1	c	164	164	0.2300	0.2800	28	3.80	0.041548	0.061575	0.1959331	TRUE

yo1ad	yo1a	57523	1	165	165	0.1100	0.2400	24	2.20	0.009503	0.045239	0.0602164	FALSE
yo1ae	yo1a	57523	0	17	17	0.1700	0.0700	17	5.10	0.022698	0.003848	0.0676934	FALSE
yo1ae	yo1a	57523	0	21	21	0.1600	0.1600	16	3.20	0.020106	0.020106	0.0643398	FALSE
yo1ae	yo1a	57523	0	19	19	0.1600	0.1200	16	2.80	0.020106	0.011310	0.0439823	FALSE
yo1ae	yo1a	57523	0	15	15	0.1200	0.1500	15	2.40	0.011310	0.017671	0.0347774	FALSE
yo1ae	yo1a	57523	0	14	14	0.2900	0.1800	29	2.60	0.066032	0.025447	0.1189485	FALSE
yo1ae	yo1a	57523	0	16	16	0.1700	0.2300	23	2.20	0.022698	0.041548	0.0706701	FALSE
yo1ae	yo1a	57523	0	22	22	0.2100	0.0800	21	2.60	0.034636	0.005027	0.0515613	FALSE
yo1ae	yo1a	57523	0	11	11	0.2000	0.1700	20	3.30	0.031416	0.022698	0.0892879	FALSE
yo1ae	yo1a	57523	0	12	12	0.0600	0.2000	20	11.00	0.002827	0.031416	0.1883383	FALSE
yo1ae	yo1a	57523	0	18	18	0.3400	0.3000	34	5.00	0.090792	0.070686	0.4036943	FALSE
yo1ae	yo1a	57523	0	13	13	0.1300	0.3200	32	3.70	0.013273	0.080425	0.1733412	FALSE
yo1ae	yo1a	57523	0	20	20	0.3000	0.2700	30	2.10	0.070686	0.057255	0.1343383	FALSE
yo1ae	yo1a	57523	1	170	170	0.1600	0.1000	16	3.00	0.020106	0.007854	0.0419402	FALSE
yo1ae	yo1a	57523	1	169	169	0.1500	0.1200	15	2.20	0.017671	0.011310	0.0318793	FALSE
yo1ae	yo1a	57523	1	166	166	0.1200	0.1200	12	2.50	0.011310	0.0282743	0.0282743	FALSE
yo1ae	yo1a	57523	1	167	167	0.2600	0.1100	26	3.40	0.053093	0.009503	0.1064135	FALSE
yo1ae	yo1a	57523	1	171	171	0.1200	0.2400	24	2.00	0.011310	0.045239	0.0565486	FALSE
yo1ae	yo1a	57523	1	172	172	0.1400	0.2400	24	2.00	0.015394	0.045239	0.0697276	FALSE
yo1ae	yo1a	57523	1	168	168	2.4300	0.2400	243	2.00	4.637694	0.043239	4.6829326	FALSE
yo1af	yo1a	57523	0	b	38	0.1700	0.1900	19	2.00	0.022698	0.028353	0.0510508	FALSE
yo1af	yo1a	57523	0	b	41	0.1700	0.1900	19	4.60	0.022698	0.028353	0.1174169	FALSE
yo1af	yo1a	57523	0	b	28	0.1800	0.1600	18	3.10	0.025447	0.020106	0.0706072	FALSE
yo1af	yo1a	57523	0	b	37	0.1800	0.1500	18	2.10	0.025447	0.017671	0.0452742	FALSE
yo1af	yo1a	57523	0	b	36	0.1300	0.1600	16	3.80	0.013273	0.020106	0.0634208	FALSE
yo1af	yo1a	57523	0	b	42	0.1000	0.1300	13	3.60	0.007854	0.013273	0.0380289	FALSE
yo1af	yo1a	57523	0	b	39	0.1000	0.1200	12	4.40	0.007854	0.011310	0.0421601	FALSE
yo1af	yo1a	57523	0	b	34	0.1700	0.2400	24	3.30	0.022698	0.045239	0.1120959	TRUE
yo1af	yo1a	57523	0	b	32	0.2300	0.1400	23	3.60	0.041548	0.015394	0.1024944	FALSE
yo1af	yo1a	57523	0	b	31	0.2200	0.2300	23	8.40	0.038013	0.041548	0.3341552	FALSE
yo1af	yo1a	57523	0	b	30	0.2200	0.1800	22	8.40	0.038013	0.025447	0.2665325	FALSE
yo1af	yo1a	57523	0	b	24	0.1000	0.2200	22	3.40	0.007854	0.038013	0.077943	FALSE
yo1af	yo1a	57523	0	b	40	0.3700	0.2400	37	7.50	0.07521	0.045239	0.5728493	FALSE
yo1af	yo1a	57523	0	b	25	0.3200	0.3600	36	4.30	0.080425	0.101788	0.3917563	FALSE
yo1af	yo1a	57523	0	b	29	0.3100	0.2200	31	4.00	0.075477	0.038013	0.2269799	FALSE
yo1af	yo1a	57523	0	b	27	0.1900	0.3100	31	8.00	0.028353	0.075477	0.4153182	FALSE
yo1af	yo1a	57523	0	b	33	0.1300	0.3000	30	4.80	0.013273	0.070686	0.2015016	TRUE
yo1af	yo1a	57523	0	b	43	1.0000	2.2000	220	3.70	0.785398	3.801324	8.4854346	TRUE
yo1af	yo1a	57523	0	b	26	0.3300	0.5500	55	6.80	0.085530	0.237583	1.0855826	FALSE
yo1af	yo1a	57523	0	b	35	0.4100	0.4800	48	3.30	0.132025	0.180956	0.5164185	TRUE
yo1af	yo1a	57523	0	b	23	0.4100	0.1600	41	11.80	0.132025	0.020106	0.8975758	FALSE
yo1af	yo1a	57523	1	b	174	0.1900	0.1000	19	3.90	0.028353	0.007854	0.076033	FALSE
yo1af	yo1a	57523	1	b	176	0.1700	0.1100	17	2.30	0.02698	0.009503	0.0370315	TRUE
yo1af	yo1a	57523	1	b	175	0.1600	0.1400	16	3.30	0.020106	0.015394	0.0565749	FALSE
yo1af	yo1a	57523	1	b	173	0.1500	0.1000	15	3.90	0.017671	0.007854	0.0497746	FALSE
yo1ag	yo1a	57523	0	b	77	0.0600	0.1900	19	8.90	0.002827	0.028353	0.138522	TRUE
yo1ag	yo1a	57523	0	b	75	0.1900	0.1900	19	6.30	0.028353	0.028353	0.1785230	FALSE

yo1ag	yo1a	57523	0	b	44	44	0.0900	0.1800	18	6.30	0.006362	0.025447	0.1001971	FALSE
yo1ag	yo1a	57523	0	b	55	55	0.1600	0.1200	16	2.20	0.020106	0.011310	0.0345575	TRUE
yo1ag	yo1a	57523	0	b	50	50	0.1600	0.0500	16	4.90	0.020106	0.001963	0.0540707	FALSE
yo1ag	yo1a	57523	0	b	59	59	0.1000	0.1600	16	4.50	0.007854	0.020106	0.0629103	FALSE
yo1ag	yo1a	57523	0	b	67	67	0.1400	0.1400	14	4.10	0.015394	0.015394	0.0631145	FALSE
yo1ag	yo1a	57523	0	b	80	80	0.1300	0.1100	13	3.10	0.013273	0.005503	0.0353036	FALSE
yo1ag	yo1a	57523	0	b	51	51	0.1200	0.0600	12	5.80	0.011310	0.002827	0.0409977	FALSE
yo1ag	yo1a	57523	0	b	68	68	0.1100	0.0500	11	4.60	0.009503	0.001963	0.0263736	FALSE
yo1ag	yo1a	57523	0	b	49	49	0.1000	0.1000	10	5.40	0.007854	0.007854	0.0424115	FALSE
yo1ag	yo1a	57523	0	b	57	57	0.2700	0.2300	27	9.00	0.057255	0.041548	0.4446135	FALSE
yo1ag	yo1a	57523	0	b	48	48	0.2500	0.1800	26	6.40	0.049087	0.025447	0.2335095	FALSE
yo1ag	yo1a	57523	0	b	58	58	0.2100	0.2500	25	2.30	0.034636	0.049087	0.0962819	FALSE
yo1ag	yo1a	57523	0	b	65	65	0.1900	0.2500	25	5.50	0.028353	0.049087	0.2129605	FALSE
yo1ag	yo1a	57523	0	b	52	52	0.1900	0.2400	24	2.90	0.028353	0.045239	0.1067080	FALSE
yo1ag	yo1a	57523	0	b	66	66	0.0700	0.2300	23	12.00	0.003848	0.041548	0.2722759	FALSE
yo1ag	yo1a	57523	0	b	53	53	0.2000	0.2200	22	2.80	0.031416	0.038013	0.092008	FALSE
yo1ag	yo1a	57523	0	b	47	47	0.1500	0.2200	22	3.59	0.017671	0.038013	0.0998540	FALSE
yo1ag	yo1a	57523	0	b	74	74	0.2100	0.1800	21	2.60	0.034636	0.025447	0.0781078	FALSE
yo1ag	yo1a	57523	0	b	45	45	0.2000	0.1900	20	4.20	0.031416	0.028353	0.1255144	FALSE
yo1ag	yo1a	57523	0	b	54	54	0.1700	0.2000	20	2.00	0.022698	0.031416	0.0541139	FALSE
yo1ag	yo1a	57523	0	b	76	76	0.2900	0.3800	38	5.70	0.066052	0.113411	0.5114705	FALSE
yo1ag	yo1a	57523	0	b	63	63	0.3400	0.3400	34	3.40	0.090792	0.090792	0.3086926	FALSE
yo1ag	yo1a	57523	0	b	62	62	0.3300	0.2000	33	7.10	0.085530	0.031416	0.4151572	FALSE
yo1ag	yo1a	57523	0	b	60	60	0.3200	0.1600	32	5.80	0.080425	0.020106	0.2915396	TRUE
yo1ag	yo1a	57523	0	b	46	46	0.3000	0.3000	30	3.64	0.070686	0.070686	0.2572962	FALSE
yo1ag	yo1a	57523	0	b	56	56	0.1600	0.3000	30	9.90	0.020106	0.070686	0.4494202	FALSE
yo1ag	yo1a	57523	0	b	79	79	0.2500	0.7000	225	2.25	0.3976075	0.384845	4.9060346	TRUE
yo1ag	yo1a	57523	0	b	64	64	0.4800	0.2200	48	5.50	0.180956	0.038013	0.6021643	FALSE
yo1ag	yo1a	57523	0	b	61	61	0.4000	0.3000	40	7.20	0.126664	0.070686	0.7068578	FALSE
yo1ag	yo1a	57523	1	183	183	0.1800	0.1600	18	1.80	0.022447	0.020106	0.0409977	FALSE	
yo1ag	yo1a	57523	1	182	182	0.1600	0.0600	16	2.30	0.020106	0.0263736	0.0263736	FALSE	
yo1ag	yo1a	57523	1	180	180	0.1200	0.2100	21	3.90	0.011310	0.034636	0.0895942	TRUE	
yo1ag	yo1a	57523	1	178	178	0.1700	0.2000	20	3.50	0.022998	0.031416	0.0946993	FALSE	
yo1ag	yo1a	57523	1	181	181	0.1900	0.2000	20	2.80	0.028353	0.031416	0.0836762	FALSE	
yo1ag	yo1a	57523	1	179	179	0.3200	0.3700	37	6.40	0.084245	0.107521	0.6014260	FALSE	
yo1ag	yo1a	57523	1	177	177	0.3600	0.2100	36	8.00	0.107788	0.034636	0.5456942	FALSE	
yo1ah	yo1ah	57523	0	b	87	87	0.1900	0.1900	19	2.00	0.028353	0.028353	0.0567057	TRUE
yo1ah	yo1ah	57523	0	b	85	85	0.1700	0.1700	17	2.90	0.022698	0.022698	0.0658242	FALSE
yo1ah	yo1ah	57523	0	b	90	90	0.1900	0.1500	19	4.20	0.028353	0.017671	0.0966510	FALSE
yo1ah	yo1ah	57523	0	b	97	97	0.1800	0.1800	18	2.00	0.025447	0.025447	0.0508938	FALSE
yo1ah	yo1ah	57523	0	b	96	96	0.1800	0.1600	18	5.90	0.025447	0.020106	0.1343815	FALSE
yo1ah	yo1ah	57523	0	b	93	93	0.1800	0.0800	18	3.90	0.025447	0.005027	0.0594232	FALSE
yo1ah	yo1ah	57523	0	b	85	85	0.1700	0.1700	17	2.90	0.022698	0.022698	0.0658242	FALSE
yo1ah	yo1ah	57523	0	b	69	69	0.1600	0.0900	16	9.74	0.020106	0.006362	0.1288987	FALSE
yo1ah	yo1ah	57523	0	b	82	82	0.1300	0.1000	13	3.70	0.013273	0.007854	0.0390853	FALSE
yo1ah	yo1ah	57523	0	b	94	94	0.1200	0.1300	13	4.00	0.006362	0.013273	0.0392699	FALSE
yo1ah	yo1ah	57523	0	b	94	94	0.1200	0.0600	12	2.60	0.011310	0.011310	0.0294053	FALSE
yo1ah	yo1ah	57523	0	b	70	70	0.1200	0.1200	12	9.96	0.011310	0.002827	0.0704030	FALSE

yolah	y01a	57523	0	b	81	81	0.1000	0.1200	12	6.70	0.007854	0.011310	0.0641984	FALSE
yolah	y01a	57523	0	b	91	91	0.1100	0.0200	11	4.90	0.009503	0.000314	0.0240528	FALSE
yolah	y01a	57523	0	b	100	100	0.2700	0.2900	29	12.80	0.057255	0.066152	0.7891674	FALSE
yolah	y01a	57523	0	b	83	83	0.2700	0.2700	27	3.90	0.057255	0.057255	0.2232964	FALSE
yolah	y01a	57523	0	b	95	95	0.2500	0.1000	25	4.60	0.049087	0.007854	0.1309650	FALSE
yolah	y01a	57523	0	b	89	89	0.2200	0.2100	22	2.50	0.038013	0.034636	0.0908116	FALSE
yolah	y01a	57523	0	b	71	71	0.2100	0.0300	21	15.73	0.034636	0.000707	0.2779718	FALSE
yolah	y01a	57523	0	b	98	98	0.2000	0.1600	20	3.60	0.031416	0.020106	0.0947397	FALSE
yolah	y01a	57523	0	b	72	72	0.3600	0.3600	36	6.93	0.101788	0.101788	0.7053875	FALSE
yolah	y01a	57523	0	b	92	92	0.2700	0.3200	32	3.60	0.057255	0.080425	0.2478243	FALSE
yolah	y01a	57523	0	b	88	88	0.5000	1.5000	150	1.50	0.196349	1.767144	1.4726203	TRUE
yolah	y01a	57523	0	b	78	78	0.6800	0.3600	58	8.20	0.264208	0.101788	1.5005805	TRUE
yolah	y01a	57523	0	b	102	102	0.2500	0.5400	54	14.00	0.049087	0.229022	1.9467648	TRUE
yolah	y01a	57523	0	b	73	73	0.4700	0.2700	47	9.50	0.173494	0.057255	1.0960615	FALSE
yolah	y01a	57523	0	b	84	84	0.3200	0.4600	46	2.90	0.080425	0.166190	0.3577915	FALSE
yolah	y01a	57523	0	b	86	86	0.4000	0.4000	40	3.30	0.125664	0.125664	0.4146899	FALSE
yolah	y01a	57523	0	b	112	112	0.1900	0.1900	19	3.00	0.028353	0.028353	0.0850585	FALSE
yolah	y01a	57523	0	b	106	106	0.1700	0.1700	17	2.30	0.022698	0.022698	0.052254	FALSE
yolah	y01a	57523	0	b	136	136	0.1600	0.0500	16	14.80	0.020106	0.01963	0.1633156	TRUE
yolah	y01a	57523	0	b	104	104	0.1600	0.1600	16	3.80	0.020106	0.020106	0.0764035	FALSE
yolah	y01a	57523	0	b	117	117	0.1500	0.1400	15	3.70	0.017671	0.015394	0.0611707	FALSE
yolah	y01a	57523	0	b	122	122	0.1500	0.0800	15	10.00	0.017671	0.005027	0.1134889	FALSE
yolah	y01a	57523	0	b	108	108	0.1500	0.0600	15	8.60	0.017671	0.002827	0.0881452	FALSE
yolah	y01a	57523	0	b	109	109	0.1400	0.0600	14	10.30	0.015394	0.002827	0.0938893	FALSE
yolah	y01a	57523	0	b	128	128	0.1200	0.1200	12	2.80	0.011310	0.011310	0.0316672	FALSE
yolah	y01a	57523	0	b	111	111	0.1200	0.0800	12	7.10	0.011310	0.005027	0.0579938	FALSE
yolah	y01a	57523	0	b	127	127	0.1000	0.1000	10	2.80	0.007854	0.007854	0.0219911	FALSE
yolah	y01a	57523	0	b	105	105	0.2900	0.2400	29	6.50	0.066052	0.045239	0.3616952	FALSE
yolah	y01a	57523	0	b	119	119	0.2500	0.2800	28	3.40	0.049087	0.061575	0.1881263	FALSE
yolah	y01a	57523	0	b	118	118	0.2700	0.2700	27	3.40	0.057255	0.057255	0.19466686	FALSE
yolah	y01a	57523	0	b	110	110	0.2600	0.1600	26	6.60	0.053093	0.020106	0.2415569	FALSE
yolah	y01a	57523	0	b	126	126	0.2300	0.2300	23	2.40	0.041548	0.041548	0.0997141	FALSE
yolah	y01a	57523	0	b	103	103	0.2100	0.1500	21	2.00	0.034636	0.017671	0.0523075	FALSE
yolah	y01a	57523	0	b	114	114	0.2000	0.0700	20	12.10	0.031416	0.03848	0.2133493	TRUE
yolah	y01a	57523	0	b	107	107	0.2500	0.3800	38	3.30	0.049087	0.113411	0.2681229	TRUE
yolah	y01a	57523	0	b	101	101	0.3600	0.2300	36	4.30	0.101788	0.041548	0.3081703	TRUE
yolah	y01a	57523	0	b	115	115	0.3500	0.3300	35	5.70	0.096211	0.085530	0.5179618	FALSE
yolah	y01a	57523	0	b	113	113	0.3500	0.1700	35	8.20	0.096211	0.022698	0.4875276	FALSE
yolah	y01a	57523	0	b	116	116	0.3100	0.2300	31	5.80	0.075477	0.041548	0.3393703	FALSE
yolah	y01a	57523	0	b	135	135	0.3000	0.1600	30	14.30	0.070686	0.020106	0.6491624	TRUE
yolah	y01a	57523	0	b	125	125	0.3000	0.3000	30	2.90	0.070686	0.070686	0.2049887	FALSE
yolah	y01a	57523	0	b	123	123	1.0000	2.6000	260	3.60	0.785398	5.309287	10.9704323	TRUE
yolah	y01a	57523	0	b	121	121	0.5000	1.2000	120	2.20	0.196349	1.230972	1.4600540	TRUE
yolah	y01a	57523	0	b	120	120	0.2200	0.4800	48	3.40	0.038013	0.180956	0.3722470	TRUE
yolah	y01a	57523	0	b	124	124	0.4500	0.4500	45	2.70	0.159043	0.159043	0.4294161	FALSE
yolah	y01a	57523	0	c	154	154	0.1900	0.1300	19	2.70	0.028353	0.013273	0.0561952	TRUE
yolah	y01a	57523	0	c	143	143	0.1900	0.1900	19	3.90	0.028353	0.028353	0.1105761	FALSE

yo1aj	yo1a	57523	0	c	134	134	0.1800	0.1800	18	5.70	0.025447	0.025447	0.1450472	FALSE
yo1aj	yo1a	57523	0	c	140	140	0.1700	0.1400	17	6.00	0.022698	0.015394	0.1142753	FALSE
yo1aj	yo1a	57523	0	c	159	159	0.1000	0.1700	17	4.00	0.007854	0.022698	0.0611039	FALSE
yo1aj	yo1a	57523	0	c	136	136	0.1600	0.0500	16	14.80	0.020106	0.001963	0.1633156	TRUE
yo1aj	yo1a	57523	0	c	144	144	0.1600	0.1600	16	4.00	0.020106	0.020106	0.0804247	FALSE
yo1aj	yo1a	57523	0	c	147	147	0.1500	0.1500	15	2.00	0.017671	0.017671	0.0534429	FALSE
yo1aj	yo1a	57523	0	c	133	133	0.1400	0.1400	14	3.70	0.015394	0.015394	0.0569570	FALSE
yo1aj	yo1a	57523	0	c	137	137	0.1200	0.1200	12	7.40	0.011310	0.011310	0.0836920	FALSE
yo1aj	yo1a	57523	0	c	161	161	0.1000	0.1100	11	5.10	0.009503	0.009503	0.0442611	FALSE
yo1aj	yo1a	57523	0	c	153	153	0.1000	0.0900	10	3.90	0.007854	0.007854	0.0277206	FALSE
yo1aj	yo1a	57523	0	c	62	62	0.0500	0.0500	10	5.10	0.001963	0.001963	0.0250345	FALSE
yo1aj	yo1a	57523	0	c	141	141	0.1900	0.2900	29	7.40	0.028333	0.066052	0.3492977	FALSE
yo1aj	yo1a	57523	0	c	142	142	0.2800	0.2800	28	3.90	0.061575	0.061575	0.2401431	FALSE
yo1aj	yo1a	57523	0	c	145	145	0.2200	0.2500	25	2.80	0.038013	0.049087	0.1219408	FALSE
yo1aj	yo1a	57523	0	c	146	146	0.2400	0.2400	24	12.80	0.045239	0.045239	0.5790579	FALSE
yo1aj	yo1a	57523	0	c	157	157	0.2000	0.2300	23	3.70	0.031416	0.041548	0.1349823	FALSE
yo1aj	yo1a	57523	0	c	138	138	0.2200	0.2200	22	7.10	0.038013	0.038013	0.2698940	FALSE
yo1aj	yo1a	57523	0	c	160	160	0.2100	0.1300	21	3.60	0.034686	0.013273	0.0862366	TRUE
yo1aj	yo1a	57523	0	c	131	131	0.2100	0.2100	21	4.70	0.034686	0.034686	0.16277893	FALSE
yo1aj	yo1a	57523	0	c	163	163	0.2100	0.0800	21	3.80	0.034686	0.003027	0.0753589	FALSE
yo1aj	yo1a	57523	0	c	156	156	0.3900	0.3900	39	4.30	0.119459	0.119459	0.5136735	FALSE
yo1aj	yo1a	57523	0	c	149	149	0.3400	0.3400	34	6.70	0.090792	0.090792	0.6083061	FALSE
yo1aj	yo1a	57523	0	c	130	130	0.3400	0.2800	34	2.60	0.090792	0.061575	0.1980772	FALSE
yo1aj	yo1a	57523	0	c	132	132	0.3400	0.2800	34	3.80	0.090792	0.061575	0.2894975	FALSE
yo1aj	yo1a	57523	0	c	148	148	0.2900	0.3300	33	4.00	0.066052	0.0855620	0.331634	FALSE
yo1aj	yo1a	57523	0	c	129	129	0.3200	0.3200	32	3.30	0.080425	0.080425	0.2654015	FALSE
yo1aj	yo1a	57523	0	c	152	152	0.3200	0.3200	32	2.30	0.080425	0.080425	0.1849768	FALSE
yo1aj	yo1a	57523	0	c	155	155	0.4600	0.3100	46	4.10	0.166190	0.075477	0.4954170	FALSE
yo1aj	yo1a	57523	0	c	150	150	0.4300	0.4600	46	3.20	0.145220	0.166190	0.4982562	FALSE
yo1aj	yo1a	57523	0	c	151	151	0.3000	0.4600	46	3.20	0.070886	0.166190	0.3790014	FALSE
yo1aj	yo1a	57523	0	c	139	139	0.4300	0.4300	43	7.10	0.145220	0.145220	1.0310620	FALSE
yo1aj	yo1a	57523	0	c	158	158	0.4000	0.4000	40	3.00	0.125664	0.125664	0.3769908	FALSE
yo1aj	yo1a	57523	0	c	1	1	0.1000	0.1700	17	5.60	0.007854	0.022698	0.0855455	FALSE
yo1bb	yo1b	57523	0	c	5	5	0.2100	0.1100	21	2.20	0.034636	0.009503	0.0485533	FALSE
yo1bb	yo1b	57523	0	c	2	2	0.2000	0.1600	20	3.70	0.031416	0.020106	0.0953158	FALSE
yo1bb	yo1b	57523	0	a	11	11	0.1800	0.1800	18	5.60	0.025447	0.025447	0.1425025	FALSE
yo1bb	yo1b	57523	0	b	14	14	0.1600	0.1200	16	3.70	0.020106	0.011310	0.0581194	FALSE
yo1bb	yo1b	57523	0	a	13	13	0.1500	0.1500	15	2.00	0.017671	0.017671	0.0353429	FALSE
yo1bb	yo1b	57523	0	b	16	16	0.1000	0.1000	10	2.80	0.007854	0.03848	0.163834	FALSE
yo1bc	yo1bc	57523	0	a	10	10	0.2700	0.2300	27	4.70	0.057255	0.041548	0.2321871	FALSE
yo1bc	yo1bc	57523	0	a	12	12	0.2000	0.1100	20	2.50	0.031416	0.09503	0.0511490	FALSE
yo1bc	yo1bc	57523	0	b	15	15	0.3000	0.2900	30	3.70	0.070886	0.066052	0.2529648	FALSE
yo1bc	yo1bc	57523	0	a	8	8	1.2000	1.0000	120	2.70	1.130972	0.785398	2.5870994	TRUE

yo1bc	57523	0	b	17	17	0.4000	0.4300	43	2.60	0.125664	0.145220	0.3521487	FALSE
yo1b	57523	0	a	9	9	0.4000	0.3200	40	2.00	0.125664	0.080425	0.2060883	TRUE
yo1bd	57523	0	b	23	23	0.1800	0.1800	18	3.10	0.025447	0.025447	0.0788853	FALSE
yo1bd	57523	0	b	24	24	0.1400	0.1400	14	2.60	0.015394	0.015394	0.0400339	FALSE
yo1bd	57523	0	b	20	20	0.0600	0.1100	11	5.20	0.002827	0.009503	0.0320599	FALSE
yo1bd	57523	0	b	19	19	0.0600	0.1000	10	4.00	0.002827	0.007854	0.0213928	FALSE
yo1bd	57523	0	b	18	18	0.1700	0.2600	26	2.50	0.022698	0.053093	0.0947386	FALSE
yo1bd	57523	0	b	25	25	0.2500	0.1900	25	4.50	0.049087	0.028353	0.1742404	TRUE
yo1bd	57523	0	b	27	27	0.2000	0.1200	20	4.50	0.031416	0.011310	0.0961327	TRUE
yo1bd	57523	0	b	21	21	0.3900	0.3600	39	6.10	0.119459	0.1011788	0.6748018	FALSE
yo1bd	57523	0	b	22	22	0.2900	0.3900	39	4.70	0.066052	0.119459	0.4359506	FALSE
yo1bd	57523	0	b	28	28	0.1600	1.2000	120	1.00	0.020106	1.130972	0.5755393	TRUE
yo1bd	57523	0	b	26	26	0.2300	0.4200	42	4.50	0.041548	0.138544	0.4052062	FALSE
yo1be	57523	0	c	37	37	0.1400	0.1400	14	2.40	0.015394	0.015394	0.0369451	FALSE
yo1be	57523	0	c	29	29	0.0900	0.1300	13	2.50	0.009362	0.013273	0.0245437	FALSE
yo1be	57523	0	c	31	31	0.0900	0.1300	13	4.50	0.006362	0.013273	0.0441786	FALSE
yo1be	57523	0	c	30	30	0.0700	0.1100	11	4.60	0.003848	0.009503	0.0307090	FALSE
yo1be	57523	0	c	33	33	0.1000	0.0900	10	3.00	0.001854	0.006362	0.0213235	FALSE
yo1be	57523	0	c	32	32	0.2300	0.1800	23	3.00	0.041548	0.025447	0.1004916	FALSE
yo1be	57523	0	c	34	34	0.2700	0.3400	34	2.30	0.057255	0.090792	0.1702545	FALSE
yo1be	57523	0	c	35	35	0.2100	0.3100	31	2.20	0.034636	0.057477	0.1211240	FALSE
yo1be	57523	0	c	36	36	1.0000	1.0000	100	6.60	0.785398	0.785398	0.4712385	TRUE
yo1bf	57523	0	c	38	38	0.8100	0.8100	81	2.30	0.515299	0.515299	1.1851884	FALSE
yo1bg	57523	0	d	41	41	0.1400	0.0900	14	2.00	0.015394	0.006362	0.0217555	FALSE
yo1bg	57523	0	d	40	40	0.1000	0.1300	13	2.00	0.007854	0.013273	0.0211272	FALSE
yo1bg	57523	0	d	45	45	0.0700	0.1000	10	4.60	0.003848	0.007854	0.0269156	FALSE
yo1bg	57523	0	d	39	39	0.2900	0.2300	29	2.00	0.060502	0.041548	0.1075995	TRUE
yo1bg	57523	0	d	44	44	0.2100	0.1000	21	7.40	0.034636	0.007854	0.1572130	FALSE
yo1bg	57523	0	d	42	42	0.7800	0.7600	78	1.40	0.477836	0.453646	0.6520370	TRUE
yo1bg	57523	0	d	43	43	0.5500	0.4700	55	3.30	0.237583	0.173494	0.6782771	FALSE
yo1bh	57523	0	d	50	50	0.1600	0.1900	19	3.40	0.020106	0.028353	0.0823803	FALSE
yo1bh	57523	0	d	47	47	0.0400	0.1600	16	9.20	0.001257	0.020106	0.0982689	FALSE
yo1bh	57523	0	d	52	52	0.0800	0.1500	15	3.70	0.005027	0.017671	0.0419913	TRUE
yo1bh	57523	0	d	83	83	0.0900	0.1500	15	4.20	0.006362	0.017671	0.0504696	FALSE
yo1bh	57523	0	d	84	84	0.1400	0.1000	14	2.70	0.015394	0.007854	0.0313845	FALSE
yo1bh	57523	0	d	51	51	0.1100	0.1400	14	4.60	0.009503	0.015394	0.0572633	FALSE
yo1bh	57523	0	d	46	46	0.1200	0.1100	12	2.00	0.011310	0.009503	0.0208130	FALSE
yo1bh	57523	0	d	53	53	0.1000	0.0800	10	2.80	0.007854	0.005027	0.0180327	FALSE
yo1bh	57523	0	d	48	48	0.0600	0.1000	10	4.70	0.002827	0.007854	0.0251013	FALSE
yo1bh	57523	0	d	81	81	0.2600	0.2700	27	2.20	0.053093	0.057255	0.1213832	FALSE
yo1bh	57523	0	d	49	49	0.2600	0.2600	26	2.30	0.053093	0.053093	0.1221136	FALSE
yo1bh	57523	0	d	80	80	0.2500	0.1800	25	2.60	0.049087	0.025447	0.0968945	FALSE
yo1bh	57523	0	d	55	55	0.2300	0.2300	23	3.20	0.041548	0.041548	0.1329521	FALSE
yo1bh	57523	0	d	82	82	0.2100	0.1700	21	2.50	0.034636	0.022698	0.0716675	FALSE
yo1bh	57523	0	d	79	79	0.2100	0.1600	21	2.50	0.034636	0.020106	0.0684278	FALSE
yo1bh	57523	0	d	57	57	0.3300	0.3300	33	4.40	0.085530	0.085530	0.3763311	FALSE
yo1bh	57523	0	d	56	56	1.7000	1.0000	170	1.30	2.269799	0.783398	1.9858776	TRUE

yo1bh	57523	0	78	78	0.4300	0.3400	43	670	0.145220	0.090792	0.7906400	FALSE
yo1bh	57523	0	d	54	0.1800	0.4200	42	300	0.025447	0.138544	0.2453865	FALSE
yo1bh	57523	0	e	75	0.1800	0.1600	18	330	0.025447	0.020106	0.0751625	FALSE
yo1bh	57523	0	e	60	0.1100	0.1500	15	280	0.009503	0.017671	0.0380447	TRUE
yo1bh	57523	0	e	70	0.0600	0.1200	12	770	0.008287	0.011310	0.0544280	FALSE
yo1bh	57523	0	e	59	0.1100	0.1100	11	280	0.009503	0.0266093	0.0266093	FALSE
yo1bh	57523	0	d	58	0.2200	0.2600	26	790	0.038013	0.053093	0.3595691	FALSE
yo1bh	57523	0	e	71	0.2200	0.1500	22	390	0.038013	0.017671	0.1085851	TRUE
yo1bh	57523	0	e	74	0.2000	0.1900	20	350	0.031416	0.028353	0.1045553	FALSE
yo1bj	57523	0	e	76	0.1200	0.1600	16	290	0.011310	0.020106	0.0455531	TRUE
yo1bj	57523	0	e	85	0.0900	0.1600	16	450	0.006362	0.020106	0.0595528	FALSE
yo1bj	57523	0	e	73	0.1300	0.0800	13	450	0.013273	0.005027	0.0411745	FALSE
yo1bj	57523	0	e	86	0.2300	0.2600	26	200	0.041548	0.053093	0.0946404	FALSE
yo1bj	57523	0	e	72	0.3100	0.2100	31	480	0.075477	0.034636	0.2642716	TRUE
yo1bj	57523	0	e	77	0.8000	1.0000	100	190	0.502654	0.785398	1.2236493	TRUE
yo1ca	57523	0	e	3	0.1900	0.1500	19	320	0.028353	0.017671	0.0736389	FALSE
yo1ca	57523	0	e	4	0.1100	0.1600	16	450	0.009503	0.020106	0.0666213	FALSE
yo1ca	57523	0	e	6	0.1800	0.2200	22	610	0.025447	0.038013	0.1935534	FALSE
yo1ca	57523	0	e	5	0.1200	0.2100	21	330	0.011310	0.034636	0.0751605	FALSE
yo1ca	57523	0	e	2	0.2500	0.3600	36	430	0.049087	0.101788	0.3243809	FALSE
yo1ca	57523	0	e	1	0.2600	0.4100	41	370	0.053093	0.132025	0.3424687	FALSE
yo1cb	57523	0	e	7	0.2000	0.6100	61	1520	0.031416	0.292246	2.4598336	TRUE
yo1cc	57523	0	e	8	1.0000	0.8000	100	320	0.783398	0.502654	2.0608830	TRUE
yo1cd	57523	0	e	14	0.0800	0.1500	15	410	0.005027	0.017671	0.0465309	FALSE
yo1cd	57523	0	e	13	0.0700	0.1100	11	740	0.003648	0.009503	0.0494015	FALSE
yo1cd	57523	0	e	15	0.2900	0.2700	29	200	0.066552	0.057255	0.1233074	FALSE
yo1cd	57523	0	e	10	0.2300	0.2700	27	340	0.041548	0.057255	0.1679651	FALSE
yo1cd	57523	0	e	12	0.2200	0.2200	22	200	0.038013	0.038013	0.0760265	FALSE
yo1cd	57523	0	e	9	0.3400	0.2200	34	420	0.090792	0.038013	0.2704909	FALSE
yo1cd	57523	0	e	11	0.3000	0.4400	44	610	0.070686	0.152053	0.6793531	FALSE
yo1ce	57523	0	e	20	0.1900	0.1500	19	320	0.028353	0.017671	0.0736389	FALSE
yo1ce	57523	0	e	18	0.0800	0.1300	13	290	0.013273	0.013273	0.0265347	FALSE
yo1ce	57523	0	e	16	0.2600	0.2500	26	290	0.053093	0.049087	0.1481613	FALSE
yo1ce	57523	0	e	17	0.2300	0.2200	23	270	0.041548	0.038013	0.1074070	FALSE
yo1ce	57523	0	e	19	0.3100	0.2200	31	200	0.075477	0.038013	0.1134899	FALSE
yo1cf	57523	0	e	24	0.1100	0.1900	19	250	0.009503	0.028353	0.0473202	FALSE
yo1cf	57523	0	e	22	0.1100	0.1800	18	810	0.009503	0.025447	0.1415483	FALSE
yo1cf	57523	0	e	26	0.1200	0.1600	16	270	0.011310	0.020106	0.0424115	TRUE
yo1cf	57523	0	e	25	0.1200	0.0500	12	390	0.011310	0.001963	0.0258828	FALSE
yo1cf	57523	0	e	21	0.2000	0.1100	20	1120	0.031416	0.009503	0.2291476	FALSE
yo1cf	57523	0	e	23	0.2400	0.3700	37	580	0.045239	0.107521	0.4430035	TRUE
yo1cf	57523	0	e	29	1.7000	0.4000	170	100	2.269799	0.125664	1.1977312	TRUE
yo1cg	57523	0	e	27	0.2500	0.1900	25	350	0.049087	0.028353	0.1355203	FALSE
yo1cg	57523	0	e	28	0.2000	0.2100	21	290	0.031416	0.034636	0.0957753	FALSE
yo1ch	57523	0	e	30	0.1400	0.1900	19	330	0.015394	0.028353	0.0721820	FALSE
yo1ch	57523	0	e	36	0.1600	0.1200	16	350	0.020106	0.011310	0.0549778	FALSE
yo1ch	57523	0	e	32	0.1600	0.0800	16	250	0.020106	0.005027	0.0314159	FALSE

## LWD master

yo1ch	yo1c	57523	0	34	34	0.1200	0.1400	14	3.00	0.011310	0.015394	0.0400553	FALSE
yo1ch	yo1c	57523	0	31	31	0.1100	0.1400	14	3.20	0.009503	0.015394	0.0398354	FALSE
yo1ch	yo1c	57523	0	35	35	0.1100	0.0900	11	3.40	0.009503	0.006362	0.0269706	FALSE
yo1ch	yo1c	57523	0	33	33	0.1000	0.1000	10	2.50	0.007854	0.007854	0.0196349	FALSE
yo1ci	yo1c	57523	0	37	37	0.1600	0.0600	16	2.00	0.020106	0.002827	0.0229336	FALSE